HAZY

a brief introduction to CLOUDY 80.06 Introduction and Commands

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CLOUDY 80.06

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1 INTRODUCTION

This is a brief synopsis of the input, output, and assumptions for the radiative-collisional equilibrium program CLOUDY. It fully defines the commands used to drive the program and the output it generates. The methods, approximations, and assumptions used by CLOUDY are outlined, although this part, like CLOUDY itself, is still under construction.

1.1 Overview

Many environments are encountered in which dilute gas is heated and ionized by the radiation field of a central object. Under these circumstances it is possible to predict the physical conditions (that is, the run of ionization, density, and temperature) of the gas, and its resulting emission-line spectrum, in a unique and self-consistent manner. This is done by simultaneously solving the equations of statistical and thermal equilibrium, equations which balance ionization-neutralization processes, and heating-cooling processes, respectively. Osterbrock (1988) and Aller (1984) provide definitive synopses of the basic physics governing such environments, with particular emphasis on low-density nebulae ionized by relatively soft radiation (i.e., starlight), while Davidson and Netzer (1979), Halpern and Grindlay (1980), Kallman and McCray (1982), Kwan and Krolik (1981), Wills, Netzer, and Wills (1985), and Ferland and Shields (1985) provide additional details of effects of high-energy radiation and line transfer.

1.2 What Must be Specified

One powerful asset of photoionization analysis is the large number of observables resulting from only a few input parameters. Intensities of roughly 500 emission lines are predicted by CLOUDY (many of these are of negligible intensity at any one time, of course) and these result from the specification of only a) the shape and intensity of the incident continuum, b) the chemical composition of the gas, and c) the geometry of the gas, including its radial extent and the dependence of density on radius. The following subsections describe the general philosophy of the specification of each.

1.2.1 Incident Continuum

Both the shape and intensity of the incident continuum must be specified.

The shape of the continuum should be specified between an energy of 1.001×10^{-5} Ryd ($\lambda \sim 1$ cm) and an energy of 100 MeV ($\sim 7.354 \times 10^{6}$ Ryd). (In much of the following discussion energy will be given in Rydbergs. The ionization potential of

1 INTRODUCTION

hydrogen is nearly 1 Rydberg. See section 14.9 below for an exact definition.) A physically motivated continuum spanning the full energy range should be specified, if possible. The continuum can be specified as a fundamental form (such as blackbody emission, optically thin bremsstrahlung emission, or a power-law with optional exponential cutoff), interpolated from tables of points, or a continuum predicted by previous calculations with CLOUDY. Additionally, a set of "built-in" continua (for instance, some of the Mihalas 1972 and Kurucz 1979 model atmospheres, the observed Crab Nebula continuum, or several "typical" AGN continua) can be specified.

The intensity of the continuum must also be specified in some manner. In general, the continuum can be specified as a flux (energy or photon) per unit area of cloud, in which case the inner radius of the cloud need not be specified (a plane parallel geometry will be assumed if the inner radius is not specified), or the continuum can be specified as a luminosity (energy or photon) radiated by the central object into 4π sr, in which case the inner radius of the cloud must be specified. In the first case the predicted emission-line spectrum will give the line intensity (energy radiated per unit area of cloud) and in the second case, the total line luminosity. The intensity of the continuum can be set by specifying the flux of photons, a flux density, or a luminosity, at arbitrary energies, or by giving the absolute visual or bolometric magnitude of the continuum source.

Up to ten continua of any form can be blended. If more than one continuum is entered, then there must be exactly the same number of shape and luminosity specifications. The code will stop if there are not.

1.2.2 Chemical Composition

The program considers hydrogen, helium, carbon, nitrogen, oxygen, neon, magnesium, aluminum, silicon, sulfur, argon, calcium, and iron, in detail. All stages of ionization are treated, and all published charge exchange, radiative recombination, and dielectronic recombination processes are included as recombination mechanisms. Photoionization from valence and inner shells and many excited states, as well as collisional ionization by both thermal and supra-thermal electrons, are included as ionization mechanisms. The default composition is close to a solar mixture, several other standard mixtures can easily be specified, and an arbitrary composition can be entered.

1.2.3 Geometry

The geometry is always spherical, but can be made effectively plane parallel by making the inner radius much larger than the thickness of the cloud. The default is for the gas to be constant density and fully fill its volume, but several other pressure laws and models with only part of the volume filled can be computed as well.

CLOUDY normally assumes an "open" geometry, or one in which the gas has a very small covering factor (these terms are defined in section 2 below). This can be changed with the "SPHERE" command, which sets the covering factor to a large enough value for continuous radiation escaping the cloud in the direction towards the central object to always interact with gas on the other side. Line photons which cross the central hole interact with gas on the other side if "SPHERE STATIC" is set, but do not interact (because of a Doppler shift due to expansion) if "SPHERE EXPANDING" is set (this case is the default when "SPHERE" is specified).

1.2.4 Velocity Structure

Normally, CLOUDY assumes only thermal broadening of lines, the absence of any sort of internal velocity structure, and that the gas covering factor is so small that photons escaping the computed ionization structure do not interact with other emitting gas (i.e., an open geometry is assumed).

These assumptions can be changed in several ways. A component of microturbulence can be added with the "TURBULENCE" command. A "WIND" model, in which case a Sobolev (large velocity gradient) model is assumed, can be computed.

1.3 What is Computed and Printed

CLOUDY is driven by a set of command lines which are four letter keywords (either upper or lower case) followed by free format numbers which may be mixed with letters. Normally CLOUDY is executed as a stand-alone program. In this case fortran unit 5 is read for input, and unit 6 is used for output. It is also possible for a larger program to drive CLOUDY directly.

The program begins by echoing the input commands (with the exception of lines beginning with an "#", "%", or "*", these line have no effect). The input stream ends with either a blank line or the end-of-file. Some properties of the incident radiation field, such as luminosity and number of photons in certain frequency ranges, are then printed.

CLOUDY works by dividing a spherical nebula into a set of thin concentric shells. The shells are chosen to have thicknesses which are small enough for the physical conditions to be nearly constant within; the physical thicknesses of the shells are continuously adjusted to ensure this. Each of these shells is referred to as a "zone", and typically $\sim 100-200$ zones are computed in a optically thick model. The physical conditions in the first and last zones are always printed and intermediate zones may be printed if needed (this is governed by the "PRINT EVERY" command). The print-out

for each zone begins with a line giving the zone number, its temperature, the distance from the center of the spherical nebula to the center of the zone, and some other properties of the solution. The next line gives some intensities of selected emission lines, while the following line gives the relative contributions of various emission lines to the radiation pressure, if this amounts to more than 5% of the gas pressure. The next lines give the ionization fraction and level populations of hydrogen excited states (2s and 2p are printed separately), and the remaining lines give the relative populations of ionization stages of the remaining elements. Many details about the conditions within the zone are intermixed with these relative populations.

After the zone calculations are complete and the model is finished, some warnings, cautions, or notes about the calculation may follow. The code is designed to check that its range of validity is not exceeded, and to complain if this occurs, or if it feels that some parameter has been mis-set. Next, optional plots of the incident and emergent continua, gas opacities, or heating-cooling curves, etc, may follow.

The final printout begins with a recapitulation of the commands, followed by the predicted emission-line spectrum. The first two columns of the emission-line spectrum give the ion and wavelength, the third column is the log of the luminosity or intensity of the emission line, and the last column gives its intensity relative to the reference line, which is usually H β (others can be chosen with the "NORMALIZE" command). The third column will be either the luminosity (energy radiated by a shell of gas covering Ω sr of the central object), if the continuum luminosity is specified as energy radiated into 4π sr, or the line intensity (energy emitted per square centimeter of the gas slab) if the incident continuum is specified as a flux. If the geometry is spherical, but the continuum is specified per unit area, then the line intensities will be expressed relative to the inner radius. Only the strongest emission lines are printed; the relative intensity of the weakest line to print is adjusted with the "FAINT" command.

Finally, the last page of the printout gives some averages of the ionization fractions over the slab, the optical depths in various lines and continua, the intensity of the continuum emerging from the cloud, and other properties of the nebula.

1.4 Acknowledgements

CLOUDY's development has been added by conversations with far too many people to list here. The roles of Peter G. Martin and Hagai Netzer were special, however. Peter added several of the commands which deal with ordering of supplemental line lists and the luminosity option on the blackbody command, insisted that CLOUDY run on a VAX, and provided access to the University of Toronto VAX 11/780 at a crucial time. Hagai and I have spent countless hours arguing over methods, assumptions, and just whose code had the bug. These comparisons are the only way to debug codes as large as CLOUDY or ION. My collaborators, J. Baldwin, R. Boyd, E. Capriotti, R. Carswell, S. Cota, M. Elitzur, A. Fabian, C. Gaskell, R. Johnstone, K. Korista, D. Lambert, W. Mathews, J. Mihalszki, R. Mushotzky, S. Persson, M. Rees, G. Shields, and J. Truran contributed to the development of various parts of CLOUDY. Portions of the code were written by R.F. Carswell, S.A. Cota, and P.G. Martin. Sections of the code are taken from published work of Hummer (1988) and Press et al. (1986). Significant problems or suggestions which led to the improvement of CLOUDY were discovered/made by M. Diaz, B. Espey, M. Gaskell, R. Johnstone, S. Morris, and G. Perola.

Finally, the development of CLOUDY would not have been possible without the continued support of The National Science Foundation, through grants AST 80-2522, 83-05094, 85-12414, 87-19607, and most recently AST 90-19692. A generous allotment of time on the Ohio Supercomputer Center CRAY Y-MP is also gratefully acknowledged.

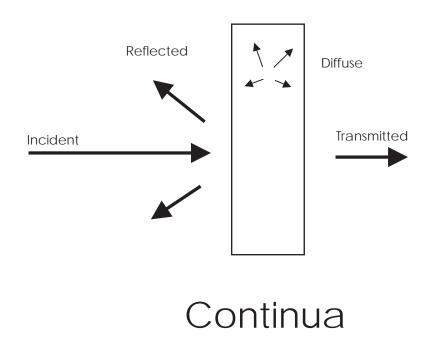


Figure 1: This figure illustrates several of the continua which enter in the calculations. Individual continua can be output by use of the "punch" command. continua

2 **DEFINITIONS**

2.1 Continua

Figure 1 shows several of the continua computed in the calculation.

Incident continuum The incident continuum is the external continuum emitted by the central object and striking the illuminated face of the cloud. It is usually specified in the initial conditions for the calculation. Usually absorption of the incident continuum is the only energy source for the cloud. Within the cloud the incident continuum is diminished by extinction.

Diffuse continuum The diffuse continuum (often referred to as the diffuse field) is the radiation field emitted by gas within the nebula. Examples include the Lyman,

2.2 Geometry

Balmer, or two-photon continua emitted by hydrogen. These fields are very nearly isotropic, and can be significant sources of ionizing radiation under some circumstances.

The main difference between the calculation of a stellar atmosphere and a model nebula is in the treatment of the diffuse fields. In a nebula they are by definition much weaker than the attenuated incident continuum, and the gas albedo is generally small. By contrast, in a stellar atmosphere the local mean intensity is often dominated by the diffuse field. As a result the diffuse fields can be treated by lower order approximations in a nebula than in a stellar atmosphere.

Transmitted continuum The transmitted continuum is the net continuum emergent from the shielded face of the cloud. It includes both the attenuated incident continuum and the transferred diffuse continuum.

Reflected continuum The reflected continuum is the continuum emitted from the illuminated face of the cloud in the direction towards (i.e., within 2π sr of) the source of the incident continuum. This is only computed for an open geometry (defined below).

2.2 Geometry

The geometry is always spherical, but can be changed to effectively plane parallel by making the inner radius much larger than the thickness of the cloud. In addition, it is possible to make the geometry nearly cylindrical, or a wind. The summary at the end of the calculation will say whether the geometry was plane parallel (i.e., the thickness over the inner radius, $\delta r/r_{in} < 0.1$), a thick shell ($\delta r/r_{in} < 3$), or spherical ($\delta r/r_{in} \geq 3$).

Illuminated and shielded faces of the cloud. The side of the cloud in the direction towards the source of ionizing radiation is referred to as the illuminated face of the cloud while the opposite side of the cloud is referred to as the shielded face of the cloud.

Covering factor The covering factor is the fraction of 4π sr covered by gas, as viewed by the central source of ionizing radiation. It is normally written as $\Omega/4\pi$ (Osterbrock 1988), has the limits $0 \leq \Omega/4\pi \leq 1$, and is the fraction of the radiation field emitted by the central object which actually strikes nebular gas. Many of the predicted luminosities are for a shell covering Ω sr, while line intensities are per unit area.

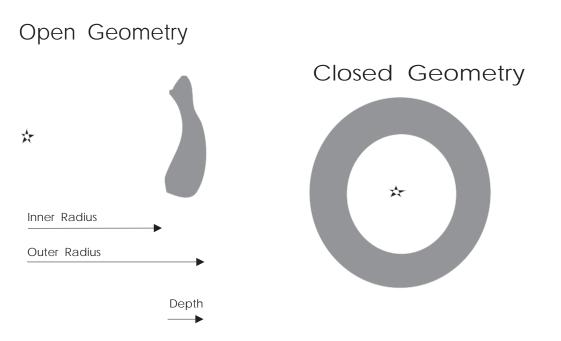


Figure 2: This figure shows the two limiting geometries which can be assumed in the calculations. The hatched area represents nebular gas. An open geometry is the default, and a closed geometry will be computed if the "sphere" command is entered. geometry

2.2.1 Open vs closed geometry

Two limiting cases can be identified for the geometry and its influence upon the ionization calculations. Here, they are referred to as "open" and "closed" geometries. Figure 2 shows examples of both. Which is the best approximation depends on the gas covering factor. The choice largely affects the calculation of the diffuse fields. These are defined in the following.

Open geometry An "open" geometry is one in which the covering factor of the gas is small and all radiation which escapes from the illuminated face of the cloud, towards the source of continuous radiation, then escapes from the system without further interaction with the gas. This is thought to be the case in, for example, the broad-line region of active nuclei or filaments in the Crab Nebula. In this case $Ly\beta$ and higher lines can escape from the nebula, and the "on-the-spot" assumption cannot be used for the innermost regions of the nebula. This geometry is the default condition for the code, and will be assumed if the "SPHERE" command (described below) is not specified.

2.2 Geometry

Closed geometry Here, emission-line gas covers $\sim 4\pi$ sr as seen by the central star. If the star is small relative to the nebula, then all diffuse fields emitted by the nebula, which escape from the illuminated face of the nebula towards the star, then go on to strike the other side of the nebula. This geometry is implicitly assumed in most calculations of planetary nebulae and H II regions. Here, the "on-the-spot" assumption provides an excellent description of the hydrogen ionization balance (see, for example, Van Blerkom and Hummer 1967; Bässgen et al. 1988; Osterbrock 1988). This geometry will be assumed if the "SPHERE" command is entered.

Static vs expanding The SPHERE command has two optional arguments, "STATIC" and "EXPANDING", which determine how line photons from either side of the shell interact. The "STATIC" option causes the code to assume that the shell is stationary, so that all lines interact across the nebula. In this case, Lyman line interaction should ensure that case B emissivity is reached. If $\Omega/4\pi \sim 1$ but the nebula is expanding then the diffuse fields interact across the nebula, but the expansion velocity of the shell ensures that diffuse line photons do not; in this case the "EXPANDING" option should be set. This second case is the default when SPHERE is specified with no options.

These geometrical considerations make differences in the predicted emission-line spectrum at the $\sim 10\%$ level, largely because of the different treatments of the diffuse fields and line optical depths.

Matter-bounded The nebula is said to be matter-bounded if the outer limit to the emission-line region is marked by the outer edge of the cloud. In this case the cloud is optically thin to the incident continuum.

Radiation-bounded The nebula is said to be radiation-bounded if the outer limit to the emission-line region is marked by an ionization front. In this case nearly all of the incident continuum has been absorbed by the cloud.

3 LIMITS, ASSUMPTIONS, AND RELIABILITY

This section outlines some of the assumptions and limits which define the range of validity of CLOUDY. The code is designed to check that the limits of its validity are not exceeded during a calculation. CLOUDY should print a warning after the last zone results if any aspects of the calculation are on thin ice.

3.1 Time Steady

Although it is possible to follow the time-dependent recombination and cooling of an optically thin cell of gas following the rapid extinction of the radiation field with the "TIME" command, steady-state is generally assumed. Various time scales characterize the approach to equilibrium of an ionized gas (see Spitzer, 1962, and Ferland 1979 for a specific application); generally, the longest is the recombination time scale,

$$T_{rec} \approx \frac{1}{\alpha(T_e) N_e} \approx 1.15 t_4^{0.8} N_9 \ hours \tag{1}$$

where t_4 is the temperature in units of 10^4 K, and N₉ is the density in units of 10^9 cm⁻³. CLOUDY is not appropriate for the treatment of situations where conditions change more rapidly than this.

3.2 Atomic Database

By its nature, the electron temperature of a photoionized gas is low compared with the ionization temperature of the mixture of atoms and ions, as defined by the Saha equation (if the two were comparable, the gas would be collisionally ionized). Because of this, the rate coefficients describing collisional effects, such as the production of cooling emission lines, are often dominated by the cross section near threshold. This is where laboratory experiments are difficult and *ab initio* quantum theory must often be used. As a result, the collision strengths undergo constant revision, hopefully towards better and more reliable values. To cite one extreme example, the collision strength for transitions within the ³P ground term of Ne⁺⁴ has undergone three revisions between 1984 and 1991, each by a factor of 10, because of theoretical uncertainties in positions of autoionizing states which have not been observed (Lennon and Burke 1991). The intensities of all emission lines can be affected by major changes in the atomic data for only one line for some conditions. This is because (in this case) the infrared fine structure lines of Ne⁺⁴ can be important coolants in low-density high-ionization gasses such as planetary nebulae, and changing their cooling rate alters the thermal structure

3.3 Continuous Opacity

of the entire nebula. Such changes often give even models of time-steady objects such as planetary nebulae certain time-dependent characteristics.

At present, there are fairly reliable calculations of collision strengths and transition probabilities for the majority of the important coolants in moderate ionization nebulae. This is not the case for photoionization cross sections, recombination coefficients, and charge transfer rate coefficients. Photoionization cross sections for inner electron removal by high energy radiation are fairly well known; the uncertainties are in the valence cross sections. To cite one extreme example, the cross sections for removal of outer electrons of atoms and ions of sulfur have been calculated by Chapman and Henry (1971) and by Reilman and Manson (1979). The Chapman and Henry results are consistently larger than those of Reilman and Manson, often by factors approaching 10. Similarly, low-temperature (through low-lying autoionizing states) dielectronic recombination rate coefficients have not been computed for most third row elements and iron. Extensions to the Opacity Project (Seaton 1987) should soon correct this situation. These differences result in a factor of four difference in the predicted intensity of [S II] 6731 in certain H II region calculations, where valence shell photoionization is especially important. The differences are smaller for planetary nebulae or active galactic nuclei where inner electrons are energetically accessible (because the radiation field is much harder). CLOUDY uses unpublished cross-sections of Mendoza; these are intermediate between the two published extremes. Fortunately, the photoionization-recombination cross section database will improve dramatically with the completion of the Opacity Project and its extension to recombination processes, in a few years.

Another uncertainty in the atomic/molecular data base is the rate coefficients for charge transfer. This process is often the dominant neutralization mechanism for singly or doubly ionized heavy elements. At present some charge exchange rate coefficients are the result of Landau-Zenner calculations using semi-empirical potential curves; these are thought to be accurate to better than a factor of three. Even the best quantal calculations of charge transfer rate coefficients are not thought to have an accuracy much better than 50 percent. Unpublished tests suggest that these uncertainties affect many line intensities at the $\sim 20\%$ level, and some by more than this. These uncertainties underscore the importance of atomic/molecular theory for the interpretation of astrophysical spectroscopy.

3.3 Continuous Opacity

All significant continuous opacity sources are treated for the energy range considered by the code, 1.001×10^{-5} Ryd to 7.354×10^{6} Ryd. These opacity sources include inverse bremsstrahlung, grains (when present), H⁻ absorption, electron scattering, the damping wings of hydrogen Lyman lines (i.e., Rayleigh scattering), pair production, photoelectric absorption by the ground and excited states of the 13 elements included in the calculation, and photoabsorption by molecules. This treatment should be adequate as long as the optical depths to electron scattering are not large; CLOUDY is not now designed to model Compton-thick regimes.

A warning will be issued after the last zone calculation if the nebula is optically thick to an opacity source which is not fully treated.

3.4 Temperature Range

CLOUDY assumes that the electrons are non-relativistic, which limits it to temperatures below roughly 10^9 K. Tests (see section 20.3 below) show that CLOUDY goes to the Compton temperature of the radiation field to great accuracy in the limit of very high levels of ionization for blackbody radiation fields between 3K and 10^{10} K. There is no formal lower temperature limit to its validity, but the approximations used for ionic recombination coefficients (Pequignot and Aldrovandi 1986) were not intended for temperatures below 10K, (gas this cold is generally molecular, however) and the approximations for most charge transfer rate coefficients were not intended to be used below temperatures between 10^2 K to 10^3 K. The free-free gaunt factors, taken from Hummer (1988), do not extend above ~ 10^8 K or below ~ 10^3 K.

The present range of validity of the code is now approximately from 10K to 10^9 K. Temperatures outside this range can still be treated, although with greater uncertainty. (This applies to ions, atoms, and hydrogen molecules over the stated temperature range; work on heavy element molecules is still in progress.)

3.5 Density Range

There is no formal lower limit to the density which CLOUDY can treat. The set of heavy element fine structure lines, which dominate cooling at low densities, is complete for low and moderate stages of ionization, and fine structure optical depth and maser effects are fully treated using the escape probability formalism. Note that for very low density models ($N_H \leq 10^{-1}$ cm⁻³) with "typical" values of the ionization parameter (defined below) it is usually necessary to also consider diffuse sources of radiation such as the cosmic x-ray background, diffuse interstellar starlight, and the cosmic ray background. These must be specified independently as part of the incident continuum.

There is no formal high density limit, other than the (inexact) treatment of radiative transfer (see Avrett and Loeser 1988) and the approximate treatment of the collisional-radiative ionization processes for excited levels of the heavy elements. Hydrogen and atoms and ions of helium are treated as 10-level atoms, including all of the physical processes which allow the approach to LTE (see, for example, Mihalas 1978). Tests with a hydrogen density of 10¹⁹ cm⁻³ show that CLOUDY's hydrogen

and helium atoms do go to LTE at high densities; thus there is no formal high density limit to its validity. The treatment of Stark broadening for hydrogen lines follows Puetter (1981), so radiative transfer is treated correctly (in the context of the escape probability formalism) for densities above $\sim 10^{10}$ cm⁻³. The treatment of the other 11 elements is presently not as complete as hydrogen and helium, but 3-body recombination is included as a general recombination process, so the treatment of these elements is approximately correct at high densities.

CLOUDY has been tested at densities of 10^{-4} cm⁻³ and 10^{19} cm⁻³ on 32-bit machines. The numerical (not physical) limit to the density will actually be set by the limits to the range of the floating point numbers allowed by the machine in use (densities of 10^{-6} cm⁻³ and 10^{20} cm⁻³ don't work on IEEE 32-bit machines for this reason). The physics incorporated in the code imposes no lower limit to the density. The physical high-density limit is probably now set by the approximate treatment of three-body recombination-collisional ionization for the heavy elements ($\geq 10^{13}$ cm⁻³), and the approximate treatment of line transfer (i.e., escape probabilities). Non-LTE ionization, thermal equilibria, and line transfer at high densities is an area of on-going research.

3.6 Radiative Transfer

Line intensities are computed with stellar atmosphere conditions in mind. This means that radiative transfer effects, including possible maser emission, are treated. Collisional effects, including excitation and de-excitation, continuum florescence, recombination, etc, are all included as general line excitation mechanisms, and "nebular" approximations, such as the approximation that all atoms are in the ground state, are not made. The treatment of level populations is designed to go to LTE in the high density case.

Line and continuum transfer is currently treated using escape probabilities. This is probably the weakest assumption in the present prediction of the line intensities. Work is now underway to begin the conversion to formally correct transport methods. There is no way to judge the error introduced by the escape probability approximation, although it is known to be exact if the conditions do not vary across the line forming region (Elitzur 1982).

3.7 Hydrogen

Hydrogen is treated as a ten level (plus continuum) atom. The 2s and 2p states are treated separately, so $Ly\alpha$ and 2-photon emission are computed properly in low-density nebulae. Quantum numbers between 3 and 6 are treated assuming full l-mixing, as in Seaton (1959), but with all collisional and radiative transfer effects included. Levels between 7 and 100 are treated by substituting three pseudo-states with properties chosen to mimic these high-n states. Tests show that the hydrogen line emissivity predicted by CLOUDY agrees with all of Seaton's results to ~ 0.1%, and with Hummer and Storey's (1987) case B H β emissivity predictions to ~ 1% for $N_H \leq 10^{10}$ cm⁻³.

Although the H β emissivity is predicted by CLOUDY with great precision for all densities, this is not true of the infrared hydrogen lines at low densities. The intensities of these lines are somewhat sensitive to the degree of l-mixing of the upper levels. They are predicted with precision in the context of the *full l-mixing* approximation, but this approximation is not valid for low densities. The differences can be judged by comparing Seaton's (1959) calculation (which CLOUDY reproduces to three significant figures) with the *l*-state calculations presented by Pengelly (1964). One of the worst cases is Paschen α , for which Seaton predicts intensities 21% smaller than Pengelly. Beware.

The full set of hydrogen level balance equations are solved by working with LTE departure coefficients. As a result, the departure coefficient of the ground state diverges for very low temperatures when the gas is ionized yet cold, so it is not possible to treat hydrogen line transfer in detail for temperatures below 1000K on 32-bit machines. For very low temperatures CLOUDY uses a special set of approximations (fitted to the results of Martin 1988) to solve for the hydrogen ionization balance and predict emissivities. The intensities of these lines are reliable for temperatures above $\sim 10^2$ K as long as radiative transfer and optical depth effects are not important. (It is unlikely that significant HII emission will occur for gas colder than this 10^2 K limit.) If such low temperatures occur, and the matrix solution is not used, then a comment is printed after the last zone calculation.

Finally, the hydrogen density used by CLOUDY is the *total* hydrogen density, usually referred to by the label "HDEN", and is given by

$$N(H) = N(H^{\circ}) + N(H^{+}) + N(H^{-}) + 2N(H_{2}) + 2N(H_{2}^{+}) + 3N(H_{3}^{+}) \quad .$$
(2)

3.8 Helium

Model atoms. Helium is treated as three separate atoms/ions; ionized helium (a ten level atom), the singlets (a ten level atom), and the triplets (presently a five level atom). The treatment of the three ions is entirely analogous to that of hydrogen; it goes to LTE in the limits of large photon or particle densities. The low-temperature limit to the matrix treatment of the He^o singlets and He⁺ are 1000K and 1500K respectively. Below these temperatures approximations to case B results are used.

As with hydrogen, these model singlet and He⁺ atoms assume complete l-mixing for levels $3 \le n \le 100$. As mentioned above, this is not a good approximation for low densities. For instance, the intensity of $\lambda 4686$ is exact at high densities, but differs by nearly 40 percent from low density case B predictions. For the time being, it is probably better to use the case B predictions, rather than the results of the 10-level atom calculations, for HeII line emission at low densities, when line transfer and collisional excitation are not important. The predictions of the ten-level atom are better when either process is important, or the density is high enough for complete l-mixing to be a good approximation.

Helium Radiative Transfer. The helium line and continuum transfer problem is one whose importance in determining the intensities of many ultraviolet lines is generally underestimated (see, for example, the discussion by Netzer and Ferland 1984). Recombinations to the He⁺ ground and first excited state, and HeII Ly α , all ionize hydrogen, and the He II Ly α line undergoes Bowen fluorescence (Osterbrock 1988; Netzer, Elitzur, and Ferland 1985). Unfortunately these continua, and especially the Bowen lines, can be the main source of photoelectric heating in the He⁺⁺ zone of some high-ionization nebulae. Fundamental uncertainties in the treatment of the Bowen problem introduce substantial uncertainties in the local heating rate, and hence in the intensities of some ultraviolet lines, such as C III] λ 1909 and C IV λ 1549, because these lines are very temperature sensitive. My experience is that minor changes in the treatment of the Bowen problem typically results in ~ 20% changes in the intensities of these ultraviolet lines in certain low density nebulae, and in the near ultraviolet [Ne V] lines.

3.9 Atoms and Ions of the Heavy Elements

Most heavy elements are treated as two level systems (ground term and continuum) although photoionization from excited states is included for those cases where it is sometimes important (O^{++} and N^+ are two examples). All published charge transfer, radiative and dielectronic recombination, collisional ionization, and three body recombination processes are included in the ionization balance.

The treatment of the heavy element ionization balance should be exact in the nebular limit, but approximate for very high photon or particle densities because of the two-level treatment.

3.10 Molecules

At the present time a major effort is being made to complete the treatment of the heavy-element molecular equilibria and cooling in the code. The treatment of the hydrogen molecules/ions H⁻, H₂, H₂⁺, H₃⁺, and HeH⁺ is now fairly complete. The equilibrium of the heavy-element molecules is now treated with various levels of approximation. The predictions are thought to be correct for nebular (N < 10^8 cm⁻³)

conditions, but do not now go to LTE in the high nucleon-photon limits, and do not go to the fully molecular limit.

3.11 Reliability

There are several issues to address in regards to the general question of reliability of the code. The first is the effects of the bugs which surely must exist in a code the size of CLOUDY. I have seldom found bugs in sections of the code older than roughly $\sim 2-3$ years. Younger sections of the code sometimes contain bugs that only manifest themselves in exceptional situations. It is my belief that the issue of reliability in the face of complexity will increasingly be the single major problem limiting the development of large-scale numerical simulations. New methods of writing code will have to be developed if we are to take full advantage of the power of future machines. Machines are getting faster more quickly than people are getting smarter.

Test cases which are designed to exercise the code in certain well-posed limits are presented in sections 25 and 24 below. Calculations of certain standard nebulae are also shown there. The code is well-behaved in these simple limits, and agrees well with predictions of similar codes when applied to "nebular" situations.

The second issue is the validity of the numerical methods used to simulate conditions in the nebulae. Fundamental uncertainties arise for cases where the density is high (N $\gg 10^{10}$ cm⁻³). The radiative transfer techniques used by CLOUDY are approximate (see the discussion by Avrett and Loeser 1988). Unfortunately, no definitive calculation now exists for the complete non-LTE equilibrium and emission for an intermediate density (~ 10^{10} cm⁻³) cloud. For less extreme conditions (N $\ll 10^{10}$ cm⁻³) nebular approximations are valid, and the comparisons presented below (section 24) shows good agreement with other codes designed to work in this limit.

Uncertainties in the atomic data base are a third concern. A great deal of progress will result over the next few years with the completion of the Opacity Project (Seaton 1987), although charge transfer, a process normally treated on a molecular basis, will remain an uncertainty.

In the end the uncertainties can probably best be judged by looking at both the dispersion among the various photoionization calculations presented in section 24 and the changes that have occurred in the predictions made by CLOUDY itself over the past few years. Much of the dispersion is due to changes in the atomic data base, changes which are likely to settle down with the completion of the Opacity Project.

3.12 The Future

The eventual goal is for CLOUDY to give reliable results for all extremes of conditions between and including the intergalactic medium and stellar atmospheres. I estimate

3.12 The Future

that the code is now well over half-way complete.

Current work centers on making the code formally correct in the optically thin limit for all extremes of radiation and matter densities. Much has already been done, and present efforts center on helium, molecules, and the heavy elements.

Line transfer is now treated with escape probabilities, an approximation which is not formally correct when conditions vary across the line forming region (see, for instance, Avrett and Loeser 1988). A major change, to be completed within the next year, is to transfer Ly α correctly, using the proper mixture of redistribution functions, using an approach similar to that of Hummer and Kunasz (1980).

By the time this work is complete, the Opacity Project (Seaton 1987) should also be finished, and attention will return to the heavy elements. An approach similar to that now used for hydrogen and helium (employing several pseudo-states to allow the model atom to correctly approach LTE) will be used to ensure that the treatment of the heavy elements is correct for all densities and temperatures.

The two major remaining concerns will be the continuum transport (especially in the infrared) and line transfer (complete redistribution is a good approximation for most lines). Both can be treated in a straightforward manner using standard radiative transfer techniques.

4 COMMANDS

This section summarizes the commands which drive CLOUDY. They are grouped together by purpose, and individual commands are discussed after examples of their use.

4.1 Default Conditions

CLOUDY is designed to be easy to use, so that a minimum number of commands are needed to drive it. The general philosophy is for a reasonable set of initial conditions to be assumed by default. These default conditions are summarized in Table 1. The code is also designed to check that its assumptions are not violated, and to complain if problems occur, if its limits are exceeded, or if the input parameters are misused.

Table 1: Default Conditions

Variable	Value	Section	Quantity
rdfalt	$10^{25} { m ~cm}$	4.8.4	default inner radius
router	$10^{30} { m ~cm}$	4.8.4	default outer radius
telow	10K	4.10.9	lowest temperature allowed by code
tehigh	$10^{10}\mathrm{K}$	-	highest allowed temperature
tend	$4000 \mathrm{K}$	4.11.7	lowest temperature to allow in model
thlo	$1000 \mathrm{K}$	4.9.7	lowest temperature in H^o matrix
the1lo	$1000 \mathrm{K}$	-	lowest temperature in He° singlet matrix
the2lo	$1500 { m K}$	-	lowest temperature in He ⁺ matrix
flxfnt	10^{-10}	4.14.6	relative flux of high energy to consider
cylind	$10^{35} { m ~cm}$	4.8.2	half-thickness of cylinder in geometry
toler	0.02	4.10.15	tolerance in heating-cooling match
faint	10^{-4}	4.12.1	relative intensity of faintest line to print
emm	$1.001 \times 10^{-5} \mathrm{Ryd}$	-	low energy limit to radiation field
egamry	$7.354 \times 10^{6} \mathrm{~Ryd}$	-	high energy limit to radiation field
nend	300	4.11.9	limiting number of zones
colend	$10^{30} { m cm}^{-2}$	4.11.2	limiting total hydrogen column density
colpls	$10^{30} { m cm}^{-2}$	4.11.2	limiting ionized hydrogen column density
colnut	$10^{30} {\rm ~cm^{-2}}$	4.11.2	limiting neutral hydrogen column density
grains?	no grains	4.9.5	grain mixture
abundances	"solar"	4.6.1	default composition

4.2 Command Format

When executed as a stand-alone program, CLOUDY reads Fortran unit 5 for input and produces output on unit 6. The code is also designed to be used as a subroutine of other, much larger, programs. In this case the input stream is entered using the subroutine calls described in section 10 below. In either case, this input stream must contain the commands used to drive the program. The commands used to set the initial conditions in code are described next.

All commands are entered as free format lines, beginning with a four character key word specifying the purpose of the command, and usually followed by one or more numbers or keywords. Up to 100 separate commands may be entered; this is limited by the variable NKRD which appears in several parameter statements throughout the code. Most commands use cgs units. The command lines can be in any order, and can be up to 80 characters long, in either lower or upper case. The end of each line is marked either by column 80, the end-of-line, a colon ":", a semi-colon ";", or a percentage sign "%". The input stream ends with either a blank line or the end-of-file. In the following examples the individual command keywords are shown extending beyond column 4, and these extra characters are completely ignored (except for some special commands which use optional keywords).

4.2.1 Example formats

Sections describing each of the commands are introduced by examples of their use. In these examples optional parameters are shown surrounded by square brackets ("[" and "]"). Examples are shown below.

```
*following needs flux density, but frequency is optional
f(nu) = -12.456 [at .1824 Ryd]
*the luminosity command has several optional keywords
luminosity 38.3 [solar, range, linear]
*the phi(h) command has the range option
phi(h) = 12.867 [range ...]
```

These indicate only that the parameters are optional, and the brackets need not be input on the command line.

Most commands require four character matches to be recognized. In some cases the leading character is a blank, which is indicated by an underscore ("_", an example is the keyword "_LTE"). Other examples are shown below. The underscore should not be typed, only a space character.

```
*blackbody with T=50,000, in strict TE
```

blackbody 50,000 lte
* use nlr abundances
abundances nlr

4.2.2 The continue option

It is sometimes not possible to enter all the required values on a single line for the "INTERPOLATE" and "ABUNDANCES" commands. In these two cases the original command line can be continued on following lines with a series of lines beginning with the keyword "CONTINUE". The format on a "CONTINUE" line is unchanged, and there is no limit to the number of "CONTINUE" lines which can be included.

4.2.3 Numerical input

Numbers are entered in free-format, and exponential notation cannot be used. For instance, the entry "1E20" will be interpreted as the numbers 1 and 20, and no error message will result. Generally, CLOUDY avoids exponential notation on input by entering numbers as logs, so "1E20" is usually entered as "20.0". Commas can be freely embedded in input numbers and they may be preceded or followed by characters to increase readability (i.e., "T=1,000,000K" and "1000000", and usually "T=6", are equivalent, but T=1E6 is not). A period or full stop (".") by itself is interpreted as a character, not numeral or number. Default values are often available. As an example, the "POWER LAW" command has three parameters, the last two being optional. The following are all acceptable (but not equivalent) forms of the command;

```
power law, slope=-1.4, exponential cutoffs at 9 Ryd and 0.01 Ryd powe -1.0 5 power law, slope=-1.4 .
```

The last version uses the default cutoffs, i.e, none. Note that implicit negative signs (for instance, for the slope of the power law) *do not* occur in any of the following commands.

4.2.4 Comments

Comments may be entered among the input data in several ways. Anything on a line which occurs after a colon, semi-colon, or percentage sign is completely ignored; this can be used to document parameters on a line. Any line beginning with a "#", "%", or a "*" is totally ignored; it is not even printed. A line beginning with "c_" is ignored, but printed (note that there was a space after the c). There is also a "TITLE" command, to enter a title for the model, as described below.

4.2.5 Some systematics

An attempt has been made to beep the input quantities as logical as possible. Most quantities are entered as the log of the number, but some are linear. Many commands have the sub-keywords "_log" and "linear" to force one or the other interpretation to be used. The following outlines some systematics of how these are entered.

Temperature CLOUDY will interpret a temperature as a log if the number is less than or equal to 10, and linear if greater than 10. Many commands have the optional keyword "linear" to force temperatures below 10K to be interpreted as the linear quantity rather than the log.

Linear vs log for other parameters The pattern for other quantities is not as clear as for the case of temperature. Generally, quantities are interpreted as logs if negative, but may be linear or logs if positive (depending on the command).

4.2.6 An example

Specific commands to describe the continuum (luminosity and shape), and geometrical details are discussed next. As a minimum, the hydrogen density, continuum shape, continuum luminosity or intensity, and possibly the starting radius, must be specified. As an example, a simple model of a planetary nebula could be computed by entering;

```
title - this is the input stream for a simple planetary nebula
* this is the temperature and total luminosity of the central star
black body, temperature = 100,000K, luminosity=38;[log(L)- ergs/s]
radius 17 ;log of starting radius in cm
hden 4 ;log of hydrogen density - cm<sup>-3</sup>
filling factor 0.3 ;set a filling factor of 30 percent
sphere ; tell cloudy this is a sphere with large covering factor
```

4.3 Combinations of Continua

The continuum shape can be set by interpolating on tables of points, read in from predictions of previous calculations, and/or by specifying fundamental forms such as blackbody, power law, or bremsstrahlung emission. It is possible to combine up to 10 continua of any shape.¹ When more than one continuum is entered, the series of

¹Restrictions on the number of tables which could be entered existed in CLOUDY versions 73 and before, but have been lifted. Restrictions on which types of continua could be combined existed in CLOUDY versions 67 and before, but have been lifted.

luminosity and shape commands must be in the same order (i.e., map one to one). There must always be exactly the same number of continuum luminosity and shape specifications; CLOUDY will stop if there are not.

As an example, the following would be a rough approximation of an accretion disk and boundary layer around a white dwarf:

```
black body, temp=500,000K
luminosity (total) 37
power law, slope=1.333, cutoff=0.6 Ryd; this is a rising power law
luminosity (total) 37
```

CLOUDY will stop if more than 10 continua are entered. This limit is set by the variable LIMSPC which occurs in several PARAMETER statements throughout the code. Increase LIMSPC everywhere if more than 10 continua are required.

4.4 Continuum Luminosity

The commands setting the intensity or luminosity of the continuum are described here. CLOUDY actually works with continuum fluxes in units similar to "photons cm⁻² s⁻¹ Ryd⁻¹", to avoid single-precision floating-point exponent limits on 32-bit IEEE machines. The intensity of the incident continuum can be set by specifying a luminosity, the number of photons, a flux density f_{ν} , or the absolute visual or bolometric magnitude. These can be the quantity emitted by the central object into 4π sr (with units s⁻¹) or the surface flux at the illuminated face of the cloud (with units cm⁻² s⁻¹). The intensity of the predicted emission lines will be either a intensity (energy radiated per unit area of cloud), or the luminosity radiated by a shell covering Ω sr, where Ω is the angular coverage of the nebula and $\Omega/4\pi$ is the covering factor. Which is predicted depends on how the incident continuum was specified.

4.4.1 Continuum Normalization

For many luminosity or flux commands there is no ambiguity as to whether the incident continuum is specified as per unit area of cloud surface, or the continuum radiated into 4π sr. Examples include the "IONIZATION PARAMETER" command (continuum per unit area) and the "LUMINOSITY" command. For other commands there may be an ambiguity. In these cases CLOUDY assumes that the quantity is specified as the total radiated into 4π sr if the ionization parameter deduced by assuming that the continuum is per unit area is greater than U= 10^{10} , while the ionization parameter deduced by assuming that the continuum is assumed to be per unit area otherwise.

4.4.2 The RANGE Option

For most of the luminosity commands the default is for the quantity entered to be the number of photons or luminosity in ionizing radiation (13.6 eV $\leq h\nu \leq 100$ MeV). Other energy intervals can be specified with the "RANGE" option, an optional keyword on the "LUMINOSITY", "Q(H)", and "PHI(H)" commands.

The range option appears on the line specifying the luminosity and is invoked by entering the keyword "RANGE". When "RANGE" is specified there are an additional two parameters, the low and high energy limits to the energy range in Rydbergs. These appear as the second and third numbers on the line. The position of the keyword "RANGE" on the command line does not matter, but the order of the numbers on the line does. If the first optional number is negative or the keyword "_log" appears then both of the extra numbers are interpreted as logs. If either parameter is zero then the low $(1.001 \times 10^{-5} \text{ Ryd})$ or high $(7.354 \times 10^6 \text{ Ryd})$ energy limit of the continuum will be substituted. If both energies are specified then the second number must be larger than the first (unless the second is zero). If only one parameter appears then only the lower limit of the range will be changed, and the high energy limit will be left at its default of $7.354 \times 10^6 \text{ Ryd}$. If the keyword "TOTAL" (equivalent to "RANGE TOTAL") appears with no parameters then the full energy range considered by the program will be used.

The following are some examples of the use of the range option in modifying the range on the "LUMINOSITY" command. The default condition on the "LUMINOSITY" command is for the single parameter to be the log of the luminosity (erg s⁻¹) in ionizing (1 Ryd $\leq h\nu < 7.354 \times 10^{6}$ Ryd) radiation.

```
* this will use the default range, only ionizing radiation
luminosity 38 ;log of luminosity in erg/sec
```

```
* either will be the total luminosity
luminosity total 38
luminosity range total 33.4
* this will be the luminosity in visible light
luminosity 37.8 range .15 to .23 Ryd
* the luminosity in radiation more energetic than 0.1 Ryd
luminosity 38.1 range -1
* this will be the luminosity in non-ionizing radiation
luminosity 39.8 range 0 1
```

4.4.3 absolute [visual, bolometric] magnitude -2.3

It is possible to specify the luminosity in "magnitudes", a quaint unit of historical interest. One of the keywords "bolometric" or "visual" must also appear. The absolute bolometric magnitude M_{bol} is related to the total luminosity by

$$L_{total} = 3.826 \times 10^{33} \times 10^{(4.72 - M_{bol})/2.5} \ erg \ s^{-1} \ . \tag{3}$$

The absolute visual magnitude M_V is approximately related to the flux at 5550Å by

$$\nu F_{\nu}(5550 \text{\AA}) \approx 3.086 \times 10^{33} \times 10^{(4.79 - M_V)/2.5} \ erg \ Hz^{-1} \ s^{-1}$$
 . (4)

The conversion between flux and absolute visual magnitude is approximate, with typical errors of roughly a percent, because CLOUDY assumes that the V filter has an isophotal wavelength of 5550Å, and does not actually integrate over the incident continuum using a V-filter transmission function.

The starting radius for the calculation must be specified since this command specifies the luminosity radiated into 4π sr.

4.4.4 f(nu) = -12.456 [at .1824 Ryd]

This command allows the flux density f_{ν} to be specified. The first number is the log of either the specific luminosity radiated by the central object into 4π sr (erg s⁻¹ Hz⁻¹) or the surface flux density at the illuminated face of the cloud (erg s⁻¹ Hz⁻¹ cm⁻²). In the second case the number is $4\pi J_{\nu}$, where J_{ν} is the mean intensity of the incident continuum.

The optional second number is the frequency in Rydbergs where f_{ν} is specified; the default is 1 Ryd, and in the example above the continuum is specified at $0.1824 \text{ Ryd} = 5000\text{\AA}$. The frequency can be any within the energy band considered by the code, presently 1.001×10^{-5} Ryd to 7.354×10^{6} Ryd. If the energy is less than or equal to zero then it is interpreted as the log of the energy in Rydbergs, and the linear energy itself if positive.

It is not necessary to also specify the starting radius if f_{ν} is specified (per unit area) using this command.

4.4.5 ionization parameter = -1.984

The ionization parameter is the dimensionless ratio of photon to hydrogen densities, and is defined as

$$U \equiv \frac{Q(H)}{4\pi r^2 N_H c} \equiv \frac{\phi(H)}{N_H c}$$
(5)

where r is the separation between the source of ionizing radiation and the cloud, N_H is the total hydrogen density (ionized, neutral, and molecular), c is the speed of light, and Q(H) is the number of hydrogen-ionizing photons emitted by the central object (s^{-1}) .² In this expression $\phi(H)$ is the surface flux of ionizing photons $(cm^{-2} s^{-1})$. The number entered is the log of the ionization parameter. The ionization parameter is a useful quantity in plane parallel constant-density models, because of homology relations between models with different photon and gas densities but the same ionization parameter (see Davidson 1977).

It is not necessary to also specify a starting radius since the ionization parameter and hydrogen density together uniquely determine the flux of ionizing photons. If the starting radius is not specified, it is automatically set to 10^{25} cm to produce an effectively plane parallel model. The predicted emission-line intensities will be given as intensities (energy per unit area of emitting gas) unless a starting radius is also specified, in which case a luminosity is predicted.

4.4.6 luminosity 38.3 [solar, range, linear]

The number is either the log of the luminosity emitted by the central object into 4π sr, (erg s⁻¹)

$$L = 4\pi R_{star}^2 \int_{\nu_1}^{\nu_2} \pi F_{\nu} \, d\nu \quad , \tag{6}$$

the surface energy flux (erg $\text{cm}^{-2} \text{ s}^{-1}$) at the inner face of the cloud

$$L = \int_{\nu_1}^{\nu_2} 4\pi J_{\nu} d\nu \quad , \tag{7}$$

or the log of the total luminosity in solar units, if the "SOLAR" keyword is specified. The number is interpreted as the luminosity itself, rather than a log, if the optional keyword "LINEAR" appears on the line.

The default range is over hydrogen-ionizing energies (1 Ryd $\leq h\nu \leq 7.354 \times 10^6$ Ryd). The "RANGE" option can be used to adjust the values of ν_1 and ν_2 . If the integrated mean intensity (equation 7) at the illuminated face of the cloud is specified then the predicted emission-line intensities will also be per unit area of gas. If the continuum intensity is specified as the total luminosity emitted by the central object into 4π sr, the emission lines will be the luminosity radiated by a shell covering Ω sr.

If the optional keyword "SOLAR" appears, the number is interpreted as the log of the *total* luminosity, relative to the luminosity of the sun (unless the "LINEAR" keyword is also used, in which case the quantity will be the relative luminosity itself). The range option cannot be used if the luminosity is specified in solar units (it will be ignored if it appears). The emission-line intensities will be the luminosity radiated by a shell covering Ω sr.

²Before version 65 of the code the electron density was used rather than the hydrogen density. Before version 75 N_H was the atomic/ionic hydrogen density, and did not include molecules.

The following are examples of the luminosity command.

```
*log of luminosity (erg/s) in ionizing radiation
luminosity 36
* roughly the eddington limit for one solar mass
luminosity total 38
* both are a total luminosity 1000 times solar
luminosity solar 3
luminosity linear solar 1000
* this will be the luminosity in visible light
luminosity 37.8 range .15 to .23 Ryd
```

It may or may not be necessary to specify a starting radius, depending on whether the luminosity or flux is specified.

$4.4.7 \quad nuf(nu) = 43.456 [at .1824 Ryd]$

This command allows the flux density νf_{ν} to be specified. The first number is the log of either the specific luminosity radiated by the central object into 4π sr (erg s⁻¹) or the surface flux density at the illuminated face of the cloud (erg s⁻¹ cm⁻²). Either can be at an arbitrary frequency. In the second case the number is $4\pi\nu J_{\nu}$, where J_{ν} is the mean intensity of the incident continuum.

The optional second number is the frequency in Rydbergs where f_{ν} is specified; the default is 1 Ryd, and in the example above the continuum is specified at $0.1824 \text{ Ryd} = 5000\text{\AA}$. The frequency can be any within the energy band considered by the code, presently 1.001×10^{-5} Ryd to 7.354×10^{6} Ryd. If the energy is less than or equal to zero, it is interpreted as the log of the energy in Rydbergs, and the linear energy if positive.

It may or may not be necessary to specify a starting radius, depending on whether the luminosity or flux is specified.

4.4.8 phi(h) = 12.867 [range ...]

This command is used to specify $\phi(H)$, the log of the surface flux of hydrogen-ionizing photons (cm⁻² s⁻¹) striking the inner face of the cloud. It is defined as

$$\phi(H) \equiv \frac{Q(H)}{4\pi r_{inner}^2} \equiv \frac{R_{star}^2}{r_{inner}^2} \int_{\nu_1}^{\nu_2} \frac{\pi F_{\nu}}{h\nu} \, d\nu \,\,, \tag{8}$$

as in Ferland, Netzer, and Shields (1979), and is proportional to the optical depth in excited lines, such as the Balmer lines. The RANGE option can be used to change the default energy range in equation 8.

The inner radius need not be specified if this command is used since this command specifies the photon flux (i.e., per unit area).

4.4.9 Q(H) = 56.789 [range ...]

The log of the total number of ionizing photons emitted by the central object (with units s^{-1}) can be specified rather than the luminosity;

$$Q(H) = 4\pi R_{star}^2 \int_{\nu_1}^{\nu_2} \frac{\pi F_{\nu}}{h\nu} d\nu$$
(9)

where the default value for ν_1 is 1 Ryd, and the default value for ν_2 is the high energy limit to the code, presently 7.354×10^6 Ryd. The RANGE option can be used to change the energy bounds ν_1 and ν_2 . The photon flux (per unit area of cloud surface) can be specified with the "PHI(H)" command, described above.

It is necessary to specify a starting radius if this command is used.

4.5 Continuum Shape

The continuum should be specified between an energy of 1.001×10^{-5} Ryd ($\lambda \simeq 1$ cm; the low-energy continuum is important for Compton cooling, photoionization from excited states of hydrogen and helium, free-free heating, H⁻ heating, and grain heating) and 100 MeV $\simeq 7.354 \times 10^{6}$ Ryd (where the Klein-Nishina electron-scattering cross section is small, pair production is a competitive heating and opacity source, and the hard continuum is usually well rolled-over). CLOUDY will complain, but compute the model if possible, if the continuum is not specified over the full energy range. An intensity of zero will be assumed for missing portions of the continuum.

4.5.1 background, z=1.825, [f=100; no fireball]

This command will specify a continuum shape and intensity chosen to mimic the cosmic radio-X-ray background, as described by Ostriker and Ikeuchi (1983) and Ikeuchi and Ostriker (1986). Their ultraviolet continuum shape is a $\alpha = -1$ power-law, with a mean intensity J_{ν} at 912Å given by

$$4\pi J_{v}(912\mathring{A},z) = 4\pi \times 10^{-21} \left\{\frac{1+z}{3.5}\right\}^{4} f \ erg \ Hz^{-1} \ cm^{-2} \ s^{-1}$$
(10)

where z is the redshift and f the an optional scale factor entered as the second parameter. Its default value is f = 1, and z = 0 (i.e., now) is assumed if no redshift is entered. Judging from Bechtold et al. (1987) and Bajtlik, Duncan, and Ostriker (1988), f is within a factor of 10 of unity. This command specifies *both* the shape and intensity of the continuum.

Primordial fireball radiation is included in the generated background. This radiation field is assumed to be a blackbody radiation field, in strict thermodynamic equilibrium, with temperature given by

$$T_{fireball} = 2.756 \,(1+z)^{\,o} K \tag{11}$$

where the redshift dependence is from Peebles (1971) and the present temperature of the background is assumed to be $T_{fireball} = 2.756 \pm 0.016$ K (Wilkinson 1987). This background can be an important source of Compton cooling for low density clouds. If the optional keyword "NO FIREBALL" appears on the line then the background due to the primordial fireball radiation will not be included.

Thermal background radiation can also be specified independently with the "FIREBALL" command, described below.

If a starting radius is not specified, then a value of 10^{25} cm will be assumed. Some objects, such as Ly α forest clouds, may be very large. Note that for the geometry to be plane parallel it is necessary to make sure that $\delta r/r \ll 1$ (if $\delta r/r \ge 1$ then the incident continuum will be attenuated by the r^{-2} geometric factor). It may be necessary to specify a larger starting radius in some circumstances.

4.5.2 blackbody t=100,000 [linear;luminosity;radius;density; lte]

The continuum will be a blackbody with temperature given by the input number, the temperature in degrees Kelvin. The temperature may be entered directly, or as a log. The number is assumed to be a log if it is less than or equal to 10 and linear if greater than 10. (As a result, temperatures less than or equal to 10K are entered as logs, i.e., 5K = 0.69897, 10K = 1). Temperatures lower than 10K will be interpreted as the linear quantity rather than as a log if the keyword "LINEAR" appears. Embedded commas can improve readability, such as

black body, Temp=1,000,000K

which is equivalent to

black body t=6

Blackbody luminosity options. The luminosity of the black body can also be specified with options which may occur on this command line. (This option was added by P.G. Martin.) If the luminosity is specified with any of these options, then it must not also be specified with another luminosity command for this continuum source. The keywords which can appear on the line are as follows:

blackbody 5, luminosity = 38 If the keyword "LUMINOSITY" appears then the second number is the log of the *total* luminosity (erg s⁻¹) of the black body, $4\pi R_{star}^2 \sigma T_{eff}^4$. This example would be a 10⁵ K planetary nebula nucleus at the Eddington limit.

blackbody 5, radius = 10 The log of the radius of the blackbody R_{star} (in cm) is used to set the total luminosity when the keyword "RADIUS" appears. The total luminosity is $4\pi R_{star}^2 \sigma T_{eff}^4$. This example is also typical of a planetary nebula nucleus.

blackbody 50,000K, energy density = 500K The energy density of the blackbody radiation field, expressed as the equivalent blackbody temperature T_u in degrees K, is used to set the luminosity when the "ENERGY DENSITY" keyword appears anywhere on the line. The energy density temperature is defined from Stefan's law and the actual energy density of the radiation field u (erg cm⁻³):

$$T_u \equiv \left(\frac{u}{a}\right)^{1/4} \tag{12}$$

where a is the Stefan's radiation density constant.

The second number is assumed to be a log if it is less than or equal to 10 and linear otherwise. Numbers smaller than 10K will be interpreted as the linear temperature rather than as a log if the keyword "LINEAR" appears. (Note that if the linear option is used, then the blackbody temperature must also be linear since the key triggers both.) Note also that microwave background radiation should also be included if $T_u \leq 2.8$ K. CLOUDY will complain, but compute the model, if the energy density of the incident continuum corresponds to a temperature less than the present energy density temperature of the universe.

blackbody, t=50,000K, _lte The keyword "_LTE" (note the leading space) with no second number is equivalent to the "ENERGY DENSITY" option with T_u set to the color temperature of the radiation field. This is a quick way to check that ionization and level populations go to LTE in the high radiation field limit. (This corresponds to strict thermodynamic equilibrium, not LTE, of course.)

blackbody, t=100,000 K, dilution factor = -14 Here the second parameter is the dilution factor W, defined as

$$W \equiv \frac{J_{\nu}}{B_{\nu}} \approx \frac{\pi R_{star}^2}{4\pi R_{inner}^2} \tag{13}$$

where R_{star} is the radius of the star and R_{inner} is the separation between the illuminated face of the cloud and the center of the star. The approximation on the RHS assumes that $R_{star} \ll R_{inner}$. The dilution factor can be entered either directly or as a log (if the latter, then it will be negative). The example above is a rough approximation of the radiation field within a typical planetary nebula.

Starting radius If the radiation field is normalized by specifying the equivalent energy density T_u , either explicitly or with the "_LTE" option, or by setting a dilution factor, then it is not necessary to also specify the starting radius since the intensity of the incident continuum is uniquely determined. An inner radius of 10^{25} cm will be assumed if the inner radius is not set; this usually will result in a plane parallel geometry. It *is* necessary to set a starting radius for the luminosity or radius options, however, since these specify luminosity and not intensity.

4.5.3 bremsstrahlung, temp = 8

The continuum will be (approximately) characteristic of optically thin hydrogen bremsstrahlung emission. The assumed form is given by;

$$f_{\nu} \propto \nu^{-0.2} \exp(-h\nu/kT)$$
 . (14)

The temperature may be entered directly, or as a log. In this example the temperature would be 10^8 K. The argument is assumed to be the log of the temperature if it is less than or equal to 10, and linear otherwise. The form of the continuum is only approximate since a simple power-law gaunt factor is assumed, and the emission from an optically thin gas with cosmic abundances is actually characterized by hundreds of overlapping emission lines (see, for example, Kato 1976).

4.5.4 extinguish column dens=23, leak=0.05, low=4 Ryd

After the continuum has been fully generated and normalized to the correct intensity, this command will modify the shape by extinguishing ionizing energies by photoelectric absorption by a cold neutral slab with column density N f dr (cm⁻²) given by the first argument (entered as a log; f is the filling factor). The form of the extinction is a simple single power-law fit to the absorption curves calculated by Cruddace et al. (1974);

$$f'_{\nu}(\nu \ge 1 \ Ryd) = f_{\nu} \left\{ \eta + (1 - \eta) \exp\left(6.22 \times 10^{-18} \nu_{Ryd}^{-2.43} N', f \ dr\right) \right\}$$
(15)

where f_{ν} and f'_{ν} are the incident and attenuated continua, Nf dr is the column density, ν_{Ryd} is the frequency in Rydbergs, and η is the leakage. The non-ionizing $(h\nu < 1 \text{ Ryd})$ continuum is not extinguished by this command.

The second optional number is the fractional leakage through the absorber η (see Ferland and Mushotzky 1982), which has a default value of 10^{-4} . This second number is interpreted as a log if it is negative and linear otherwise. A warning is printed if the leakage is zero, since it is possible that there will be no ionizing radiation in this case. If temperature failures occur or the solutions seem unphysical when the "EXTINGUISH" command is given then it is likely that nearly all ionizing radiation has been attenuated. A plot of the generated continuum (with the "PLOT CONTINUUM" command) may prove interesting.

The third optional number is the lowest energy for the absorption to occur. It must be greater than 1 Ryd (the default) and is entered as linear Rydbergs. The continuum with energies below this will be unaffected by the absorption. The optional arguments may be omitted from right to left.

The command acts by first generating the continuum shape, neglecting extinction. The continuum is then normalized using any of the luminosity commands (i.e., "Q(H)", "IONIZATION PARAMETER", "LUMINOSITY", etc.), then the continuum is extinguished. The continuum which actually strikes the illuminated face of the cloud does not have the ionization parameter or luminosity actually entered. (These values would be correct were the extinction not present.) Physically, the luminosity of the central object is not changed by the presence of an absorbing cloud along the line of sight.

4.5.5 fireball [redshift = 2000]

This command generates a blackbody radiation field in strict thermodynamic equilibrium (i.e., $T_{color} = T_u$, where u is the energy density). The optional argument is the redshift z; if it is not entered then z = 0 is assumed. The temperature of the blackbody is given by

$$T_{fireball} = 2.756 \,(1+z)^{\,o} K \tag{16}$$

where the redshift dependence is from Peebles (1971) and the present temperature of the background is assumed to be $T_{fireball} = 2.756 \pm 0.016$ K (Wilkinson (1987). This command specifies *both* the shape and intensity of the radiation field. A starting radius of 10^{25} cm will be assumed if no starting radius is specified.

4.5.6 interpolate [$\nu(Ryd)$ or log $\nu(hz)$], log(f_{ν})

Under most circumstances the continuum will actually be entered as a table of points. CLOUDY interpolates upon this table using straight lines in log-log space. Up to 100 ordered pairs of points can be entered, with "CONTINUE" lines used to continue entering values after the initial "INTERPOLATE" line is filled. The first of each pair of points is *either* the energy in Rydbergs (either linear or as a log) *or* the log of the

frequency (in Hertz); the second number of each pair is the log of the relative flux density per unit energy interval (f_{ν}) at that energy. CLOUDY assumes that the log of the energy in Rydbergs was entered if the first number is negative; that the log of the frequency was entered if the first number is greater than 5; and linear Rydbergs otherwise. Any of the three styles can be chosen, but must be used consistently within the command. If the first energy is entered as zero then it is interpreted as the low energy limit of the code. In this case the remaining energies will be interpreted as linear Rydbergs if the second number is positive, and the log of the energies in Rydbergs if negative. An energy of zero Ryd is not allowed (except for the first), and the energies must be in increasing order. The luminosity of the continuum is then set by any one of the luminosity commands.

The INTERPOLATE command can be freely mixed with other continuum shape commands, and a total of up to 10 INTERPOLATE and TABLE (see below) commands can be entered.³ Note that "TABLE" and "INTERPOLATE" are actually two forms of the same command. The total number of "TABLE" and "INTERPOLATE" commands entered together cannot exceed 10, the current value of the variable LIMSPC, which occurs in parameter statements throughout the code.

As an example, the following approximates a metal-poor 45,000K stellar atmosphere; the energies are entered in Rydbergs:

```
* following is 45000k atmosphere from Shields and Searle
interpolate (0.00001 -11.106) (.58 -1.5792) (.99 -1.44) (1.01 -1.7018)
continue (1.8 -1.905) (1.81 -1.939) (2.57 -2.208) (2.59 -2.247)
continue (3 -2.3994) (3.02 -2.8193) (3.49 -2.9342) (3.51 -4.143)
continue (3.99 -5.582) (4.01 -6.3213) (6 -9.9) (10 -17.3) (20 -30)
continue (10,000,000 -30)
q(h) = 52.778151
```

Note that the continuum should be specified between 1.001×10^{-5} Ryd and 7.354×10^{6} Ryd even if the intensity is small; if it is not fully specified then a warning will be issued and a model computed with the unspecified continuum set to zero intensity, if this is possible. As a further note, it is important that the continuum be physically correct. For instance, stellar model atmospheres emit almost no X-rays, while real OB stars *are* X-ray sources (although neglecting X-rays for these stars is generally a safe approximation).

CLOUDY will stop if more than 100 frequency points are entered. The maximum number of frequency points allowed is set by the variable NTERP which occurs in several PARAMETER statements throughout the code. NTERP is presently 100. If

 $^{^{3}\}mathrm{Limits}$ to the use of the INTERPOLATE command existed in versions 73 and before, but have been lifted.

more points are needed then NTERP should be increased everywhere this parameter occurs in the code.

4.5.7 laser, frequency = 3.5Ryd

The intensity of the continuum will be very small, except within $\pm 5\%$ of the specified energy, where it will be very large.⁴ The energy is specified in Rydbergs, and it is interpreted as a log if it is negative. This is a useful way to check on the computation of the photoionization rate integrals.

4.5.8 power law, slope=-1.4 [high cut=60 Ryd [low cut=.001]]

N.B. IT IS VERY DANGEROUS TO USE THIS COMMAND. The continuum will be a power-law, with optional low and high energy exponential cutoffs, parameterized by the cut-off frequencies $\nu_{high \ cut}$ and $\nu_{low \ cut}$, expressed in Rydbergs. The form of the continuum is

$$f_{\nu} = \nu^{+\alpha} \exp(-\nu/\nu_{high\ cut}) \exp(-\nu_{low\ cut}/\nu)$$
 . (17)

The first number on the command line is the slope α . Note that there is no implicit negative sign in this exponent; typical AGN have $\alpha_{ox} \sim -1.4$, (Zamorani et al. 1981). The second (optional) number is the high energy cutoff $\nu_{high\ cut}$ expressed in Rydbergs. The default value of $\nu_{high\ cut}$ is 10^{10} Ryd $\sim 10^{11}$ eV. The third optional number is the low energy cutoff $\nu_{low\ cut}$; the default value is 0 eV.

It is generally a very bad idea to use this command. CLOUDY treats the entire continuum between very low and very high energies. Extrapolating "reasonable" continua past the optical-ultraviolet region into microwave or γ -ray energies will have unexpected effects. Power law continua with slopes smaller than -1 will have unphysically large photon occupation numbers and brightness temperatures at very low energies, probably producing catastrophic Compton cooling and free-free heating. Continua with slopes greater than -1 will be dominated by the radiation field at energies of many MeV, resulting in large Compton heating and pair production rates. A further problem is that the exponential cutoffs can drive the continuum to zero intensity when either argument in the exponential becomes large. This is unphysical, and can cause numerical problems.

It is *much* better to use the "'INTERPOLATE"' command, and enter physically reasonable low and high energy continua. There is a special version of the command, "TABLE POWER LAW" (see below) for entering a well behaved $f_{\nu} \propto \nu^{-1}$ power law continuum.

⁴The luminosity normalization for this command was not exact before version 74.

$\nu(\mathrm{Ryd})$	$\log(F_{\nu})$	slope
1.00(-5)	-3.388	+2.50
9.12(-3)	4.0115	-1.00
0.206	2.6576	-0.50
1.743	2.194	-1.00
4.130	1.819	-3.00
26.84	-0.6192	-0.70
7.35(+3)	-2.326	-1.67
7.40(+6)	-7.34	

Table 2: AGN Continuum

4.5.9 table, [agn, akn120, ...]

Any of several default continuum shapes, which are stored as a permanent part of the code in BLOCK DATA SCALAR, can be entered with this command. This is a special version of the "INTERPOLATE" command, described above. The same interpolation on a table of input frequencies and fluxes described there is done when this command is entered. The TABLE command can be freely mixed with other shape commands, and a total of up to ten TABLE and INTERPOLATE commands can be entered.

table_agn If the keyword "_AGN" appears (note the presence of a leading space), then a continuum similar to that deduced by Mathews and Ferland (1987) will be used. The continuum is meant to be similar to "typical" radio quiet active galaxies. The points used to describe this continuum are given in Table 2. This continuum differs from the Mathews and Ferland (1987) continuum only in that the continuum is assumed to have a sub-millimeter break at 10 microns. For wavelengths longer than 100μ m the continuum is assumed to have a slope $f_{\nu} \sim \nu^{+2.5}$, appropriate for a self-absorbed synchrotron continuum (Rybicki and Lightman 1979). Note that this is the observed continuum, and may not be directly related to the continuum actually striking BLR gas.

The energy of the sub-millimeter break is not well determined observationally, but has a major impact on certain models, as discussed by Ferland and Persson (1989). The energy of the break can be adjusted with the "BREAK" keyword. The break can be adjusted between the limits of 0.2 Rydberg and 1.001×10^{-5} Ryd by entering the keyword "BREAK", followed by a number specifying the energy of the break. The number is interpreted as the log of the energy in Rydbergs if it is negative, as linear Rydbergs if positive, and as the (linear) wavelength of the break in microns if a second keyword "MICRONS" appears. If no number appears, but the keywords "NO BREAK" does, then a break at an energy of 1.001×10^{-5} Ryd is assumed. The

$ u(\mathrm{Ryd}) $	$\log(F_{\nu})$	slope
1.00(-5)	-5.	+2.50
9.115(-3)	-0.5604	-1.00
3676.	-6.166	-2.
7.40(+6)	-12.77	

Table 3: Power Law Continuum

following shows equivalent ways of generating a continuum with a break at 10 microns;

table agn break .00912 ; energy in Ryd table agn break -2.04 ; log of energy in Ryd table agn break 10 microns ; wavelength in microns table agn no break ; no sub-millimeter break

Note that the nature of the continuum in AGN is still an open question. The continuum given here is very simplistic, and quite uncertain in the ionizing ultraviolet. Recent work suggests this continuum may not be correct for low redshift Seyfert galaxies (Binette et al. 1989; Clavel and Santos-Lleo 1990).

table power law [spectral index -1.4, low=.01, hi=20] This option produces a power law continuum which is well-behaved at both the high and low energy ends. The default condition (when no numbers occur on the input line) is for the form $f_{\nu} \propto \nu^{\alpha}$ with $\alpha = -1$ between 10 microns and 50 keV, and has slopes $\alpha = \nu^{5/2}$ at lower energy, and $\alpha = \nu^{-2}$ at higher energies. The spectral mid-range spectral index (for the region from 10 microns to 50 keV) has a default of $\alpha = -1$. Table 3 summarizes the default continuum.

Three optional numbers may appear on the command line. The first number sets the slope of the mid-range spectral component (infrared to X-ray) and has a default of -1. Note that implicit negative signs are never used in CLOUDY. The second optional number is the energy (in Rydbergs) of the infrared break; the default is 10 microns. If this second number is zero then the low energy limit to the continuum $(1.001 \times 10^{-5}$ Ryd) will be used. The number is interpreted as the log of the energy in Rydbergs if it is negative, and linear otherwise. The third optional number is the energy of the break in the X-ray continuum. The default is 50 keV, and if it is zero then the high energy limit of the continuum $(7.354 \times 10^6 \text{ Ryd})$ is used. The number is interpreted as a log if the energy of the infrared break is entered as a log and linear otherwise. The numbers may be omitted from right to left.

$\nu(\mathrm{Ryd})$	f_{ν}
1.0(-5)	3.77E-21
5.2(-4)	1.38E-21
1.5(-3)	2.10E-21
0.11	4.92E-23
0.73	1.90 E- 23
7.3	2.24E-24
73.	6.42 E - 26
7.3(+3)	$4.02 \text{E}{-}28$
1.5(+6)	2.08E-31
7.4(+6)	1.66 E-32

Table 4: Crab Continuum

table crab If the keyword "CRAB" appears then the continuum summarized by Davidson and Fesen (1985) is generated. The luminosity of the continuum *is not* specified by this command. This is the net observed continuum, originating in both the pulsar and nebula, and not the pulsar continuum alone. The continuum is entered in the block data as the observed flux at Earth (erg cm⁻² s⁻¹ Hz⁻¹) and is given in Table 4.

According to Davidson and Fesen, the total luminosity of the Crab is $L_{tot} = 10^{38.14}$ erg s⁻¹, so the Crab continuum could be generated by the commands

luminosity (total) 38.14 table Crab

table akn120 If the keyword "AKN120" appears then the continuum summarized by Peterson et al. (in preparation) is used. This is the net continuum, as observed with a small beam, and may not be the continuum actually striking emitting gas. The continuum is described by the observed flux at Earth (erg cm⁻² s⁻¹ Hz⁻¹) and is given in Table 5.

According to Peterson the specific luminosity at 1320Å is $\nu L_{\nu} = 1.84 \times 10^{44} h^{-2}$ erg s⁻¹, where $h \equiv H_o/100 \text{ km s}^{-1} \text{ mpc}^{-1}$, so, setting h = 0.75, the AKN120 continuum could be generated by the commands

nuf(nu) = 44.514 at 0.6906 Ryd
table akn120

table star Kurucz; Mihalas Emergent continua from several stellar atmosphere calculations are also available. These are accessed with the keyword "STAR", followed

$\nu(\mathrm{Ryd})$	$f_{ u}$
1.0(-5)	1.5(-26)
1.9(-5)	1.6(-26)
3.0(-4)	1.4(-23)
2.4(-2)	8.0(-25)
0.15	1.6(-25)
0.30	1.8(-25)
0.76	7.1(-26)
2.0	7.9(-27)
76.	1.1(-28)
7.6(+2)	7.1(-30)
7.4(+6)	1.3(-34)

Table 5: Akn120 Continuum

Table 6: Mihalas (1972) Continua

Т.	$\log(g)$
30,000	4.0
$32,\!500$	4.0
$35,\!000$	4.0
37,500	4.0
40,000	4.0
$45,\!000$	4.0
$50,\!000$	4.0
$55,\!000$	4.0

by a sub-keyword ("Mihalas" or "Kurucz") to indicate which set of atmospheres is to be used. At present subsets of the Mihalas (1972) non-LTE OB stellar atmospheres and the Kurucz (1979; with supplements) line-blanketed LTE atmospheres are available. Both are static plane-parallel atmospheres. The parameters of the models now included are summarized in Tables 6 and 7. The temperature and author of the calculation (presently Kurucz or Mihalas) must be specified; these can be in any order.

Any temperature between the lowest and highest temperatures listed in the tables can be interpolated, but only the listed gravities and metalicities can be generated at present. If the specified temperature is within a tenth of a percent of one of the temperatures listed in Tables 6 or 7 then exactly the published continuum will be used, otherwise a linear interpolation in temperature — magnitude (Mihalas) or $\log(f_{\nu})$ (Kurucz) space will be done. Extrapolation is not performed; the temperature must be

Т.	$\log(g)$	[Z]	Reference
30,000) 4.0	0.0	Kurucz (1979)
35,000) 4.5	0.0	private communication
40,000) 4.5	0.0	private communication
45,000) 4.5	0.0	Kurucz (1979)
50,000) 4.5	0.0	Kurucz (1979)

Table 7: Kurucz (1979) Continua

between the lowest and highest values.

The following would roughly correspond to θ^1 C Ori, the ionizing star in the Orion Nebula;

table star Kurucz 39,000
q(h) 49 .

Note that these stellar atmospheres emit little energy above 4 Ryd, while real OB stars are actually X-ray sources. Sciortino et al. (1990) find a correlation the X-ray and bolometric luminosities which can be fitted by

$$\log L_x = 1.08 \left(+0.06 / -0.22 \right) \log L_{bol} - 9.38 \left(+2.32 / -0.83 \right), \tag{18}$$

i.e., the X-ray luminosity is typically 6.3 dex fainter than the bolometric luminosity. A source temperature of 0.5 kev is quoted by Sciortino et al. This X-ray continuum must be explicitly added as an independent continuum source. Tests show that the high energy light has little effect on conditions in the HII region, but *does* affect the ionization in the PDR.

table_ism [factor = 0.7] The local interstellar radiation field is generated with the keyword "_ISM". This uses Figure 2 of Black (1987) to represent the *unextinguished* local interstellar radiation field. This command specifies *both* the shape and luminosity of the radiation field. The continuum generated by CLOUDY is exactly that given by Black, except that the radiation field between 1 and 4 Ryd is interpolated from the observed/inferred values. Actually, it is thought that this part of the radiation field is heavily absorbed by gas in the ISM, so that little 1–4 Ryd radiation exists, at least in the galactic plane. Such absorption can be introduced with the "EXTINGUISH" command, described elsewhere. The TABLE ISM command also specifies the luminosity of the incident radiation field, since this is also directly observed. There is an optional parameter, specifying a scale factor for the intensity of the entire radiation field. It is the log of the scale factor if less than or equal to zero, and the scale factor

$\log(\nu)$	$\log(\nu f_{\nu})$	$\log(\nu)$	$\log(\nu f_{\nu})$
9.00	-7.93	14.14	-2.30
10.72	-2.96	14.38	-1.79
11.00	-2.47	14.63	-1.79
11.23	-2.09	14.93	-2.34
11.47	-2.11	15.08	-2.72
11.55	-2.34	15.36	-2.55
11.85	-3.66	15.54	-2.62
12.26	-2.72	16.25	-5.68
12.54	-2.45	17.09	-6.45
12.71	-2.57	18.00	-6.30
13.10	-3.85	23.00	-11.30
13.64	-3.34		

Table 8: Local Interstellar Radiation Field

itself if positive. The default is zero (i.e., Black's radiation field). The actual numbers used by CLOUDY to interpolate on Black's table are given in Table 8. The frequencies are in Hz, and the product νf_{ν} in erg cm⁻² s⁻¹.

The actual ISM radiation field incident on a typical region in the galactic plane would be generated by:

table ism extinguish by 22 .

table read [fortran unit 8] This command is used to read in the continuum predicted from previous calculations using CLOUDY. Here, the initial calculation is used to predict the continuum transmitted through a cloud. This command is then used in subsequent calculations, in which the transmitted continuum from the first calculation is to be included in the incident radiation field of the second calculation. The file containing the previously computed continuum must have been produced by the current version of CLOUDY by including the "PUNCH TRANSMITTED CONTINUUM" command in the initial calculation. This PUNCH command is described elsewhere, and produces a file containing the frequency (in Rydbergs) and the transmitted flux νf_{ν} . This continuum is the sum of the attenuated incident continuum and the fraction of the diffuse emission from the cloud which is emitted and transmitted in the outward direction.

This table can be freely mixed with all of the other continuum shape commands, but only one table can be read in using this command. If more than one "TABLE READ" command occurs, only the last will be honored. The default is for the file

4.6 Chemical Composition

Table 9: Solar Composition				
Atom	Solar	Old Solar		
Key	default	OSOLar		
He	0.098	0.10		
\mathbf{C}	3.63(-4)	4.7(-4)		
Ν	1.12(-4)	9.8(-5)		
0	8.51(-4)	8.3(-4)		
Ne	1.23(-4)	1.0(-4)		
Mg	3.80(-5)	4.2(-5)		
Al	2.95(-6)	2.7(-6)		
Si	3.55(-5)	4.3(-5)		
\mathbf{S}	1.62(-5)	1.7(-5)		
Ar	3.63(-6)	3.8(-6)		
Ca	2.29(-6)	2.3(-6)		
Fe	4.68(-5)	3.3(-5)		
grains?	no	no		

containing the continuum points to be FORTRAN I/O unit 7 (i.e., named "fort.7" on UNIX machines, or "assigned" with the ASSIGN NAME FOR007 statement on VMS machines). The I/O unit number is changed with the optional argument on the line.

When this command is used, punch output (using the "PUNCH" command) must not also be produced on the same Fortran I/O unit number; the input file will be overwritten if this occurs. The first two lines of the input file contain header information, and are skipped. They should not be deleted.

4.6 Chemical Composition

The composition will be "solar" (defined in Table 9; these are taken from Grevesse and Anders 1989) unless a different mixture is specified. Abundances are always specified by number relative to hydrogen, not by mass.

4.6.1 abundances he c n o ne mg al si s ar ca fe

The chemical composition is entered with a line beginning with the command "ABUNDANCES", followed by: a) a set of 12 abundances; b) a single number to set all of the abundances, or c) a second keyword to select one of several stored abundance sets. Abundances are always by number relative to the total hydrogen density (the sum of atomic, ionic, and molecular).

Arbitrary abundances. An arbitrary abundance set can be specified by entering all twelve abundances with the "ABUNDANCES" command. The elements must be in exactly the same order as indicated above, and all twelve abundances must be specified. Abundances of zero are not allowed; CLOUDY will stop. The code may crash due to floating point underflow, followed by division by zero, if an abundance is made too small (i.e., such that the volume number density (cm⁻³) of the element underflows to zero). The composition can be specified on several lines with "CONTINUE" lines following the initial "ABUNDANCES" line.

The best way to enter abundances is as the log of the abundance by number relative to hydrogen;

abundances he=-1 c=-4.3 n=-5 o=-2.3 ne=-1.2 mg=-8 al=-8 continue si=-8 s=-8 ar=-8 ca=-8 fe=-8 ; (deplete Fe, 3rd row).

The abundances can also be entered as a set of scale factors indicating the desired abundances relative to solar;

```
abundances he=1 c=1 n=10 o=1 ne=1.2 mg=1 al=.93
continue si=1 s=1 ar=1 ca=1 fe=0.00001 ; (deplete iron)
```

In general it is better to use the first style since the default solar composition changes from time to time. The code decides which type is used by checking the sign of each number. The numbers are interpreted as linear scale factors relative to solar if *all* are positive, and as logs of the abundance relative to hydrogen if *any* are negative. Be sure to check the abundances listed in the header to confirm that the composition has been entered correctly.

Setting all at once. If exactly one number is entered on the "ABUNDANCES" line then all of the elements heavier than hydrogen are given this abundance; the number can be either the relative abundance or its log. The number will be interpreted as a log if it is less than or equal to zero, and as the abundance if positive. Either of the following commands will give all elements between and including helium and iron an abundance of 10^{-10} by number relative to hydrogen:

abundances -10 abundances 0.000,000,000,1

This is useful for debugging the hydrogen atom. The "METALS" command, described below, is useful for changing abundances of all elements heavier than helium.

			ncu nbu			
Atom	H II Region	Planetary	Nova	Cameron	Primordial	NLR
key	HII, H II	PLANetary	NOVA	CAMEron	PRIMordial	_NLR
He	0.095	0.10	0.10	0.0677	0.072	0.10
С	3(-4)	7.8(-4)	9.4(-3)	4.22(-4)	1.0(-10)	5.0(-4)
Ν	7(-5)	1.8(-4)	9.8(-3)	8.72(-5)	1.0(-10)	1.1(-4)
0	4(-4)	4.4(-4)	1.7(-2)	6.93(-4)	1.0(-10)	7.9(-4)
Ne	1.1(-4)	1.1(-4)	2.0(-3)	9.77(-5)	1.0(-10)	9.5(-5)
Mg	3(-6)	1.6(-7)	4.2(-5)	3.98(-5)	1.0(-10)	4.0(-5)
Al	2(-7)	2.7(-7)	2.7(-6)	3.20(-6)	1.0(-10)	1.0(-7)
Si	3(-6)	1.0(-5)	4.3(-5)	3.76(-5)	1.0(-10)	1.0(-7)
\mathbf{S}	1(-5)	1.0(-5)	1.7(-5)	1.88(-5)	1.0(-10)	2.2(-5)
Ar	3(-6)	2.7(-6)	3.8(-6)	3.99(-6)	1.0(-10)	4.9(-6)
Ca	2(-8)	1.2(-8)	2.3(-6)	2.35(-6)	1.0(-10)	1.0(-7)
Fe	3(-6)	5.0(-7)	3.3(-5)	3.38(-5)	1.0(-10)	1.0(-7)
grains?	Orion	PN	no	no	no	Orion

Table 10: Stored Abundance Sets

Stored abundance sets. Table 10 lists the abundance sets which are stored as a permanent part of the code. These sets are entered if there are no numbers on the line, but a keyword occurs, as in the following examples. The four character part of the keyword which must be matched for the key to be recognized is capitalized in the table.

```
abundances Cameron
abundances hii region [no grains]
abundances h ii region [no grains]
abundances nova
abundances planetary nebula [no grains]
abundances primordial
abundances NLR
```

The assumed abundances are from a variety of sources, and their present values are given in Table 10, by number relative to hydrogen. The default "solar" abundance used pre-1990 (Table 9) can be entered by using the "OSOLAR" keyword.

"CAMERON" abundances are from Cameron (1982; note that the helium abundance is *very* low, either it or the Big Bang is wrong). The "HII region" abundances are a subjective mean of the Orion Nebula abundances determined by Baldwin et al. (1991), Rubin et al. (1991), and Osterbrock et al. (1991).

Some mixtures have certain elements, especially Si, Ca, Al, Mg, and Fe in H II regions and planetary nebulae, with gas-phase compositions reduced by depletion onto

grains. Specifying "H II REGION", "_NLR", or "PLANETARY NEBULA" will invoke grains and the mixtures given in Table 10. Grains set in this manner will have the properties appropriate for the type of grains indicated (see bottom line of the Table, and the section on grains, 21 below). Grains can also be specified separately with the "GRAINS" command. If grains are set by both the "GRAINS" and "ABUNDANCE" commands then the parameters set by the "GRAINS" command are used.

In some circumstances, it is interesting to explore the effects of grain-free mixtures, with the opacity/thermal effects of the grains suppressed, but with the (depleted) gas-phase abundances unchanged. The optional keyword "NO GRAINS" can be placed in the "ABUNDANCES" line. In this case grains will not be included in the calculation, but the observed (depleted) gas-phase abundances will still be used.⁵

4.6.2 metals 0.05 [log, linear]

This command multiplies the entire mixture of metals (elements heavier than helium) by the scale factor entered on the line. This is useful when the effects of global enrichments or depletions are to be investigated. If the number is zero or negative then it is assumed to be the log of the number; if positive then a linear scale factor. If the "LINEAR" keyword appears then the number is interpreted as linear (unless negative). If the "LOG" keyword appears then the number is interpreted as the log of the metal abundance, no matter what sign the number has.

Combinations such as

```
abundances planetary nebula
metals 3
```

```
or
```

```
metals 3
abundances planetary nebula
```

would multiply the planetary nebula gas phase mixture by three,⁶ while

metals -10

would multiply the default solar mixture by 10^{-10} .

The depletion factor is stored as the variable DMETAL, in the common block of the same name. The default is unity. The "METALS" command has no effect on the grain abundance. Physically, the two should scale together in some manner.

 $^{^5 \}mathrm{In}$ versions 77 and before, the abundances of depleted elements were set to solar values when "no grains" was set.

⁶Limits to the ordering of the ABUNDANCES and METALS commands existed before version 72 but have been lifted.

4.7 Density Laws

Several commands specify the run of hydrogen density with radius. The default condition is constant density, with the total hydrogen density (atomic, ionic, and molecular) given by the command "HDEN". Power law and sinusoidal density distributions, as well as constant gas pressure, constant total (gas and radiation) pressure models, or an arbitrary density law, can also be computed.

4.7.1 constant density, pressure, gas pressure

This command has several optional keywords, depending on what is to be held constant. These are described next.

4.7.2 constant density

This is the default. The hydrogen density, the sum

$$HDEN \equiv N(H^{\circ}) + N(H^{+}) + N(H^{-}) + 2N(H_{2}) + 2N(H_{2}^{+}) + 3N(H_{3}^{+}), \qquad (19)$$

is kept constant. This is not quite an isochoric density law because the total particle density is not constant. This is because the electron and molecular fraction varies with the run of ionization. I prefer this type of model because the homology relations with the ionization parameter (Davidson 1977) are preserved. The hydrogen nucleon density is set with the "HDEN" command, which has as an option a power-law dependence on radius.

4.7.3 constant gas pressure [index=-1]

An isobaric density law is specified with this command. The gas pressure

$$P_{gas} = N_{tot} \, k \, T_e \quad , \tag{20}$$

where N_{tot} is the total particle density, is kept constant. This type of model is trendy today in active nuclei, but not really warranted since the ionizing continuum is seldom constant over the sound travel time across a typical cloud. (The latter is several months for "standard" BLR clouds, and constant pressure is really only approached after conditions have been stable for several sound travel times.) The optional index α will force the pressure to change as a power-law of the radius;

$$P_{gas}(r) = P_o \left(\frac{r}{r_o}\right)^{\alpha} \tag{21}$$

where P_o is the pressure at the inner radius.

The results of this command are not exact; the actual gas pressure will vary from zone to zone with an rms scatter of typically 0.7 percent.

4.7.4 constant pressure [no continuum]

If you are holding the pressure constant, you really should hold the total pressure, particle and radiation, constant. This option turns on the physics discussed by Ferland and Elitzur (1984), and Elitzur and Ferland (1986).

The pressure is the *total* pressure, the sum of the gas and radiation pressure;

$$P(r) = P(r_o) + \int a_{rad} \rho \, dr = P_{gas} + P_{lines} \tag{22}$$

where a_{rad} is the radiative acceleration due to the incident continuum (see equation 176) and ρ is the density (gm cm⁻³). This pressure law includes thermal gas pressure (P_{gas}), the nearly isotropic pressure due to trapped emission lines (P_{lines}), and the outward force due to the attenuation of the incident radiation field (the integral; this can be turned off by specifying the "no continuum" option on the command line).

CLOUDY will stop if the internal line radiation pressure builds up to more than half of the total pressure, since such clouds would be unstable unless they are self-gravitating. It is necessary to do at least a second iteration when radiation pressure is important since the total line optical depths must be known to compute line widths, escape probabilities, and level populations, reliably. If more than one iteration is to be done then the radiation pressure will not be allowed to exceed the gas pressure on any except the last iteration.

The results of this command are not exact; the actual total pressure will vary from zone to zone with an rms scatter of typically 0.7 percent. It is not possible to specify the optional power-law index for this pressure law.

4.7.5 dlaw p1, p2, p4 ... p10

An arbitrary density law, specified by the user, is used. There are up to ten parameters, which are stored as a vector in the common block "DLAW". A new function "FUNCTION FABDEN(R1)" must be provided, and the version of FABDEN already in CLOUDY must be deleted. The code will stop if the initial version of FABDEN is not replaced. The argument is the radius in centimeters, and the function returns the hydrogen density (cm⁻³). The code provided in the function must use the ten or fewer parameters in COMMON/DLAW/ DLAW(10) to compute the density at R1. Both the vector DLAW and argument to the function are double precision, although the function value is single precision.

Note that it is not consistent to specify the density with both this command and others, such as "HDEN", "CONSTANT PRESSURE", etc. There is no telling what will happen if this is done.

4.7.6 fluctuations log(period), log(max den), log(min den)

This command specifies a model in which the density varies as a sine wave. This is useful to check on the effects of inhomogeneities upon the emission-line spectrum. The first number is the log of the period of the sine wave, in centimeters. The second two numbers are the logs of the largest and smallest hydrogen densities over the sine wave. (See Mihalszki and Ferland 1983).

4.7.7 globule [density=2, radius=16, power=3]

The density law will be appropriate for a power-law density gradient, irradiated from the outside. The total hydrogen density N(r) is given by

$$N(r) = N_o \left(\frac{R}{R - \delta r}\right)^{\alpha} \tag{23}$$

where N_o is the background density outside the cloud, with default value 1 cm⁻³, and δr is the depth into the cloud, measured from the illuminated face. The log of N_o is the optional first number on the command line. R is the radius of the cloud, and has a default of one parsec, $R = 3.086 \times 10^{18}$ cm. Other radii are specified by the optional second parameter, which must be entered as a log, in cm. The optional third argument is the index α , which has the default $\alpha = 2$. The arguments can be omitted from right to left.

4.7.8 hden = 5.6, [proportional to R - 2, ...]

Hydrogen density The first number is the log of the total (ionic, atomic, and molecular) hydrogen density. This is the sum

$$HDEN = N(H^{\circ}) + N(H^{+}) + N(H^{-}) + 2N(H_{2}) + 2N(H_{2}^{+}) + 3N(H_{3}^{+}) \ cm^{-3}.$$
 (24)

If the optional keyword "LINEAR" appears the number is the density itself and not its log.

For situations where the hydrogen atom is close to LTE and the gas is hot, there is a problem in defining the neutral hydrogen density because of the well-known divergence of the partition function, as discussed, for instance, by Mihalas (1978). To avoid this difficulty, the present version of CLOUDY defines the atomic hydrogen density as the total population in $n \leq 6$, while ionized hydrogen (which contributes to the free electron sum) includes all hydrogen atoms in $n \geq 7$ states. In most circumstances (i.e., $N_H \ll 10^{13} \text{ cm}^{-3}$ and $T \leq 10^4 \text{ K}$) the ambiguity is much less than 1%. **Power-law radial dependence** The second (optional) number is the exponent α for a radial density dependence, i.e.,

$$N(r) = N_o(r_o) \left(\frac{r}{r_o}\right)^{\alpha} \quad . \tag{25}$$

If the second number is -2, as in the example above, the density will be proportional to the inverse square of the distance to the central object, and spherical models will tend to have the same ionization parameter (and hence physical conditions) across the ionized zone.

For an inverse square law density dependence, there is a critical value of the number of ionizing photons emitted by the central object,

$$Q_{crit}(H) = \alpha_B(T_e) N_o^2 4\pi R_o^3 \quad , \tag{26}$$

where $\alpha_B(T_e)$ is the hydrogen case B recombination coefficient, and N_o and R_o are the inner density and radius respectively, such that an ionization front will not be present (and the model will extend to infinite radius) when $Q(H) \ge Q_{crit}(H)$. Generally, an ionization front will not be present if the density falls off faster than an inverse square law, but rather the level of ionization will tend to *increase* with radius. In either case, if a reasonable outer radius is not set, the calculation will extend to very large radii, an unphysically small density will result, and usually the code will crash due to floating point underflow, followed by division by zero. It is usually necessary to set an outer radius when the density falls off with an index $\alpha \le -2$, since, for most circumstances, the cloud will remain hot and ionized to infinite radius.

Power-law dependence on depth The density will depend on the depth into the cloud rather than the radius if both the optional exponent *and* the keyword "DEPTH" appears. The depth is the distance (in cm) between the point in question and the illuminated face of the cloud. Here the density is given by

$$N(r) = N_o(r_o) \left(1 + \frac{depth}{r_{scale}} \right)^{\alpha}$$
(27)

where r_{scale} is the scale depth. The scale depth is entered as the third number on line, and is the log of the depth in centimeters.

Power-law dependence on column density The density will depend on the column density if both the optional exponent *and* the keyword "COLUMN" appears. Here the density is given by

$$N(r) = N_o(r_o) \left(1 + \frac{col}{col_{scale}} \right)^{\alpha} \quad . \tag{28}$$

4.8 Geometry

where *col* is the column density from the illuminated face to the point in question, and col_{scale} is the scale column density. The scale column density is entered as the third number on line, and is the log of the column density (cm⁻²).

4.8 Geometry

The geometry is always spherical, but can be made effectively plane parallel by making the radius much greater than the thickness of the nebula. It is also possible to compute a model in which the emission-line region is almost a disk.

4.8.1 covering factor 0.3

This command sets a covering factor $\Omega/4\pi$ for the emission-line region. The argument is interpreted as the log of the covering factor if less than or equal to zero, and the covering factor itself if positive. It is impossible to specify a covering factor of zero. The covering factor can also be set as an optional argument on the "SPHERE" command.

The covering factor affects both the luminosity and the radiative transfer of lines and continua. If a covering factor is set and the line or continua are predicted as luminosities, then the luminosities will be for a shell covering Ω sr, where $\Omega/4\pi$ is the covering factor. The covering factor does not affect the line intensities, (the emission per unit area) if these are predicted rather than luminosity. This covering factor is referred to as the geometric covering factor, and is stored as the variable COVGEO in the common block COVER. A second covering factor, COVRT, affects the transfer of lines and continua. Both covering factors are set by the number on this command line.

If no covering factor is entered and SPHERE is not set then the default is for a geometric covering factor of unity (the shell fully covers the continuum source) but a radiative covering factor of zero (i.e., an open geometry).

4.8.2 cylinder log(semithickness)=9.12

The model will be spherical, but truncated so as to simulate a cylinder (See Ferland et al. 1982). The inner and outer radii of the cylinder are set by the "RADIUS" command described elsewhere in this section. This command sets the full height of the cylinder to twice the number entered on the command. The argument is the log of the semi-height in cm.

The effective volume element used to compute the emissivity is given by

$$dV = 4\pi r_{in}^2 \left(\frac{r}{r_{in}}\right) \left(\frac{\min(r, h_{cyl})}{r_{in}}\right) f(r) dr$$
(29)

where r_{in} is the inner radius, h_{cyl} is the cylinder half-height, and f(r) is the filling factor. The half-height h_{cyl} is stored as CYLIND, the sole element of the common block with the same name. The default value is $h_{cyl} = 10^{35}$ cm.

4.8.3 filling factor = 0.05 [index=-1]

The first number is the filling factor for a clumpy model. It can be either the filling factor itself (which is greater than zero and less than or equal to one) or the log of the filling factor (in which case it will be less than or equal to zero). The second number is optional, and is the index α for a power law variation of the filling factor $f(\mathbf{r})$, i.e.,

$$f(r) = f(r_o) \left(\frac{r}{r_o}\right)^{\alpha}$$
(30)

where $f(r_o)$ and r_o are the filling factor and inner radius of the cloud.

The filling factor is used in two ways; first to modify the volume emissivity of the cloud,

$$dI = 4\pi j f(r) dV \Omega/4\pi$$
(31)

where $\Omega/4\pi$ is the covering factor, and second to modify the optical depth scale

$$d\tau = \alpha_{lu} \left(N_l - N_u \frac{g_l}{g_u} \right) f(r) dr$$
(32)

(see Osterbrock and Flather 1959). Filling factors greater than unity are not allowed; CLOUDY will set a filling factor of unity if a value greater than one is entered.

4.8.4 radius $\log{r(inner)} [\log{r(out;dr); parsec; linear}]$

The first number is the log of the inner radius. The second number sets a stopping radius and is optional. This can be either the log of the outer radius (if it is larger than the first number) or the log of the thickness of the cloud (if it is less than or equal to the first number).

The numbers are normally interpreted as the log of the quantity. If the optional keyword "LINEAR" appears on the line then the numbers are interpreted as the numbers themselves and not their log. The default units are centimeters, but the arguments will be interpreted as the log of the radii in parsecs if the keyword "PARSECS" appears anywhere on the line. Arguments will be interpreted as linear parsecs if both keywords appear. The following gives examples of its use.

```
radius 19.5 ; log of inner radius in cm
radius 19.5 18.5 ; as above, but a thickness of approx 3x10^18 cm
```

```
radius 19.5 20 ; inner radius as above, outer radius 10^20 cm
radius 100 linear; inner radius of 100 cm
radius 0 parsecs ; log of radius in parses, so inner radius 1 pc
radius 1 to 3 linear parsecs ; inner radius 1pc, outer 3pc
```

The default value for the outer radius is effectively infinite (actually 10^{30} cm). If the "RADIUS" command is not entered and the surface flux or ionizing radiation field is set in some unambiguous manner (for instance, with the ionization parameter or energy density temperature), then a radius of 10^{25} cm will be set by default. Under most circumstances this radius will result in an effectively plane parallel geometry.

4.8.5 sphere [expanding ; static; covering factor=.4]

CLOUDY normally assumes that the gas covering factor is small, as is the case in the BLR of AGNs. The "SPHERE" command should be included if the covering factor of the gas is large and the model spherical. This command tells CLOUDY to take into account ionization by the diffuse emission in the H and He Lyman continua and He Ly α lines produced in the far side of the nebula (i.e., from beyond the central object), and not to attenuate the ionizing continuum by pure scattering opacities, such as electron scattering, backscattering by grains, or Rayleigh scattering.

This option should be set when the geometry is spherical and gas nearly fully covers the continuum source. It should not be set when the covering factor is small, and emission from a cloud is unlikely to encounter another cloud. This latter case is the default. In the language of Van Blerkom and Hummer (1967), "SPHERE" causes CLOUDY to assume the "symmetric case" (their equation 2.14), rather than the default "zero case" (their equation 2.13) for diffuse continua. Here these are referred to as "closed" and "open" geometries, respectively.

Two optional keywords "EXPANDING" and "STATIC" determine how line transfer is handled. If "EXPANDING" (the default when "SPHERE" is entered) is set then CLOUDY assumes that line photons escaping from the illuminated face of the cloud do not interact with absorbing material on the outer side. This is the case if the expansion velocity exceeds the Doppler-width by large amounts. If "STATIC"⁷ is set then line photons do interact on both sides, so that the escape probability at the illuminated face of the cloud is small for optically thick lines. It is necessary to iterate at lease one time when the "STATIC" option is used, since the total line optical depths are not known on the first iteration. The optical depths for all lines are determined self-consistently on second and further iterations. Ly α radiation pressure in the H⁺ zones will probably be significant if "SPHERE STATIC" is set.

⁷Sphere static did not work correctly in versions 74 and before.

The optional number on the line is the covering factor for the emission-line region. It is interpreted as the log of the covering factor if it is less than or equal to zero, and the covering factor itself if positive. The covering factor can also be set using the "COVERING FACTOR" command. The effects of the covering factor are described further below.

When a covering factor of unity is set the specific effects of SPHERE are; a) the total continuous optical depths are assumed to be twice the computed optical depths, and the initial optical depth is half the total, b) all diffuse reemission (bremsstrahlung, free-bound, etc.) is counted in the outward beam rather than only half, c) scattering opacities are not considered in the attenuation of the incident radiation field, d) when STATIC is set, the optical depth in Ly α in the inner direction is set to 10⁵ on the first iteration; otherwise it is 10⁻²⁰, and e) include ionization by HeI and HeII lines from the other side of the nebula. At the end of the iteration, all inward optical depths are set to half of the total value computed from the previous iteration. The diffuse continua are transferred using methods described in later sections.

4.8.6 wind v=300 km/sec [mass=1.4]

The model will be a large velocity gradient ($v \sim R$ Sobolev approximation) wind. The line widths and escape probabilities are modified in the appropriate manner, i.e., the effective optical depth is given by

$$\tau_{lu}(R) = \sigma_{lu} R \left(N_l - N_u \frac{g_l}{g_u} \right) \left(\frac{v_{thermal}}{v_{expansion}} \right)$$
(33)

where $v_{thermal}$ and $v_{expansion}$ are the thermal and expansion velocities respectively, and R is the radius.

The first parameter on the command line is the expansion velocity v_o at the inner edge of the cloud. It must be greater than zero, and is entered in km/sec. The density at the illuminated face of the cloud is entered with the "HDEN" command, and the density is varied across the model to conserve mass flux (i.e., the product $\rho(r) r^2 v(r)$ is kept constant). Because of this, a filling factor would not make physical sense and should not be used. The optional second parameter is the mass of the central star in solar units; its default value is one solar mass.

The equations of motion of the gas are solved. Acceleration due to the opacity of roughly ten absorption lines, the continuous opacity of the gas, and the gradient of the radiation pressure due to ~ 10 lines, and deceleration due to the gravity of the central object, are included. The calculation will stop if the gas comes to rest, or if any of the other stopping criteria are met. Further details are presented in a section below. Really, something like 10⁶ lines are needed for a realistic calculation (see, for example, Abbott 1982).

4.9 Optical Depths and Radiative Transfer

In some classes of nebulae, such as H II regions and planetary nebulae, line transfer is relatively unimportant. In other objects, such as nova shells and the broad-line region of active nuclei, excited states of hydrogen have significant populations and subordinate lines become optically thick (see Ferland and Netzer 1979; Weisheit et al 1981; Kwan and Krolik 1981; Canfield and Puetter 1980). The present version of CLOUDY treats line radiative transfer in the escape probability formalism (Hummer 1968; Hummer and Kunasz 1980; Elitzur 1982; Netzer, Elitzur, and Ferland 1985). Further details are given in section 15 below.

CLOUDY is fairly fast, so there is no reason not to iterate at least one time when line transfer is important. The default is for a single pass through the cloud, and this is often adequate for low-density nebulae such as planetary nebulae or H II regions. A second iteration is usually enough to establish a fairly accurate line optical depth scale for most transitions, so that the proper escape probabilities can be computed, when line transfer is important. If $Ly\alpha$ or $H\alpha$ optical depths change by more than ~ 20% on the last iteration then a warning that the model has not converged will be printed at the end of the last iteration.

Line radiation pressure cannot be computed accurately until the total line optical depths are known, so this quantity is meaningful only after at least one iteration. CLOUDY will stop if the radiation pressure exceeds half of the surface gas pressure in a constant pressure model, since such a geometry is unstable unless it is self-gravitating. On the initial iterations of a multi-iteration constant pressure model, the radiation pressure is constrained to never exceed half the gas pressure; this is to prevent the calculation from stopping when the optical depth scale is not yet well converged.

4.9.1 case b [tau ly alpha = 9;Hummer and Storey]

With no options, this command sets the inner optical depth for hydrogen and helium $Ly\alpha$ to 10^9 , so that even a one-zone model will be close to case B. The optional number is $log(\tau_{Ly\alpha})$, so it is possible to change this assumption. One-sided escape probabilities are used in this case, so the total escape probability is simply that for the inward direction. The "CASE B" command also suppresses optical depths in excited states, in keeping with the case B approximation. This is useful for checking the behavior of the hydrogen and helium atoms in the low density limit.

Normally, the treatment of the hydrogen and helium atoms includes all collisions between the ten levels considered for each atom/ion. Case B does not define the population of the ground or first excited state, so a true comparison with case B results should have collisions from these levels turned off. This is done with the "Hummer and Storey" option, to allow comparison with their 1987 paper. Collisions from the ground and first excited states *are* included if this second option is not specified. Collisions between $n \ge 3$ levels *are* always included unless the "HYDROGEN COLLISIONS OFF" command is given. Collisions between the 2s and 2p states are always included unless the "NO 2S2P" command is given.

4.9.2 diffuse fields on!off

This command turns Λ -iteration calculation of the diffuse fields off or on. If turned on, the diffuse fields are computed with the Λ -iteration method on second and latter iterations. This approximation is only formally correct when the model is plane parallel. This command has not been carefully debugged in the past few years, and should not be used except in experimental situations. A test case presented in the appendices shows that the approximations normally used by CLOUDY reproduces the Van Blerkom and Hummer (1967) exact results with great precision (much better than 1%, see 25 below).

N.B.; this command has not been carefully debugged in some time, and will soon be removed.

4.9.3 double optical depths

This command simulates a geometry in which ionizing radiation strikes the plane parallel cloud from both sides, such as a Ly α forest cloud. At the end of the iteration, the total line and continuum optical depths are set to twice the computed optical depth. The computed model is then one half of the cloud, and the other half of the cloud is assumed to be a mirror image of the first half. Doubling the total line and continuum optical depths at the end of the iteration is the *only* effect of this command. Physical quantities such as the dimension, column densities, or line emission *are not* affected.

These approximations only make sense if the cloud is optically thick in lines, but optically thin (or nearly so) in the continua. Lines such as the Ly α transitions of HeI and HeII can be important sources of ionizing radiation; their transport will be handled correctly in this limit when this command is used. Continuum transport out of the cloud will also be treated correctly, but attenuation of the incident continuum will *not* be if the cloud is optically thick in the continuum.

4.9.4 escape __K2; incomplete; [emit; destroy]

This command specifies how line escape probabilities are to be handled. One of the keywords "_K2" or "INCOmplete" must appear. If no other keywords appear then both the emission and destruction probabilities are set to either of the specified cases. If either keyword "EMIT" or "DESTroy" appear, then only the emission or destruction probability is changed.

Table 11: Grain Populations		
Index	Type	Property
1	graphite	ISM
2	silicate	ISM
3	graphite	Orion
4	silicate	Orion
5	silicate	0.01 micron
6	silicate	0.1 micron
7	silicate	Volk PN silicate

4.9.5 grains [-2; planetary; orion; no heating...]

The effects of grains can be included, either with this command, or by using an abundance mixture which includes grains by default. The "GRAINS" command takes precedence over the default grains set with the "ABUNDANCES" command.

The treatment of grains was developed in close collaboration with P.G. Martin. Details are provided in section 21 below, and in Baldwin et al. (1991). Seven populations of grains, summarized in Table 11, are presently incorporated in the code.

The temperature, potential, and drift velocity of the grains are determined using standard assumptions, as described, for instance, by Martin (1979) or Spitzer (1948; 1978), and section 21 below. Heating by direct absorption of the continuum, $Ly\alpha$, and all other lines and continua included in the OTS fields, and gas collisions, are included as heating mechanisms in the calculation of the grain temperature. Gas heating by grain photoionization, and cooling by free particle capture onto the grain surface, is also included. The grain potential is determined by solving the photoionization-recombination balance equation, and heating/cooling of the gas by grain photoionization-recombination is determined self-consistently.

The default condition for the code is no grains, and when grains are enabled the default grain mixture has ISM properties. The optional keyword "ORION" makes the grains more similar to the large-R grains in the Orion Nebula, which have a fairly grey ultraviolet extinction. The two grain populations marked Orion in Table 11 are used in this case. The keyword "PLANETARY" makes the grains more similar to those observed in planetary nebulae; the silicate population marked "PN" and ISM graphite are then used.

The abundances of the grain populations can be changed with the optional number on the command line. This is a scale factor used to multiply the stored grain opacities. The scale factor is the log of the opacity relative to the standard value if less than or equal to zero, and the scale factor itself if positive (i.e., both "GRAINS -2" and "GRAINS .01" would use ISM grains with each of the two constituents having only 1 percent of the standard abundance).

It is also possible to turn on each species independently. If two numbers occur on the line then the first is interpreted as the abundance, and the second is a pointer to the grain type. The other grain types are not turned off by this option, so it is possible to turn on several grain types with successive "GRAINS" commands.

The optional keyword "NO HEATING" turns off photoelectric heating of the gas by grain photoionization. The optional keyword "NO COOLING" turns off free particle recombination cooling of the gas by grain collisions.

The following are some examples;

```
*ism grains with ism abundance
grains
*orion grains with half their standard abundance
grains orion .5
*turn on ism graphite and orion silicate
grains abundance=1, type=1
grains abundance=1, type=4
*only include opacity effects of ism grains
grains no heating, no cooling
```

For a closed geometry, in which the SPHERE option is set, the predicted emission-line spectrum will be the *intrinsic* spectrum of the nebula. Photon destruction by all background opacity sources (including grains) is fully treated using escape probabilities (i.e., Hummer 1968), and the predicted intrinsic intensities include this physics. The intensities *do not* include the reddening effects of any external grains which lie outside the line-forming region, however. For an open geometry, the full intrinsic emission-line spectrum is again printed, following the predicted emergent line intensities. In this case the first set of lines is the observed spectrum, including absorption and scattering by grains, as observed from the illuminated face of the cloud.

In no case is the possible presence of large amounts of grains within cold neutral regions outside the computed structure taken into account.

4.9.6 helium collisions; radiation...

helium collisions off This turns off collisions within the helium singlets and helium ion.

4.9.7 hydrogen ; redistribution ; data

This allows some details of the treatment of the hydrogen atom to be changed. Unlike the vast majority of the commands, the entire keyword "HYDROGEN" must match for this command to be recognized.

hydrogen redistribution. Ly α transfer can be treated with either complete or incomplete redistribution (see, for example, Hummer 1962); the default is incomplete redistribution, and can be changed by entering

hydrogen redistribution complete hydrogen redistribution incomplete

There is at present a fundamental uncertainty in the computation of the line radiation pressure for transitions such as Ly α . For a simple two-level atom with incomplete redistribution, it has long been known that the line-width is proportional to $(a\tau)^{1/3}$ (Adams 1972, Harrington 1973; *a* is the damping constant). It is also easily shown that for complete redistribution and a frequency independent source function that the line width would be determined by inverting the Voigt function, and hence proportional to $(a\tau)^{1/2}$. This may be the case for Ly α in practice because of "line interlocking", whereby scattered Balmer line radiation broadens the upper level of Ly α (Hubbard and Puetter 1985), or when the density is high enough for distant collisions to broaden the line. The difference in radiation pressure and emergent flux is major (factors of several) for Ly α , which can easily have an optical depth of 10^7-10^9 , when Balmer lines are also optically thick. This command determines which approximation is used. The default condition is incomplete redistribution, which minimizes the line width and radiation pressure. This issue is discussed further in Elitzur and Ferland (1986).

hydrogen lowest temp 200 Normally the level populations are determined by solving the equations of statistical equilibrium using departure coefficients. These diverge at low temperatures when hydrogen is ionized, in which case fits to Martin's (1988) results are used. The lowest temperature considered by the 10-level hydrogen atom is machine dependent, and can be altered with this command. There is a single argument, and the number is interpreted as the log of the temperature if it is less than or equal to 10. The default value of the lowest temperature is 1000K. Tests show that numerical instabilities in the matrix inversion routine limit the lowest temperature to only slightly below the default value, even with 64 bit words. There is no lower limit to the temperature on a CRAY Y-MP when double precision is enabled on the compile step, so the lowest temperature can be made arbitrarily low.

hydrogen data ... The collision data set can be changed from the default, which uses quantal calculations where possible, supplemented by data from Vriens and Smeet (1980). The commands

hydrogen data Vriens and Smeet hydrogen data Johnson

will change between the Vriems and Smeets values and those of Johnson (1972). These collision cross sections differ by factors $\sim 2-3$ for *high-n* states; this is also, at present, a fundamental uncertainly, although the Vriems and Smeets data are based on more recent experimental results.

hydrogen collisions off Collisions within the hydrogen atom can be turned off with this command. All collisions except 2s-2p are turned off by this command. (These are turned off for H and He with the "NO 2S2P" command.)

hydrogen stimulated emission off Stimulated emission is turned off with this command.

hydrogen induced processes off Induced recombination and induced Compton heating are turned off with this command. Both processes (stimulated emission and induced recombination) are turned off with the command

```
no induced processes
```

described below.

hydrogen damping off Continuum scattering due to the extreme damping wings of Lyman lines (i.e., Rayleigh scattering) can be turned off with the "DAMPING OFF" option. Rayleigh scattering is a significant opacity source is very large column density clouds.

4.9.8 iterate [2 times]

This command specifies the number of iterations to be performed. The default is a single pass through the model. A second iteration should be performed in order to establish the correct optical depth scale when line transfer or radiation pressure is important. Two iterations are often sufficient, and will be done if no numbers are entered on the command line. No more than 10 iterations can be performed because of the present limits to the sizes of several vectors used to store information. A comment will be printed after the last iteration if the total optical depth scale has not converged and another iteration is needed.

iterate to convergence $[\max=7, \operatorname{error}=.05]$ This is a special form of the "ITERATE" command, in which the code will continue to iterate until the line optical depth scale has converged, or ten iterations have been computed. The optional first number on the line is the maximum number of iterations to perform, and the default is 10. It is not possible to specify more than ten iterations. The second optional number is the convergence criterion. Normally, it is that the H α optical depth has not changed by more than 10 percent on the next-to-last iteration. The optional numbers may be omitted from right to left. The iterations will stop when the changes in the H α optical depth are less than the second number, unless H α is optically thin, in which case only a second iteration is performed.

4.9.9 no scattering opacity

This command turns off several pure scattering opacities. These include scattering by grains, electron scattering, and the extreme damping wings of Lyman lines (Rayleigh scattering). When scattering opacity is included and an open geometry is to be computed, the scattering opacity is assumed to attenuate the incident radiation field as $(1 + 0.5\tau_{scat})^{-1}$ rather than $\exp(-\tau)$ (Schuster 1905).

Scattering should be neglected in a spherical geometry with gas fully covering the source of ionizing radiation, since photons absorbed by a pure scattering process are not really lost, but continue to diffuse out with (perhaps) a slight shift in energy. Electron scattering is generally the most important scattering opacity in a grain-free mixture. If $\tau_{scat} \leq 1$ then it is reasonable to consider electron scattering as a heating and cooling process, but not as an absorption mechanism, if the energy shifts are not large (i.e., $h\nu \ll mc^2$) and the geometry spherical (this is not correct for γ -ray energies, of course). CLOUDY is not now designed to work in environments which are quite Compton thick, but the approximation of neglecting electron scattering opacity for spherical geometries should work well for nebulae where the electron scattering optical depths are less than or of order unity. (Grain scattering has no direct effect on the gas, of course.) If this command is given then Compton energy exchange and recoil ionization are still included as heating, cooling, and ionization processes, but not as opacity sources. (Thermal and ionization effects of Compton scattering are turned off with the "NO COMPTON" command.) The "NO SCATTERING OPACITY" command is automatically generated when "SPHERE" is specified.

4.9.10 turbulence = 100 km/sec

The input number is the turbulent velocity (assumed to be microturbulence) expressed in kilometers per second. This velocity field affects the line-width and optical depth scale through the Doppler width $v = \sqrt{v_{th}^2 + v_{turb}^2}$, where $v_{th} = \sqrt{2kT/m}$ is the projected line-width due to thermal motions of particles of mass m, and the turbulent line-width v_{turb} is normally zero.

4.10 Thermal Solutions

This section describes options which affect the thermal solution. These deal with the accuracy of the solution (changes in the tolerance, or permitting more or fewer temperature failures), or with additional sources of heat, such as cosmic rays or turbulence.

4.10.1 cextra -14.231 [temp to the 1.5 power]

It is possible to add an "extra" source of cooling (due to some unspecified physical process) with this command. The first number is the log of the cooling rate in erg $cm^{-3} s^{-1}$. The second number is an optional exponent to specify a temperature dependence. The cooling will be given by

$$\Lambda = 10^{c_1} \times \left(\frac{T_e}{10^4 K}\right)^{c_2} \ erg \ cm^{-3} \ s^{-1}$$
(34)

where c_1 and c_2 are the two numbers entered with this command. If the second optional argument c_2 is not specified then zero (i.e., constant cooling) is assumed.

4.10.2 constant temperature, t=10,000K [linear]

A constant temperature calculation will be performed. The number can be either the electron temperature itself, or the log of the temperature (the latter is assumed if the argument is less than or equal to 10). If the optional keyword "LINEAR" appears on the line then the number is always interpreted as the temperature itself, and not its log.

Collisional ionization of all atoms and ions is included, so this option can produce clouds in coronal or collisional equilibrium. For technical reasons, the photon array must be defined for all energies which contribute to photoionization of all stages of ionization with significant abundances. For instance, to do models of the solar corona it is necessary to include both the cool blackbody from the solar photosphere (important for excited state induced recombination, photoionization, and Compton cooling) as well as a weak ~ 10^8 K bremsstrahlung continuum to define the photon array at all possible coronal energies (see the "CORONAL EQUILIBRIUM" command, described below).

If this command is used, then it is usually necessary to specify other stopping criteria. Many calculations stop when the electron temperature falls below some lowest value, set with the "STOP TEMPERATURE" command and with the default value 4000K. This cannot happen with a constant temperature model. For instance, a

constant temperature model of a planetary nebula will continue until the limit to the number of zones (now 300) is reached. The *vast* majority of the model will consist of predominantly neutral gas well outside the Strömgren sphere, and this gas will have an small ambient level of ionization and emission due to collisional ionization. The resulting emission-line spectrum would be surprising since the neutral gas contributes significant emission. A solution would be to use the "STOP EDEN" command to stop the calculation when the hydrogen ionization front is reached.

4.10.3 coronal equilibrium, T=10,000,000K

A model in coronal equilibrium, in which the gas is mainly collisionally ionized, will be computed. The number is either the temperature or the log of the temperature (the argument is interpreted as a log if it is less than or equal to 10). This calculation is very similar to those presented by, for instance, Raymond, Cox, and Smith (1976) or Gaetz and Salpeter (1983).

The command in the example above actually issues the following commands;

```
constant temperature t=10,000,000K
stop zone 1
drmax = 0
drmin = 0
stop lyman continuum optical depth = -6
brems, t=8
ionization parameter -7
```

4.10.4 cosmic rays, background, density=1.2 [index=-2, temp=7.3]

This command turns on energy deposition and ionization due to relativistic particles, as described by Ferland and Mushotzky (1984) and section 22.1 below. The first number is the log of the cosmic ray density (N_{cr} , cm⁻³). The second optional number is a power-law index α , describing the variation of the cosmic ray density with radius, i.e.,

$$N(cr, r) = N(cr, r_o) \left(\frac{r}{r_o}\right)^{\alpha} \quad . \tag{35}$$

The default value of the index is $\alpha = 0$, or constant density. The third optional number is the log of the temperature of the fast electrons, if they are not relativistic. If this third number is specified then expressions from Balbus and McKee (1982) will be used to evaluate the electron heating rates. The options can be omitted from right to left. Collective effects are not included in the heating and ionization rates, but they may not be important either (Rephaeli 1987).

If no numbers appear on the line, but the keyword "BACKGROUND" does, then a constant cosmic ray density of $N_{cr} = 10^{-9} \text{ cm}^{-3}$ will be used. This density will produce a neutral hydrogen ionization rate of ~ 10^{-17} s^{-1} , the value quoted by Spitzer (1978) for the galactic cosmic ray ionization rate. This value is quite uncertain. If cosmic rays are not included in the calculation, but the neutral hydrogen ionization rate falls below 10^{-17} s^{-1} , the code will print a comment stating that the ionization rate fell below the galactic background rate.

4.10.5 failures 100 times

A temperature failure occurs when the heating-cooling balance is not within a certain tolerance, set by the "TOLERANCE" command, after 20 tries. Normally CLOUDY will punt after an excessive number of temperature failures (presently 20) occur. This command increases the number of allowed failures to the value entered as a parameter.

When CLOUDY stops because of excessive failures it first produces a map of heating-cooling space to give an indication of where the equilibrium temperature should have been. Section 8 below describes thermal failures in more detail, and describes the output produced before the program stops.

Failures occur most often when the code needs to "jump over" the peaks in the cooling function which occur near 2000K and 10^5 K, or if it "trips" over an ionization front because the zones are too large. Increasing the number of allowed failures is permissible as long as the global energy balance is preserved. A warning will be issued at the end of the calculation if there is a discrepancy in the global heating-cooling balance.

The default limit to the number of failures is 20, which is stored as the variable LIMFAL.

4.10.6 force temperature to 3400K

This command forces the initial estimate of the temperature of the first zone to the value entered. The temperature is interpreted as a log if it is less than or equal to 10 and the linear temperature if greater than 10. This command is useful if more than one temperature solution is possible. It forces the first guess of the temperature to the specified value, but *does not* hold the temperature constant; the temperature is determined by energy balance thereafter. (Constant temperature is set with the "CONSTANT TEMPERATURE" command.)

4.10.7 hextra -14 [scale r=18]

This command turns on "extra" heating due to some unspecified energy source, such as dissipation of turbulence. The first number is the log of the volume heating rate (erg cm⁻³ s⁻¹). The second number is the log of the scale radius r_{scale} , such that the extra heating rate varies as $\exp(-r_{scale}/(r-r_o))$, where r_o is the inner radius. The default, when r_{scale} is not specified, is constant extra heating.

4.10.8 high temperature approach

This command tells the code to search for the first temperature by approaching the thermal solution from the high temperature extreme of 10^{6} K. Normally the approach is from low temperatures. This can be useful when more than one thermal solution is possible.

4.10.9 lowest temperature = 300K [linear]

The search for the temperature of the first zone can find temperatures as low as TELOW, which has a default value of 10K. CLOUDY will not allow initial temperatures below the value of TELOW, although after the first zone the temperature can fall to values as low as TEND, which has a default value of 4000K. This command can be used to change the value of TELOW. The argument is interpreted as a log if it is less than or equal to 10, otherwise as the temperature itself. There is an optional "LINEAR" keyword to force all values to be linear, rather than logs. The number is the sole element of common block "TELOW". (TEND is changed with the "STOP TEMPERATURE" command.)

4.10.10 magnetic field, $\log(B) = 5$

The argument is the log of the magnetic field strength in Gauss. Magnetic effects are not normally included; when this is specified, cooling due to cyclotron emission, using equations from Fabian, Pringle, and Rees (1976; these assume optically thin emission) are included. The volume cooling rate is given by

$$\Lambda_{cyclotron} = N_e \, \frac{B^2}{8\pi} \, \frac{4}{3} \, \sigma_T \, c \left(\frac{v}{c}\right)^2 = 4.5433 \times 10^{-25} B^2 \, T_e \quad erg \ cm^{-3} \ s^{-1} \tag{36}$$

where σ_T is the Thomson cross-section and

$$v_e = \left(\frac{8kT_e}{\pi m_e}\right)^{1/2} = 6.2124 \times 10^5 T_e^{1/2} cm \ s^{-1}$$
(37)

is the mean electron speed. See, however, Masters, Pringle, Fabian, and Rees (1977). They show that this emission process is likely to be optically thick under some circumstances. Cyclotron optical depth effects are not now included.

Cosmic rays should not be included when a magnetic field is specified, since the effects of a field on cosmic ray transport are not now included. A warning will be printed if both are included.

4.10.11 map 4 [range 2000, 5000]

This command tells the code to compute a heating-cooling map of the specified zone. This is a useful way to check for the existence of more than one thermal solution. If no zone is specified, or if the zone is less than or equal to 0, then only a thermal map is produced for the illuminated face of the cloud, and no zone calculations are performed.

The optional keyword "RANGE" specifies the temperature range of the map. If this option is specified then the first number on the line must be the zone for the map, zero if only a map of the first zone, and the next two numbers must be the lower and upper limits to the map. These temperatures will be interpreted as logs if less than or equal to 10.

The code is left in a disturbed state after a map is computed. It is best to begin a calculation over again after a map is computed, rather than try to continue with the current model. This can be done with the "STOP ZONE" command.

4.10.12 neutrons -2 [efficiency=-2]

This command adds energy deposition and ionization by secondaries, due to the fast neutrons proposed by Sikora, Begelman, and Rudak (1989). The argument is the luminosity in fast neutrons, expressed as a fraction of the *total* photon luminosity of the incident continuum. It is interpreted as a log if less than or equal to zero, and a linear scale factor if positive.

The second argument is optional, and is the heating-ionization efficiency of the neutrons. Its default is unity. Both quantities are interpreted as logs if less than or equal to zero, and linear if greater than zero.

4.10.13 print coolants, zone 135

This turns on an option to print out the emission-line cooling arrays for the specified zone. If no zone number or 0 appears on the line then the coolants for *all* zones will be printed. The numbers printed are the log of the cooling per unit volume. Significant $(\geq 5\%)$ of the total) coolants are marked by a sharp sign (#).

4.10.14 time dependent model of zone 3

A time-dependent model of the specified zone is performed, as discussed by Ferland and Truran (1981). The model follows the recombination and cooling after the ionizing radiation is instantaneously cut off. The initial conditions are those appropriate for the zone specified as the argument. Collisional ionization is included, so this calculation is somewhat like a shock.

This command does not now work, and will not function again until development work on helium is complete.

4.10.15 tolerance 0.001

The equilibrium temperature is set by balancing the heating and cooling rates. This command is used to change the error tolerance in the heating-cooling match. The default tolerance is 0.02 (or 2%). This will be the error in the heating-cooling balance allowed in each zone; the total error or energy conservation mismatch over a model will be much smaller, usually of order ten times smaller than the tolerance specified.

The tolerance is given by the variable "TOLER", which is the sole variable in the common block "TOLER".

4.11 Stopping Criteria

In some nebulae ionized by starlight, such as certain planetary nebulae or H II regions, the outer limit of the cloud is well-defined by an ionization front (the nebula is said to be radiation-bounded), and setting an outer limit is not necessary. In these cases the model stops because nearly all ionizing radiation has been attenuated, and the temperature falls below 4000K, the default lowest allowed electron temperature. This choice of lowest temperature was made with optical emission lines in mind; if lines with very low ionization and excitation potentials (i.e., the [CII] or [OI] infrared lines) are of interest, then it is probably necessary to lower this ending temperature with the "STOP TEMPERATURE" command.

In other circumstances, particularly X-ray ionized nebulae, the gas is optically thin to hard radiation and an outer limit must be specified. In other situations, optically thin models, or ones in which only part of the Strömgren sphere is present, must be computed (in this case the nebula is said to be matter-bounded). In these cases stopping criteria must be specified. More than one stopping criteria can be specified, and the calculation will stop as soon as the first one is met. CLOUDY will say why it stopped after the last zone calculation is printed.

If no stopping criteria are set, then the calculation will usually stop because the default lowest temperature (4000K) or the default greatest number of zones (300) was reached.

4.11.1 radius inner=18 [thickness=16; parsecs; linear]

The "RADIUS" command is discussed above. The optional second number is the log of the thickness of the cloud (if the second number is less than the first) or the log of the outer radius (if the second number is greater than the first). The default outer radius is 10^{30} cm. The default units are centimeters, but the arguments will be interpreted as the log of the radius and thickness in parsecs if the keyword "PARSECS" appears anywhere on the line. The numbers are interpreted as logs unless the optional keyword "LINEAR" appears. If both keys appear then linear parsecs result.

4.11.2 stop column density=23 [neutral; ionized; total; ...]

This command causes the calculation to stop when the specified hydrogen column density (cm^{-2}) is reached. There are several optional keywords, which determine whether the column density is the total (the default), the ionized hydrogen column density, the neutral hydrogen column density, or the effective column density (defined below). For all cases the default stopping column density is 10^{30} cm⁻².

stop column density=23 The number is the log of the total hydrogen column density (atomic, ionic, and molecular hydrogen), defined as the integral

$$\int \left\{ N(H^{\circ}) + N(H^{+}) + N(H^{-}) + 2N(H_{2}) + 2N(H_{2}^{+}) + 3N(H_{3}^{+}) \right\} f(r) dr$$
(38)

where f(r) is the filling factor.

stop neutral column density=23 The number is the log of the neutral (atomic) hydrogen column density, i.e.,

$$\int N(H^{\circ})f(r)\,dr \quad . \tag{39}$$

stop ionized column density=23 The number is the log of the ionized hydrogen (H^+) column density, i.e.,

$$\int N(H^+)f(r)\,dr \quad . \tag{40}$$

stop effective column density=23 This command is actually a form of the "STOP OPTICAL DEPTH" command. Usually, low energy cutoffs in X-ray spectra are parameterized by the equivalent column density of a cold neutral absorber with cosmic abundances. Actually, what is measured is an optical depth at some energy, generally around 1.0 keV. If the gas is ionized then a much larger column density will

be needed to produce the observed absorption, and the difference is often more than an order of magnitude. Using this command, it is possible to stop the calculation when the incident continuum has been attenuated by the appropriate absorption at 1.0 keV. The calculation will stop when the absorption optical depth at 1.0 keV (neglecting all scattering) reaches a value of

$$\tau_{abs}(1.0\,keV) = N_{effec} \ 2.14 \times 10^{-22} \tag{41}$$

at 73.5 Ryd. The absorption cross section per proton for cold neutral gas is taken from Morrison and McCammon (1983). Scattering opacities *are not* included in this optical depth. In general, the actual column density will be much greater than the "effective" column density.

4.11.3 stop eden 3 [linear]

The model will stop if the electron density falls below the indicated value. The number is entered as a log; in this case the model will stop if $N_e < 10^3 \text{ cm}^{-3}$. There is an optional keyword "LINEAR" which will force the argument to be interpreted as the quantity itself, not its log. This command is a useful way to stop constant temperature models. For instance the calculation can be forced to stop at the H⁺-H^o ionization front by setting the stopping electron density of approximately half of the hydrogen density.

The following examples show a case which will stop near the He^{2+} - He^+ ionization front (for solar abundances) and a case which will stop hear the H^+ - H^o ionization front.

```
* stop at the He++ - He+ ionization front
hden 9
stop eden 9.06 ;stop when helium (10 percent by number) is He+
* stop at H+ - Ho ionization front
hden 5
stop eden 4.5 ;stop when electron density falls below hydrogen density
```

The default is an electron density of -10^{30} cm⁻³. (The negative sign is not a typo.) It is stored as the variable ENDEDN, the sole variable in common block "ENDEDN".

4.11.4 stop efrac=1.05

The model will stop when the electron fraction, defined as the ratio of electron to hydrogen densities, falls below the indicated value. This is another way to stop calculations at ionization fronts, and is useful if the hydrogen density there is not known (this occurs in constant pressure calculations, for instance). The argument is the fraction itself if it is greater than zero, and the log of the fraction if less than or equal to zero.

The default is an electron fraction of -10^{37} cm⁻³. (The negative sign is not a typo.) It is stored as the variable EFREND, the sole variable in common block "EFREND".

4.11.5 stop line 6300 reaches 0.1 relative to 5007

The model will stop when the emission line with the wavelength given by the first number exceeds an intensity given by the second number, relative to a second emission line with wavelength given by the third number, in this example $[O \ III] \lambda 5007$. If a third number is not entered, this second emission line will be H β (not the default normalization line). This command is useful for stopping matter-bounded models. This results of this command are not exact; the final intensity ratio will be slightly larger than the ratio specified.

4.11.6 stop optical depth -1 at 2.3 ryd

This command stops the calculation at an arbitrary *absorption* optical depth. The first number is the log of the optical depth, and the second number is the energy in Rydbergs. The optical depth is always a log, and the optical depth does not include scattering opacities. The second number is interpreted as a log if it is negative, linear Rydbergs if positive, and must be within the energy bounds considered by the code (presently 1.001×10^{-5} Ryd to 7.354×10^{6} Ryd). At present, only one stopping optical depth can be specified; if more than one is entered then only the last is honored.

It is traditional in X-ray astronomy to characterize low-energy cut-offs as the equivalent *completely neutral* column density. This is not correct when the gas is ionized, since the high energy absorption opacity is diminished, often by more than an order of magnitude. The deduced column density is underestimated by the same amount. It is better to convert the deduced column density back into an optical depth at 0.5 or 1 keV (this is actually the observed quantity), and use this optical depth and energy as the stopping criteria, than to use the deduced column density as a stopping criteria. Either this command, or the "STOP EFFECTIVE COLUMN DENSITY" command (which is actually a form of the "STOP OPTICAL DEPTH" command) can be used to stop the calculation at an X-ray optical depth corresponding to a certain low-energy absorption.

The optical depth used in this command is the absorption optical depth, and does not include scattering opacities. The most important scattering opacity in grain-free environments is usually electron scattering, which is grey when $h\nu \ll mc^2$. As a result

this scattering opacity does not affect the usual X-ray analysis. In general, the effects of scattering opacities are much more geometry dependent than absorption.

stop Balmer optical depth = -.3 This command is a special case of the "STOP OPTICAL DEPTH" command, in which the energy does not need to be specified, but the keyword "BALMER" is given. It will cause CLOUDY to stop when the log of the absorption optical depth at the Balmer edge ($\nu = 0.250$ Ryd) reaches the specified value. The default is $\tau_{Bac} = 10^{20}$, and the optical depth is always interpreted as a log. This is the *total absorption* optical depth at the Balmer edge, and includes all computed opacity sources such as grains or free-free absorption.

stop Lyman optical depth = 5 This is a special case of the STOP OPTICAL DEPTH command, in which the energy does not need to be specified. In this case the model will stop at an absorption optical depth of 10^5 in the Lyman continuum. The number entered is the log of the Lyman limit optical depth, τ_{912} . The default value is $\tau_{912} = 10^{20}$. The stopping criterion is *really* the total 912Å absorption optical depth, and *not* the hydrogen Lyman limit optical depth at 912Å. These are not exactly the same, especially when grains are present or the abundances of the heavy elements are enhanced.

4.11.7 stop temperature=1,000K [linear]

The model will stop if the electron temperature drops below T_{low} , the argument of this command. The temperature is interpreted as a log if the argument is less than or equal to 10K, and linear if greater than 10, or the "LINEAR" keyword appears. The default value is $T_{low} = 4000$ K. Gas cooler than this produces little optical emission, but may be a strong emitter of infrared lines such as the [Ne II] 12.8 μ m, [CII] 158 μ m, or the [OI] ³P lines. The lowest temperature allowed, T_{low} , should be adjusted so that $h\nu \gg kT_{low}$ for the lowest excitation potential ($h\nu$) transition to be considered. Note that more than one temperature is sometimes possible when $T \sim 10^3$ K, so thermal stability problems may develop if T_{low} is lowered below a few thousand degrees Kelvin. If stability problems occur then it may be necessary to increase the number of thermal failures allowed, with the "FAILURES" command. This is discussed further in section 8 below. The lowest temperature allowed is stored as the variable "TELOW", the sole variable in common block "TELOW".

4.11.8 stop thickness 9.3 [parsecs; linear]

This command sets an upper limit to the thickness of the model. The argument is interpreted as the log of the thickness unless the keyword "LINEAR" appears. The default units are centimeters, but it will be interpreted as the log of the thickness in parsecs if the keyword "PARSECS" appears on the line. The "STOP THICKNESS" command has the same effect as the optional second number on the "RADIUS" command. This command makes it possible to set a thickness when the inner radius is not specified, such as when the ionization parameter is given.

4.11.9 stop zone 123 [21 on sec iteration, ...]

In this example the calculation will stop after computing 123 zones. The default value is 300. Up to ten numbers may be entered, each being the ending zone for consecutive iterations. If fewer numbers are entered than iterations performed, then the last number will be used for all further iterations.

4.12 Output

CLOUDY is capable of keeping a printer going for hours. Several commands vary the printer's mass-loss rate, and are described here. A description of the meaning of the output follows in section 3.

4.12.1 faintest line to print -2 [_off]

CLOUDY will normally print the intensities of all emission lines with intensities greater than 10^{-4} of the reference line, usually H β . This command changes the limit to the relative intensity of the weakest line to be printed. The argument is either the log (if less than or equal to zero) or the linear value of the intensity of the weakest line to print (if positive), relative to the reference line. The reference line is usually H β , and can be changed with the "NORMALIZE" command. In the case shown here, only lines with intensities greater than 1% of H β will be printed.

If no numbers are entered, but the keyword "_OFF" appears, then all lines are printed, even those with zero intensity.

4.12.2 line 1909

The relative intensities of a few selected lines are given for every printed zone. It is possible to have one extra emission-line intensity printed by entering this command, whose argument is the wavelength of the extra line. This is a useful way to follow the buildup of a line across a model.

4.12.3 normalize to 1216 [scale factor = 100]

Emission-line intensities are usually listed relative to the intensity of H β . This command changes the reference line to any of the other predicted lines. The entire emission-line spectrum will have its relative intensity normalized to the intensity of the line whose wavelength is given by the argument.

The optional second number is a scale factor for the relative intensity array. If it is equal to 100, as in this example, then all intensities will be relative to a reference line intensity of 100. The default value is 1. The example given above will cause the intensities to be expressed relative to a Ly α intensity of 100.

4.12.4 pall

This command tells the code to print many emission lines whose intensities are simply scaled from lines usually printed, such as the higher Balmer lines, and many helium lines. These assume case B emissivities, and are not reliable at high densities, or when lines are optically thick. This option was added by P.G Martin.

4.12.5 plot continuum map opacity [Emin=.1, Emax=10, trace]

A plot of any of several properties of the calculation can be made. One of the keywords described below (continuum, map, or opacity) must appear on the command line. Up to ten plots can be generated; this limit is set by the variable NDPLOT which appears in several parameter statements throughout the code. The keyword "TRACE" will turn on a great deal of information concerning the mechanics of generating the plot.

Publication quality plots can be produced using the "PUNCH" commands (described below) to produce a file which can then be post-processed using plotting software.

4.12.6 plot continuum [Emin=1, Emax=4, _raw, trace]

If "CONTINUUM" is entered then the continuum (usually 1.001×10^{-5} Ryd $\leq h\nu \leq 7.354 \times 10^{6}$ Ryd) is plotted, unless the range is altered by entering the two optional numbers. The default is for both the incident continuum (in units of νf_{ν}) entering the cloud (plotted as .'s) and that transmitted through the cloud (the o's) to be plotted.

Plot continuum keywords It is also possible to plot specific components of the continuum. If the keyword "DIFFUSE" appears then the diffuse emission per unit volume, for the last computed zone, will be plotted. This continuum is only that emitted by the gas and grains in the optically thin limit and unity filling factor. If the

keyword "EMITTED" appears, then the net integrated continuum produced by the cloud is plotted. This is the sum of the continuum emitted in the inward and outward directions from the computed ionization structure, and does not include the incident continuum. If the keyword "REFLECTED" appears, then only the continuum emitted from the illuminated face of the cloud is plotted. This includes the back-scattered portion of the incident continuum, along with diffuse emission from the cloud. This is meaningful only for non-spherical geometries. If the option "_RAW" is specified, then the continuum in units actually used inside CLOUDY (cm⁻² s⁻¹ cell⁻¹) will be plotted. If the keyword "PHOTON" appears, then the units of the plotted continuum will be photons cm⁻² s⁻¹ Ryd⁻¹).

4.12.7 plot opacity [absorption, scattering, total min=1 max=4]

If the keyword "OPACITY" is entered then the opacity of the first and last zones (per hydrogen atom) is plotted. The continuum between 1.001×10^{-5} Ryd $\leq h\nu \leq$ 7.354×10^{6} Ryd is usually plotted, unless this is adjusted by entering the optional energy range. There are three optional keywords; "absorption" "scattering" or "total", to change which opacity is plotted. If none appear, then the total opacity is plotted.

plot range options For the OPACITY and CONTINUUM options, there is a further option to specify the energy range of the plot. If one number occurs on the command line then it is interpreted as the lowest energy (in Rydbergs) on the plot. If the first number is zero, then it is interpreted as the lowest energy in the continuum, presently 1.001×10^{-5} Ryd. The optional second number is interpreted as the highest energy shown on the plot. If the second number is omitted or zero, then it is interpreted as the high energy limit of the code, presently 7.354×10^{6} Ryd. If either number is negative then both are interpreted as the log of the energy, otherwise they are assumed to be the linear energy in Rydbergs. If the first number is zero (i.e., interpreted as the lowest energy of the upper limit to the plot, and not its log.

4.12.8 plot map [Tmin=3,000K, Tmax=20,000K, linear]

If the keyword "_MAP" (note the leading space) appears then a plot of the heating and cooling rates as a function of temperature will be made. This will follow the last zone calculated, and will be appropriate for the attenuated continuum and physical conditions in that zone.

plot map range options The high and low temperatures on the map can be changed by entering one or two optional numbers. If no numbers appear then a range

of 10 K to 10^9 K is assumed. If only one number appears then only the lower temperature limit is changed. If two numbers appear then both lower and upper limits are changed.

If the first number is less than or equal to ten then both numbers are interpreted as logs of the temperature. If the first number is greater than ten then both numbers are interpreted as the temperature itself. If the keyword "LINEAR" appears then both numbers are interpreted as the temperature itself no matter how large or small they may be.

4.12.9 print every 1000 [5 37 93]

CLOUDY will always print the results for the first and last zone. This command can be used to vary the number of zones printed in between. In the example above, it will print every 1000 zones on the first iteration, every 5 zones on the second iteration, etc. Normally about 100 - 200 zones are computed per model, so printing every five or ten zones on the last iteration may be useful. If there are fewer numbers entered than iterations performed, then the last number entered will be used for all further iterations. The default value is to print only the first and last zones.

4.12.10 print arrays

This option tells the code to print the ionization balance arrays for all elements heavier than helium. The first line is the vector of ionization rates, in units s^{-1} . The second line is the vector of recombination rates, also s^{-1} . These lines are the two diagonals of the bi-diagonal matrix used in the solution of the ionization balance equation, and include *all* ionization and recombination processes.

4.12.11 print coolants, zone 135

This turns on an option to print out the emission-line cooling arrays for the specified zone. If no zone number or 0 appears on the line then the coolants for *all* zones will be printed. The numbers printed are the log of the cooling per unit volume. Significant $(\geq 5\%)$ of the total) coolants are marked by a sharp sign (#).

4.12.12 print departure coefficients

This command tells the code to print departure coefficients in addition to the relative populations for the lowest seven of the ten levels of hydrogen, H^- , helium, and some molecules.

4.12.13 print heat

This tells the code to print out the relative heating due to each stage of ionization or physical process. The number is the fraction of the total heating due to this particular stage of ionization, and is printed directly below the relative abundance of that stage.

4.12.14 print last

Normally, results for every iteration are printed as they are computed. If this command is entered then only results for the last iteration will be printed.

4.12.15 print only [header, zones]

The keyword "ONLY" shortens the printout somewhat by stopping the calculation prematurely. If it appears, then another keyword, presently "HEADER" or "ZONES", must also appear. The command "PRINT ONLY HEADER" will cause the code to stop after printing the header information. The command "PRINT ONLY ZONES" will cause the code to stop after printing the zone results on the first iteration.

4.12.16 print short

The detailed final printout is shortened when the "SHORT" keyword appears. Only the emission lines, and a short summary of some thermal properties of the model, will be printed.

4.12.17 print starting at 61

This option turns off all printout until the specified zone is reached.

4.12.18 punch option [unit=8]

Punch (output on an arbitrary output unit) any of several possible pieces of information. This command is a primary output mechanism for CLOUDY. The options are many; physical quantities such as temperature, ionization, density, for each zone are produced for some options, for other cases the continuum or other quantities predicted by the code can be output. In all cases, the general idea is for the file produced by this command (called "fort.n" in UNIX, where n is the integer on the command line) to then be post-processed by other plotting programs to produce final plots.

The current options are summarized in Table 12, and one of these keywords must appear. Only one keyword per line is recognized. The four character key which must be matched is capitalized. This command causes a subroutine called "PUNCHR" to be

called after every zone calculation. If "SPECial" is specified then a portion of the subroutine will be used, which can be changed to fit the circumstances.

The optional number on the line is the FORTRAN I/O unit number used for the output. Up to ten PUNCH commands, with or without different output numbers, can be entered. Unit 7 will be used for the first file if no number appears on the line. If no I/O unit number appears on subsequent "PUNCH" commands the unit number will be incremented by one on each call i.e., the second file will be fort.8). This is to ensure that no more than one PUNCH command writes to a given file.

Normally the results are produced for every iteration. Only results from the last iteration will be produced if the "LAST" keyword appears on the line.

Note that CLOUDY uses FORTRAN logical unit 6 for output, and unit 5 for input. These units cannot also be used for punch output, and the same logical output unit cannot be used for more than one punch option.

punch continuum This command is the primary mechanism for printing out the continuum predicted by the code. The first column is the energy in Rydbergs. The second column is the incident continuum $(\nu F_{\nu}, \text{ erg cm}^{-2} \text{ s}^{-1})$ at the illuminated face of the cloud, and the third column is the transmitted portion of the incident continuum, in the same units. The 4th column is the continuum emitted by the computed structure, and includes a covering factor if one was specified. The 5th column gives the net transmitted continuum, the sum of the attenuated incident and diffuse continua. This would be the observed continuum is the nebula fully covers the continuum source. The 6th column is the reflected continuum. All continua are the flux (erg cm⁻² s⁻¹) and are relative to the inner radius of the clouds (i.e., the specific luminosity would be the predicted quantity multiplied by $4\pi r_{inner}^2$).

punch lines, structure This option on the PUNCH LINES command tells the code to punch the emissivity of up to ten emission lines as a function of depth into the cloud. The emission lines are specified on the following input lines, and end with a line with the keyword "END" in columns 1-3. The label used by CLOUDY to identify each line (see section 6) must appear in column 1-4 of the line, and the integer used to identify the line wavelength appears as a free-format number in later columns. The line labels and wavelengths are then punched. The depth into the cloud, and the volume emissivity (erg cm⁻³ s⁻¹, for unit filling factor) is then punched for each line. This information can then be used to reconstruct the surface brightness distribution of a resolved emission-line object.

The following illustrates its use;

punch lines, structure
totl 4861

Table 12: Punch Options

Keyword	Output
CALCium	NSTEP, CA(1, 2, 3, 4)
CARBon	NSTEP, radius, depth, CARB(1-7)
$\operatorname{CONTinuum}$	$ u_R, \nu F_{\nu}(inc), trans, diffuse, sum, reflect$
EMITted CONTinuum	$ u_R, \nu \mathrm{F}_{ u}(\mathrm{emitted \ both \ sides}) $
DIFFuse CONTinuum	$ u_R, u \mathrm{F}_{ u}(\mathrm{unit} \mathrm{vol}) $
IONIzing CONTinuum	$ u_R, u^2 \phi$
REFLected CONTinuum	$ u_R, \nu F_{\nu} $ reflected
TRANsmitted CONTinuum	$ u_R, u F_ u, \mathrm{raw}$
DR	logic behind choice of zone thickness
GRAIN OPACity	nu, extinction, absorption, scattering
GRAIN PHYSical	te, potential, drift velocity, frac heat
GAUNt factors	$ u(\mathrm{Ryd}),\mathrm{free} ext{-free gaunt factor}$
HELIum	NSTEP, radius, depth, HeI, HeII, HeIII
HYDRogen	NSTEP, TE, HDEN, EDEN, (HI, HII, H2, H2+, H3+, H-)/HDEN
IRON	NSTEP, $-\log 10(rel ioniz)^*100$
LINEs STRUcture	DEPTH, line emission per unit vol
LYMAn alpha	$ au(Lylpha),\mathrm{N}(\mathrm{2p})/\mathrm{N}(\mathrm{1s}),\mathrm{T}(\mathrm{excitation})$
_MAP	Te, heating, cooling
MOLEcules	H2/HDEN, CO/H, H2O/H, OH/H, CH/H
OPTIcal depths	nu, total, absorption, scattering optical depths
OPACities	nu, opacity(nu), albedo
LOTS	nu, flux, otscon, otslin, outcon
$_QS$	nu, qabs, qscat
OXYGen	NSTEP, $oxy(1,2,3,4)$
PHYSical cond	$NSTEP, R-R_o, TE, HDEN, EDEN, rad accel$
PRESsure	NZONE, depth, $P(gas)$, $P(rad)$, $Pinteg$
RADIus	NZONE, R, R-Ro, dr
RECOmbin effic	$\tau(912)$, rec effic to n=1
SOURce function	nu(R), diffus, opacity, source fcn, black body ratio
SPECial	Specially defined
TEMPerature	NZONE, T, dT/dr
WIND	Radius, thickness, velocity, acceleration, force multiplier

=

4.12 Output o 3 5007 totl 3727 o 1 6300 end of lines

punch transmitted continuum This command is used to save the transmitted (attenuated incident and outward component of diffuse) continuum at the end of the calculation. This punch file can then be used as part of the continuum in a later calculation, by reading in this file with the "TABLE READ" command.

Three cautions when reading this file as an input continuum: a) if the keyword "last" does not appear on the line then the continuum from each iteration will be punched. Probably results from only the last iteration are needed, so either the "last" option should the used, or the file must be edited after the initial calculation to leave only the last computed continuum; b) on the second calculation punch output should not be created on the same FORTRAN unit number as the input file. It will overwritten if this occurs; c) the program expects the first two lines to contain header information and skips them. They should not be deleted from the input file.

4.12.19 quiet

This command sets CLOUDY's quiet mode, in which nothing is printed at all. Specifically, it sets the variable TALK in common block CALLED to false. Printing can be started at a particular zone by combining this command with the "PRINT STARTING AT" command described above.

4.12.20 sort

This option causes the output spectrum to be sorted by wavelength rather than by ion. It was added by P.G. Martin. It doesn't work.

4.12.21 title This is a title

The argument is a title for the calculation, and can be useful for organizing the models in some manner. The title is reprinted several times.

4.12.22 trace zone 94 [iteration 2;hydrogen;helium;carbon;...]

This command turns on trace printout beginning *after* the zone given by the first number on the line. The trace follows the logical flow within CLOUDY, and is a useful

Table 13: Trace Reywords and Effects						
keyword	variable	Trace				
CARBon	CARBUG	carbon ionization equilibrium				
Compton	COMBUG	Compton heating, cooling, and ionization				
CONTinuum	CONBUG	prints out photon arrays, pointers				
DIFFuse fields	TRDIFF	sum of recombination coef in DIFFEM				
DR	DRBUG	choice of next zone thickness				
GRAIN	DSTBUG	details dealing with grain treatment				
EDEN	NEBUG	changes in electron density				
GAUNt	TRGANT	the free-free gaunt factors				
IRON	FEBUG	Fe Auger - fluorescence K-alpha problem				
HEATing	HEATBG	heating agents				
HELIum	HEBUG	helium ionization equilibrium				
HELIum IONIzed	HE2BG	helium ionization equilibrium				
HELIum SINGlet	HE1BG	helium ionization equilibrium				
HELIum TRIPlet	HE3BG	helium ionization equilibrium				
HYDRogen	HBUG	hydrogen ionization equilibrium				
Ly BETA	TR8446	$Ly\beta$ - OI 8446 pumping problem				
OPACities	OPCBUG	continuous opacities, zone by zone				
OPTIcal depths	OPTBUG	inner, outer optical depths in STARTR				
MOLEcules	TRMOLE	rate coefficients for molecules				
NEON	NEONBG	recombination, ionization for neon				
THREe body	BD3BUG	three-body recombination rates for metals				
TWO photon	BUG2NU	induced two photon processes				

Table 13: Trace Keywords and Effects

way to follow the internal decisions CLOUDY makes. CLOUDY uses adaptive logic to control many choices, such as the run of zone thickness with radius. This command allows these decisions to be followed in detail. If the zone is zero, or if no numbers occur on the line, then the trace is turned on at the beginning of the calculation. The second (optional with default=1) number is the iteration on which the trace should be started. It should be set to 2 to turn on the trace for the second iteration. Table 13 lists the trace keywords (column 1; the four character part of the key which must be matched is capitalized), the logical variable in CLOUDY which is affected (column 2; these are variables in the common block of the same name), and the purpose of each.

Command	quantity varied	Min	Max	Increment
BLACKBODY	temperature	def	def	0.5
BREMSSTRAHLUNG	temperature	def	def	0.5
FILLING FACTOR	filling factor	def	0	0.5
HDEN	hydrogen density	def	def	1.0
IONIZATION PARAMETER	ionization parameter	def	def	0.5
LUMINOSITY	luminosity of source	def	def	0.5
METALS	log of metalicity	def	def	0.5
PHI(H)	log of photon flux	def	def	0.5
Q(H)	log of total number of photons	def	def	0.5
RADIUS	inner radius	def	def	0.5
STOP COLUMN DENSITY	column density	def	def	0.5
TABLE STAR KURUCZ	temperature	4.477	4.699	0.1
TABLE STAR MIHALAS	temperature	4.477	4.740	0.1

Table 14: Commands with "Vary" Option

4.13 The Optimize Command

The OPTIMIZE command and its keywords tell the code to vary two or more of the initial parameters to try to find an optimal set of parameters to fit a specified emission-line spectrum, line flux or luminosity, and/or a set of column densities. The method was first implemented in CLOUDY by R.F. Carswell, who wrote most of the code for the present version. It uses the downhill simplex algorithm (Press et al. 1988) to obtain a best fit to a set of observed quantities. The desired emission-line spectrum, line flux or luminosity, and/or column densities, are specified by a series of "OPTIMIZE" commands. A keyword "VARY" can appear on several of the commands used to specify initial conditions (Table 14) to indicate which parameters are to be varied.

At a minimum, a desired emission-line spectrum, line flux, or column density, and a specification of which parameters are to be varied, must be given. The parameters to be varied during the optimization are specified by a keyword "VARY" which may appear on any of the commands listed in Table 14. Up to 20 parameters may be varied at a time; this limit is set by the variable LIMPAR which appears in several PARAMETER statements throughout the code. The quantities being varied are actually entered as logs within the code, and increments to the initial guess are also logarithmic. More than one parameter must be varied because of limitations in the current optimization algorithm. It simply cannot find a solution with only a single variable parameter.

An example of the "VARY" option in action is given in an sample input stream in

section 25 below. A typical input stream follows:

```
blackbody, 50,000K
hden 4 vary
ionization parameter -2 vary
stop zone 1
*
* the following specifies observed emission lines, order is
* label, wavelength, intensity relative to H-beta, tolerance
optimize lines
0 3 5007 intensity=13.8 error=1.
totl 3727 < 2.1 (only upper limit)
end of lines
*
* following are elements, stage of ionization, log col density
optimize column densities
carbon 4 17.4
silicon 3 14.6
end of column densities
```

Information concerning the optimization process is fed to the code as a series of keywords on the "OPTIMIZE" command; these are described next. Only one keyword will be recognized per "OPTIMIZE" command.

4.13.1 optimize, column density

This tells the code to try to reproduce a set of column densities. A series of column densities, ending with a line with the keyword "END" in columns 1–3, will be read in from subsequent lines. One column density is entered per line, and up to 100 may be specified. Columns 1 to 4 of the column density lines must contain the first four characters of the name of the element, spelled as in the output from the zone results. The first number on the line is the ionization stage, 1 indicates Atom I, 3 indicates Atom III, etc. The second number on the line is the log of the column density (cm⁻²), and the last optional number is the relative uncertainty. It has a default of 0.05 (5 percent). A column density can be specified as an upper limit by entering "<" anywhere on the line. If "<" appears then the column density is only included in the optimization if the predicted value exceeds the upper limit.

The following gives some examples of its use;

optimize column densities hydrogen 1 < 17 ;make sure optically thin in lyman continuum

80

carbon 4 17.4 error=.001
silicon 3 14.6
end of column densities

4.13.2 optimize, increment = 0.5 dex

The increments are the amounts by which each variable is changed in the first step away from the initial parameter. The default increments preset in the code were chosen with "typical" conditions in mind. The increments are logarithmic quantities which will be added to or subtracted from the initial guess. It may be necessary to increase these if the process is unable to identify a solution. If a zero is entered as an increment, then the default increment will not be changed.

The increments entered with this command affect *only* the previously selected "VARY" command. The following gives some examples of changing the increments.

```
hden 4 vary
optimize increments .1 ;this sets .1 dex changes in hden
brems 6 vary ;increments left at default
radius 13.6 vary
optimize increments .05; this sets changes in radius
```

The increments are stored in the vector variable VINCR.

4.13.3 optimize, (intensity, luminosity)=36.425 [error=0.1]

The code will try to make the predicted intensity or luminosity of the normalization line (usually H β) match the entered value. The sub-keyword is either "intensity" or "luminosity", and both have exactly the same effect. The number is the log of either the intensity or luminosity of the line, in the same units as found in the final print out. The second (optional) number is the fractional tolerance allowed for the fit between the observed and computed values. If a tolerance is not specified, then 0.05 (five percent uncertainty) is assumed.

4.13.4 optimize, iterations=75

The upper limit to the number of iterations to be performed is specified with this command. The maximum number of iterations is stored as the variable ITOPTM, which has the default of 20. It is probably a good idea to reduce the number of iterations if the initial guess is far from the solution. It may be necessary to increase the limit if the process is still making progress at the end of the calculation. The limit to the number of iterations should really be some function of the number of parameters being varied.

4.13.5 optimize, lines

This command tells the code to try to reproduce a set of relative emission-line intensities, and to begin reading a list of observed lines. Up to 100 lines may be entered; the limit is stored as the variable NOBSLM which appears in several PARAMETER statements throughout the code.

One emission line is specified per input line, and the line must contain information in the following order: columns 1 to 4 of the line must list the label CLOUDY uses to identify the line; this must then be followed by the wavelength, a free format integer. Both must exactly match the identifications used inside CLOUDY and printed as line labels in the output; the code will stop if this is not the case. Section 6 below gives the emission line or continuum labels and wavelengths. The third quantity on the line is the desired relative intensity of the line. This will be in the same units as the relative intensities normally printed at the end of the calculation. Intensities are normally relative to H β , but can be changed to other reference lines with the "NORMALIZE" command (described elsewhere). The last (optional) number is the fractional tolerance allowed for the fit between the observed and computed values. If a tolerance is not specified, then 0.05 (five percent uncertainty) is assumed. A line can be specified as an upper limit by entering "<" anywhere on the line. If "<" appears then the line is only included in the optimization if the predicted value exceeds the upper limit.

The series of emission lines ends with a line which has the keyword "END" in columns 1 to 3. If this "end" does not appear correctly then the code will continue reading lines until the end-of-file is encountered.

4.13.6 optimize, punch=9

At the end of the optimization process the optimal input parameters are entered into a file for later use. Normally this is Fortran "punch" unit 7 (i.e., fort.7 in Unix). The unit number can be changed with this command. Using this file, it is possible to make later calculations in which various quantities are also punched for plotting. Also, it is generally a good idea to confirm that a single run with CLOUDY does reproduce the final results from the many calls of the code made by the optimization method. The two should agree exactly, but would not if the code became corrupted during the many calls made during the process (this could happen if a pointer went astray, for example).

Be careful that the unit specified with this command is not the same as one of those used by the "PUNCH" command. The files will overlap if the same unit is used.

4.13.7 optimize, range -2.3 to 3.9

It is possible to establish limits to the allowed range over which parameters are to be varied. The limits which are preset in the code are indicated in Table 14. The entry "def" indicates the default limits of -1×10^{37} and 1×10^{37} .

It is sometimes necessary to establish physical limits to parameters which are varied. For instance, metalicities may be limited to the range $-1 \leq \log(Z) \leq 0$ by observations or physical plausibility. The optimization driver doesn't know this, but can be told a set of bounds with this command. The arguments are ordered pairs of limits, which are the log of the lower and upper limits to the allowed range of variation of the previous command with "vary" specified. In this way the command is similar to the "OPTIMIZE INCREMENTS" command described above. The default limits are -1E37 and +1E37 respectively. Examples follow.

```
hden 4 vary
optimize range from 3 to 5 ;this sets limits to range of density
brems 6 vary ;no range for this one
radius 13.6 vary
optimize range from 13 to 14; this sets limits to radius
```

The optimizer does not actually know about the range limit; a residual of 10^{37} is returned if a parameter outside the allowed range is used. The limits to the range are stored in the vectors VARANG(1,n) (lower limit) and VARANG(2,n) (upper limit).

4.13.8 optimize, tolerance = 0.2

The tolerance, a measure of the overall agreement between the observed and specified spectra, intensity, and/or column density, is set with this command. The tolerance is stored as the variable VTOLER, with the default value 0.10.

4.13.9 Convergence criteria

The sum of residuals

$$\sum \left[\frac{(observed - model)}{model \times \delta}\right]^2 \tag{42}$$

is accumulated over all relative intensities, line intensities or luminosities, and column densities, and minimized. In this expression "observed" and "model" are the observed and computed quantities. If the model prediction is zero then a residual of 10^{37} is returned. The uncertainty δ is specified when the observed quantities are read in and has a default value of 0.05 (5 percent). For column densities and relative line fluxes the linear quantity is used to form the residuals. To avoid floating point problems on 32-bit IEEE machines, the log of the line flux or luminosity is used. The process stops when the sum of residuals is smaller than the variable entered with the "OPTIMIZE TOLERANCE" command, which has the default of 0.10.

4.13.10 Notes concerning commands with "vary" option

The keyword "VARY" can appear on the commands in Table 14. Notes concerning these follow.

Blackbody It is not possible to specify the luminosity of the blackbody by using the keywords on the blackbody command when the VARY option is used. It is necessary to enter the luminosity using some other command, such as "LUMINOSITY" or "IONIZATION PARAMETER".

Filling factor Only the filling factor itself can be varied. It is possible to specify the optional power law for a radial dependence but it is not possible to vary it.

HDEN It is possible to specify the exponent for the optional power law density dependence upon radius or thickness. It is not possible to vary this additional parameter; only the initial hydrogen density is varied.

LUMINOSITY It is possible to specify all of the options on the luminosity command, but it is only possible to vary the luminosity itself.

PHI(H) and Q(H) It is possible to use the "RANGE" option, but only the log of the photon number will be varied.

RADIUS It is possible to specify the stopping radius on the line, but it is not possible to vary it. Only the starting radius is varied.

STOP COLUMN DENSITY All of the optional keywords (neutral, effective, etc) are recognized.

4.13.11 Notes concerning the optimization process.

Use physically motivated initial conditions. The algorithm will not be able to find a solution if one is not physically possible. For instance, an observed HeII $\lambda 4686/H\beta$ ratio of 0.5 cannot be produced by a a 20,000K blackbody, no matter how many other parameters are varied (it produces no He⁺ ionizing radiation). It is probably necessary to start with parameters in the general area of the successful model. When far from the solution, it is also a good idea to limit the number of iterations the optimizer can perform (using the "OPTIMIZE ITERATIONS" command) to stop it from over-optimizing a bad solution.

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Change the increment size The initial increment will be the largest step ever taken during the optimization process. If the initial parameters are far from the solution then it may be wise to increase the increments.

Set physically motivated limits to the variable quantities. The optimizer driver uses a pure "brute force" method, and understands surprisingly little modern astrophysics. For instance, while trying to reproduce an observed HeII λ 4686/H β intensity ratio of 0.5 by varying the temperature of a black body radiator, the algorithm is likely to examine the consequences of photoionization by a 100K radiation field. Physically, it is known that HeII emission only occurs for stars hotter than ~50,000K (Osterbrock 1988), so there is little purpose in examining temperatures lower than this. Also, the code may crash if radiation fields which produce *no* ionizing radiation are entered. The process will converge more quickly if reasonable bounds to the range of the varied quantities are set using the "OPTIMIZE RANGE" command.

Don't give up! My experience is that this process works about a quarter of the time. The problem is that the algorithm can easily "home-in" on a local minimum, which is actually a very bad solution. When this occurs, the best idea is to restart the optimization process with a different set of initial conditions. Better yet is to start the process with parameters which give answers known to be close to the solution. In order to avoid wasting time, it is also a good idea to limit the number of iterations with the "OPTIMIZE ITERATIONS" command.

4.14 Miscellaneous Commands

Several commands are useful for changing basic physical processes or internal parameters in CLOUDY. These options were largely intended to help "fine-tune" or debug CLOUDY, or to identify the importance of individual physical processes. These commands are not normally used.

4.14.1 dielectronic recombination [10]

At present rate coefficients for dielectronic recombination through low-lying autoionizing states have not been computed for most elements on the third row and higher. For the four lowest stages of ionization, the code uses the means of the rate coefficients for C, N, and O; these are $3 \pm 2 \times 10^{-13}$, $3 \pm 2 \times 10^{-12}$, $1.5 \pm 0.5 \times 10^{-11}$, and $2.5 \pm 1.4 \times 10^{-11}$, cm³ s⁻¹, for the successive stages of ionization. Because no better can be done at present, these are used for those ions which have no rate coefficients. These rate coefficients can be turned off, or the values changed by a scale factor, by entering this command. If a number is entered on the line then it is the scale factor to multiply all the above rate coefficients; if no number is entered then zero is assumed and the effect is turned off. This is a useful way to check on the importance of this recombination mechanism for specific calculations. The Opacity Project (Seaton 1987) should soon produce all needed recombination rate coefficients.

4.14.2 drive [fread, gaunts, pointers, ...

This command causes CLOUDY to enter a special debug mode, in which the program requests information and responds with deduced quantities. A flag is set when the commands are entered. Parameters for the entire model (density, continuum, and luminosity) must still be specified. This mode is entered after the last command is specified and the input stream ends with a blank line or the end-of-file.

drive escape probabilities The command causes the code to enter a debug mode in which the user enters the log of a one-sided optical depth, the code queries three of the escape probability functions, (complete redistribution with damping wings; incomplete redistribution, and complete redistribution with only the Doppler core), and responds with the one-sided escape probabilities. A null line exits the driver.

drive fread This command causes the code to enter a debug mode in which the free format input reader, subroutine FREAD, reads the input stream and prints the interpreted number. The program will request an input line, and print the interpreted number, until a line with the number zero is entered.

drive gaunts This command enters a CLOUDY debug mode in which a driver requests temperature and photon energies, queries the free-free gaunt factor routine, and responds with the returned gaunt factor. The gaunt factor routine was written by David Hummer, and is described in Hummer (1988).

drive molecules Here it is possible to change individual molecular abundances within the iteration loop.

drive pointers This command allows the user to interrogate the frequency array. After the continuum is generated, the driver will ask for energies in Rydbergs (interpreted as a log if negative) and respond with the cell pointer, frequency, cell width, boundaries, and the phase space factor $2h\nu^3/c^2$. Once complete, the calculation will continue as usual.

4.14.3 drmax 11.2

This command sets the largest allowed zone thickness. The argument is the log of the thickness in cm, and the default is 10^{30} cm. It is possible to force the zones to have a specific thickness by combining the "DRMAX" and "DRMIN" commands.

4.14.4 drmin 11.2

The number is the log of the minimum zone thickness (in cm). It may be necessary to specify this if CLOUDY starts to oscillate near an ionization front in a constant pressure model. If this happens and "DRMIN" is not set then the zones become smaller and smaller, as CLOUDY tries to damp out the oscillations. If this occurs, then, at the end of the calculation, the code will suggest using this command to establish a smallest zone size The default value is 10^{-20} cm.

4.14.5 eden -2

This command allows an "extra" component of free electrons to be added to the gas. The argument is the log of the electron density (cm^{-3}) . This command is used to test the behavior of CLOUDY in the limit of very low Compton temperatures. When $T_{color} \ll 10^4 K$, the gas is almost entirely neutral, and free electrons must be artificially added to test the Compton energy exchange problem in the strict TE limit. (Remember, charge conservation is a horrible thing to violate.)

4.14.6 flxfnt -20

The highest continuum frequency which needs to be considered in equilibrium calculations is lower for relatively soft continua, such as H II regions, than for x-ray continua, such as AGNs. The criterion used to choose the highest energy ν_{high} to be considered is that $\nu f_{\nu}(\nu_{high})/\nu f_{\nu}(\nu_{peak}) < \text{FLXFNT}$, where ν_{peak} is the frequency where the continuum reaches its maximum νf_{ν} . FLXFNT is normally 10^{-10} . This command changes the value of FLXFNT. The argument is the log of the value.

4.14.7 fudge factors 4.59678 [12.3 34.5 958 ...]

The numbers appearing on the line can be communicated to any part of the code which calls the function "FUDGE". This has a single integer argument which points to the numbers entered on the command line. In the example given above, a call to FUDGE(2) would return the value 12.3. Up to ten numbers can be entered on the command line. Extra numbers are ignored.

This option is not normally used, but can be a useful way to pass numbers to temporary or trial parts of the code. All elements of "FUDGE" are initially zeroed in the large BLOCK DATA. The function "FUDGE" is a permanent part of CLOUDY, and a warning is given at the end of the calculation if this function is ever evaluated. Also, the function checks that the pointer to the array of stored values is not larger than the number of values entered in the command line; the code will stop if too few values are entered.

4.14.8 increments 0.05 .05 [scale factor = 2]

This command adjusts the two variables used to choose the zone thickness. The thickness of the first zone is chosen so that the largest continuous optical depth through it is equal to the first number on the line. The default is 0.1. Thereafter, the zone thickness is continuously adjusted by checking that the relative ionization of hydrogen, helium, carbon, oxygen, and iron do not change by more than a factor related to the second number. The default is 0.15. If only one number appears on the line then it is interpreted as a scale factor used to multiply the default values. If any number is less than or equal to zero, then it is interpreted as the log of the quantity, and linear if greater than zero.

4.14.9 no...

It is possible to disable physical processes as a test of their importance. If a physical process is turned off, then the logical variable "PHYSOK" in the common block of the same name is set to false to indicate that the treatment of physical processes is not ok. A warning is then printed at the end of the calculation, as a reminder that the results of the calculation are not to be trusted.

4.14.10 no (2p2s;2s2p) collisions

This command turns off 2s-2p collisions in the hydrogen atom and helium singlets and ion; it is mainly used for debugging the hydrogen and helium atoms. The keyword can be either "2s2p" or "2p2s".

4.14.11 no Auger effect

This command turns off the Auger effect.

4.14.12 no Compton effect

This command turns off Compton heating and cooling of free electrons, and Compton recoil ionization of bound electrons. Electron scattering opacity *is not* turned off.

4.14.13 no fine structure line optical depths

Fine structure lines, such as the ³P 52, 88 μ m lines of O⁺², can become optically thick under certain high-luminosity conditions (see, for example, Rubin 1983). Radiative transfer effects, including stimulated and maser emission, are fully treated by CLOUDY for all fine structure lines, using escape probabilities. This command turns off the treatment of optical depths and line transfer for these lines.

4.14.14 no free free heating

Free free heating is turned off with this command. It sets the logical variable "FREEON" in the common block of the same name to false.

4.14.15 no induced processes

This command turns off induced recombination and stimulated emission for hydrogen and helium.

4.14.16 no ir pumping

This command turns off continuum pumping of infrared fine structure lines. This process can be an important heating mechanism for cool gas irradiated by a powerful infrared continuum.

4.14.17 no molecules

CLOUDY does a molecule formation network, initially based on Black (1978) and Hollenbach and McKee (1979) (see section 17.3. It includes H^+ , H^o , H^- , H_2 , H_2^+ , HeH⁺, and OH. A very brief description of the network and some results are given in Ferland (1980b). The "NO MOLECULES" command turns the network off.

4.14.18 no on the spot

This command turns on all ground state recombination coefficients, and turns off ionization by helium resonance lines. Specifically, it sets all hydrogen recombination efficiencies (in the vector HREFF(n,2)) to unity, and sets OTSMIN to 1. This last variable is then used to deduce the ionization efficiency of lines and continua; the effect of this command is to turn off such ionizations.

4.14.19 no radiation pressure

This command turns radiation pressure completely off. Radiation pressure due to trapped lines will be counted in the total pressure when the "CONSTANT PRESSURE" option is used; the default is for a constant density model. Radiation pressure is not included if constant gas pressure is specified. Acceleration due to the gradient of the radiation pressure is always included in the calculation of the radiative acceleration in "WIND" models, however, and this option turns off the extra acceleration due to trapped lines.

4.14.20 no recoil ionization

This command turns off Compton recoil ionization of hydrogen, helium, and heavy elements. Compton heating and cooling of free electrons is included, but is the only electron scattering thermal effect remaining. Bound electron scattering opacity is still included when this command is issued.

4.14.21 no secondary ionizations

This command will turn off the effects of knock-on supra-thermal electrons. Normally these are treated as in Spitzer and Tomasko (1968), Bergeron and Collin-Souffrin (1971), Shull (1979), and Shull and van Steenberg (1985). This command will make X-rays contribute 100% heat, and produce no secondary ionizations or $Ly\alpha$ excitations.

4.14.22 no Stark broadening

Stark broadening (important for densities larger than $\sim 10^{10}$ cm⁻³) is treated for hydrogen lines using escape probabilities from Puetter (1981). This turns Stark broadening off.

4.14.23 no three body recombination

This turns off three body recombination for the heavy elements. It is not possible to turn off three body recombination for hydrogen or helium.

5 OUTPUT

This section defines the output produced by CLOUDY.

5.1 Header Information

Several lines of output echo the input commands and outline some properties of the initial continuum.

5.1.1 Initial Information

This begins with the version number of CLOUDY. Major revisions, which have noticeable effects on the emission-line spectrum or which reflect significant improvements in the physics, are denoted by integer increases in the version number, while minor changes increment the revision number by 0.01. In a static version of the code, changes (usually bug fixes) are denoted by letters (i.e., .02a). The following line gives the date this version was created.

All of the input command lines, with the exception of those starting with a "#", "%", or "*", are echoed before the calculation begins, and the first twelve lines are saved to be reprinted after the calculation is completed. The input information is followed by the chemical composition of the gas. The numbers are the number density of the elements, relative to hydrogen.

5.1.2 Properties of the Continuum

This section gives a synopsis of the incident continuum. These quantities are evaluated at the illuminated face of the cloud, not in the center of the first zone. The first line gives the number of numerical frequency cells in the continuum, followed by the energy (in Ryd) of the cell with the largest flux density per unit energy interval (f_{ν}) . Next are the energies of the low and high energy limit of the continuum, both in Ryd and cm or MeV. The last two numbers are the energies of the high energy limit of the present version of the code, in Ryd and keV.

The second line gives the log of the energy (erg s⁻¹ cm⁻² or erg s⁻¹, depending on whether a flux or luminosity was specified) in the hydrogen ionizing continuum (1 Ryd $\leq h\nu < 100$ MeV), and the average energy of the hydrogen ionizing continuum, in Ryd, weighted by photon number;

$$\langle h\nu \rangle = \frac{\int_{1Ryd}^{\infty} 4\pi J_{\nu} \, d\nu}{\int_{1Ryd}^{\infty} 4\pi J_{\nu} / h\nu \, d\nu} \quad . \tag{43}$$

The log of the energy in the "X-ray" continuum (20.6 Ryd $\leq \nu \leq$ 7676 Ryd), the log of the energy (erg s⁻¹ cm⁻² or erg s⁻¹), and the number of photons (cm⁻² s⁻¹ or s⁻¹) in the Balmer continuum (0.25 Ryd – 1.0 Ryd) is then printed.

The third line gives the log of the number of photons $(\text{cm}^{-2} \text{ s}^{-1} \text{ or s}^{-1})$ in four frequency bins (1.0 Ryd $\leq \nu < 1.807$ Ryd, 1.807 Ryd $\leq \nu < 4.0$ Ryd, 4.0 Ryd $\leq \nu < 20.6$ Ryd, and 20.6 Ryd $\leq \nu < 7676$ Ryd). The last number is the flux of hydrogen ionizing photons;

$$\phi(H) = \frac{Q(H)}{4\pi r^2} \ cm^{-2} \ s^{-1} \ . \tag{44}$$

In this equation Q(H) is the total number of hydrogen-ionizing photons emitted by the central object (s⁻¹), and r is the separation between the center of the central object and the inner face of the cloud. Unlike the majority of the quantities printed in the header, $\phi(H)$ (per unit area) is always printed, never Q(H) (into 4π sr).

The fourth line of the header gives some information about the low and high energy portions of the incident continuum. The first number is the log of the luminosity in the gamma-ray (h $\nu > 7676$ Ryd ~ 100 keV) continuum. The second number on the line is the log of the number of photons over this energy range. The third number is the log of the luminosity in the continuum between 0.25 Ryd and the lowest energy considered, presently an energy of 1.001×10^{-5} Rvd. All of these entries are either per unit area, or radiated into 4π sr, depending on how the continuum was specified. The next entry is the spectral index α_{ox} , defined as in Zamorani et al. (1981), except for the difference in sign convention. This is the spectral index which would describe the continuum between 2 keV and 2500Å if the continuum could be described as a single power-law. The definition of α_{ox} used here is slightly different from that of Zamorani et al. since implicit negative signs are never used by CLOUDY. Typical AGN have $\alpha_{ox} \sim -1.4$. If no X-rays are present then $\alpha_{ox} = 0$. The last number on the line is the log of the total energy in the continuum between 1.001×10^{-5} Ryd and 100 MeV; it is given as either erg $\rm cm^{-2} \ s^{-1}$ or erg $\rm s^{-1}$, depending on how the continuum was defined. If the continuum is specified per unit area, then this number is 4π times the integrated intensity of the incident continuum. If it is specified as the total luminosity radiated into 4π sr, then the quantity is the luminosity.

The next line is optional, depending on whether the continuum is specified as the total luminosity or photon number radiated into 4π sr, or as an incident surface flux. If the continuum is specified in absolute terms, i.e., the luminosity or photon number radiated into 4π sr, then this optional line is generated. The first quantity is the log of the total luminosity in the continuum, in solar units. The absolute bolometric magnitude, absolute V magnitude, and the bolometric correction, are then given, followed by the log of the continuum specific luminosity (νF_{ν}) at H β ($\nu F_{\nu}(H\beta)$; erg s⁻¹).

5.2 Zone Results

The next line begins with two ionization parameters. The first is the dimensionless ratio of ionizing photon to hydrogen densities, defined as

$$U \equiv \frac{\phi(H)}{N_H c} \tag{45}$$

where N_H is the total hydrogen density. The second number is defined in a similar way, but the numerator is the number of photons with energies greater than 4 Ryd (i.e., helium-ionizing). The third number is the equivalent black body temperature corresponding to the energy density u at the illuminated face of the cloud [from the incident continuum and Stefan's radiation density constant a; $T_u \equiv (L/4\pi r^2 ac)^{1/4}$], and the next quantity is the Compton temperature of the incident radiation field⁸. The last number on the line is $4\pi\nu J_{\nu}(912\text{\AA})$, the flux at 912Å (erg cm⁻² s⁻¹). In this equation J_{ν} is the mean intensity of the incident continuum as defined by Mihalas (1978).

The next two lines give the incident continuum photon occupation numbers $\eta(\nu)$, defined as

$$\eta(\nu) \equiv J_{\nu} \left(\frac{2h\nu^3}{c^2}\right)^{-1} \quad , \tag{46}$$

and the incident continuum brightness temperature $T_b(\nu)$, (^oK), defined as

$$T_b(\nu) \equiv J_\nu \left(\frac{2k\nu^2}{c^2}\right)^{-1} \quad , \tag{47}$$

for five energies. These energies correspond to the lowest frequency considered (presently an energy of 1.001×10^{-5} Ryd); the ionization potential of the n = 6 level of hydrogen (1/36 Ryd); an energy of one Rydberg; four Rydbergs, and the high energy limit of the incident continuum (this depends on the continuum shape; the energy is given by the fifth number on the first line of the continuum output).

Finally, if grains are present, then the last line gives the total grain extinction (scattering and absorption) cross section (cm⁻²) per unit column density of hydrogen at several energies (P α , B α , Mg II, 1 Ryd, 4 Ryd).

5.2 Zone Results

The results of calculations for the first and last zones are always printed. Results for intermediate zones can be printed if desired (see the "PRINT EVERY" command above). The following is a line-by-line description of the output produced for each printed zone.

⁸For a blackbody radiation field $T_{Compton}$ is roughly 4% lower than the blackbody color temperature T_{color} when the energy density temperature T_u is $\ll T_{color}$. Only when $T_u \equiv T_{color}$ does induced Compton heating cause $T_{Compton} \equiv T_{color}$. If $T_u > T_{color}$ then $T_{Compton} > T_{color}$ because of induced Compton heating. All of the relevant physics is included in the Compton temperature printed here.

5.2.1 Line 1

The line begins with five "#" characters, to make it easy to locate with an editor. The zone number is the first number, followed by the temperature of the zone ("Te"). A lower case "u" will appear before the "Te" if the temperature solution is possibly thermally unstable (i.e., the derivative of the net cooling with respect to temperature is negative. See section 20.2 below). The total hydrogen ("Hden") and electron ("Ne") densities (cm⁻³) follow. The next number ("R") is the distance to the center of the zone, from the center of the central object. The depth, the distance between the illuminated face of the cloud and the center of the zone, $(r - r_o)$, and the width of the zone dr, (all are in cm), follow. The line ends with a number indicating how many iterations were needed for this zone to converge ("NTR"), followed by the total heating⁹ ("Htot"; photoelectric and otherwise, erg cm⁻³ s⁻¹), and the optical depth between the *inner* face of the cloud and the *outer* edge of the zone at the Lyman limit ("T912"; the number is the *total absorption* optical depth at 912Å, and *not* the hydrogen Lyman limit optical depth).

5.2.2 Line 2 - Emission-line strengths

The first number is the log of the surface brightness in H β (erg cm⁻² s⁻¹). The remainder of the numbers are ordered pairs, with the first being the wavelength of an emission line, and the second its intensity relative to H β . All of these are the intensities accumulated so far, with the present zone included. The selection of lines is arbitrary, and the last can be changed with the "LINE" command. This information is useful when dealing with a matter-bounded geometry, in which the emission-line intensities are set by the thickness of the cloud.

5.2.3 [Optional] wind parameters

A line describing the velocity and acceleration of the zone is printed if the "WIND" option is used. The numbers are the wind velocity at the inner edge of the zone (km s⁻¹), inward gravitational acceleration (cm s⁻²), total outward radiative acceleration, and the fraction of this acceleration caused by the incident continuum, line driving, and the gradient of the radiation pressure. The solution is probably not realistic for grain-free environments, since ~ 10⁶ lines need to be included to do radiative acceleration properly (Abbott 1982).

⁹CLOUDY defines heating as the energy input by the freed photoelectron, or $h\nu - IP$, where *IP* is the ionization potential of the atom or ion, and $h\nu$ is the energy of the photon. See Osterbrock (1988) for more details.

5.2.4 [Optional] radiation pressure

If the ratio of line radiation to gas pressure, P(radiation)/P(gas), is greater than 5%, then a line describing the source of the radiation pressure is generated. The printed line is the vector which contains the contributors to P_{rad} , and are in the order (1)=Ly α , (2)=Mg II λ 2798, (3)=C III λ 1909, (4)=Fe II UV lines, (5)=C IV λ 1549, (6)=C II λ 1335, (7)=n > 2 Lyman lines, (8)=Balmer lines, (9)=He I λ 10830, (10)=HeII Ly α , (11)=HeI Ly α , (12)=N III λ 1750, (13)=O III λ 1666, (14)=SI III λ 1207, (15)=SI III λ 1895, (16)=SI IV λ 1397, (17)=S III λ 1198, (18)=O VI λ 1035, and (19)=N V λ 1240. The numbers are the fraction of the total radiation pressure contributed by each line. Usually, the majority of the line radiation pressure comes from Ly α , C IV λ 1549, Mg II λ 2798, or the Fe II UV lines.

5.2.5 Line 3 - Hydrogen I

The line begins with the abundance of neutral and ionized hydrogen relative to all atomic-ionic hydrogen (i.e., the ratios $H^{o}/(H^{o}+H^{+})$ and $H^{+}/(H^{o}+H^{+})$. If "PRINT DEPARTURE COEFFICIENTS" has been specified then departure coefficients are also printed on the following line. Neutral hydrogen H^{o} is defined to be the total population of atomic hydrogen in the $1 \leq n \leq 6$ states. Ionic hydrogen includes the sum over higher levels and protons. Next comes the ratio "H+-/Hden", the ratio of the density of hydrogen in atomic or ionic form to the total hydrogen density in all forms (including molecular).

The following five numbers are abundances of the negative hydrogen ion and several molecules (H⁻, H₂, H₂⁺, and HeH⁺) relative to the total hydrogen abundance. The total hydrogen density is usually referred to by the label HDEN, and is the sum $H^{\circ} + H^{+} + H^{-} + 2H_{2} + 2H_{2}^{+} + 3H_{2}^{+}$. Note that, with the definition of HDEN given here, a fully molecular gas will have H₂/HDEN=0.5. These molecular abundances are also expressed as departure coefficients if this option is set. The last number on the line is the total hydrogen column density (cm⁻²).

5.2.6 Line 4 - Hydrogen II

The first two numbers are the populations of the H^o 2s and 2p levels relative to the ionized hydrogen density. The next four numbers are populations of levels 3 to 6, again relative to the ionized hydrogen density. The latter are computed assuming full l-mixing. The populations of three pseudo-states, chosen to represent the actual levels 7 - 100, are also computed, but not printed. All of these populations usually are relative to the ionized hydrogen density, but can also be printed as LTE departure coefficients if the "PRINT DEPARTURE COEFFICIENTS" command is given. The

excitation temperature T_{exc} of $Ly\alpha$, defined as

$$\frac{N(2p)/g(2p)}{N(1s)/g(1s)} = \exp\left(-h\nu/kT_{exc}\right) \quad , \tag{48}$$

is given. This is followed by the temperature corresponding to the energy of the attenuated incident continuum ("T(contn)"), and the "diffuse" continua ("T(diffs)". This includes all trapped lines and diffuse continuous emission.

5.2.7 Line 5 - Helium

The first three numbers are the total populations of the three ionization stages of helium, relative to the total helium abundance. The population of atomic helium is the sum of the total population in the triplets and singlets, including the population of the lowest six levels of each. These populations can also be expressed as departure coefficients if this option is set with the "PRINT DEPARTURE COEFFICIENTS" command. The population of He^o 2³S, relative to the total helium abundance, follows. The Compton heating and cooling rates (both erg cm⁻³ s⁻¹) are next, followed by the gas filling factor. The last number is the fraction of the total hydrogen ionizations which are caused by photoionization from the ground state.

5.2.8 Line 6 - Atomic Helium

The first group are the level populations of the 2s, 2p, and n=3-6 levels of the He^o singlets. The next group consists of populations of the 2s, 2p, and n=3s,p,d levels of the He^o triplets. Both sets of populations are relative to He⁺. Departure coefficients are also printed if requested.

5.2.9 Line 7 - Ionized Helium

The populations of the 2s, 2p, and n=3-6 levels are indicated. There are relative to He^{++} ; departure coefficients are also printed if requested. The ratio of radiation pressure to gas pressure follows.

5.2.10 Optional Grains

If grains are present, then lines giving some properties of the grain populations are printed. Each line gives the results of calculations for a specific type of grain. Normally, a type of graphite and silicate are included when grains are present. The line for each type gives the equilibrium temperature of the grain, the potential in volts, the charge, the drift velocity, followed by the gas heating (erg cm⁻³ s⁻¹) due to grain photoionization, and the dimensionless fraction of the total gas heating due to grain photoionization.

5.2.11 Pressure

Some information concerning the pressure is now printed. The gas equation of state includes thermal gas pressure, the radiation pressure due to trapped line emission, and the radiation pressure due to absorption of the incident continuum. The first number is the gas pressure $N_{gas}T_{gas}$ (cm⁻³ K), followed by the total pressure (dynes cm⁻²), followed by the gas pressure in dynes cm⁻². The radiation pressure follows. The second to last number is the radiative acceleration (cm s⁻²) at the inner edge of this zone. The radiative acceleration is computed with all continuous scattering and absorption opacities included, and opacities of roughly ten lines treated in the escape probability formalism. (Work on OB winds suggests that this result is a serious underestimate for grain-free environments. See, for instance, Abbott 1982.) The last number is a "force multiplier", defined as in Tarter and McKee (1973), and is the ratio of total opacity to electron scattering opacity.

5.2.12 Molecules

A line giving relative abundances of some molecules is printed if there is a significant molecular fraction. All molecular abundances are relative to either the total carbon or total oxygen abundance (this is indicated in the label for each). In order, the molecules are CH, CH⁺, CO, CO⁺, H₂O, and OH.

5.2.13 Carbon

The abundances of the seven stages of ionization of carbon relative to the total carbon abundance begin the line. The relative abundance of H_2O^+ and OH^+ (relative to the total oxygen abundance) follows.

5.2.14 Nitrogen

The relative populations of the eight ionization stages of nitrogen are printed first. The relative abundance of O_2 and O_2^+ (relative to the total oxygen abundance) follows.

5.2.15 Oxygen

The oxygen ionization stages are followed by the "extra" heat added at this zone (erg $cm^{-3} s^{-1}$); due to cosmic rays, turbulence, etc, and the log of the effective hydrogen recombination coefficient (cm³ s⁻¹).

5.2.16 Neon

The neon ionization balance is printed across the line.

5.2.17 Magnesium to Iron

There are too many ionization stages to print across the line. Although all stages with non-trivial abundances are computed, only the highest twelve stages of ionization are printed. The first number is an integer indicating how many stages are "off the page to the left". If the number is 2, then the first printed stage of ionization is twice ionized, i.e., Fe⁺².

5.3 Calculation stopped because ...

A series of messages appear after the printout of the last zone.

The first will say why the calculation stopped. In a valid calculation the model will stop because one of the specified stopping criteria specified were met. If no other criteria are specified, then the calculation usually stops when the default lowest temperature of 4000K is reached. If the code stops because of a probably unintended reason (i.e., internal errors, or the default limit to the number of zones) then a note is printed saying that the calculation may have halted prematurely.

The first line explains why the calculation stopped. Only one stopping criterion message will be printed. The possible messages, and their interpretations, are:

5.3.1 ... because of radiation pressure

The default density law is for a constant density. If constant pressure is specified instead (with the "CONSTANT PRESSURE" command), then CLOUDY will try to keep the total pressure, particle and radiation, constant. The radiation pressure is small at the boundaries of the cloud, so the cloud will be unstable if the ratio of radiation to total pressure exceeds 0.5. The calculation stops, and this message is generated, if this occurs on the last iteration.

5.3.2 ... because lowest EDEN reached.

The calculation can be forced to stop when the electron density ("EDEN") falls below a certain value, as set by the "STOP EDEN" command, described above. This can be used to stop the calculation at an ionization front. The default lowest electron density is negative, so this stopping criterion applies only when the command is entered.

5.3.3 ... because low electron fraction.

The calculation can be forced to stop when the ratio of electron to hydrogen densities falls below a certain value, as set by the "STOP EFRAC" command, described above. This can be used to stop the calculation at an ionization front when the hydrogen density there is not known (for instance, in a constant pressure model). The default lowest electron density is negative, so this stopping criterion applies only when the command is entered.

5.3.4 ... because wind velocity < 0

The code can perform a simple wind calculation (see section 22.4) which includes the outward force due to radiation pressure and the inward force of gravity. This message is printed if the gas comes to rest.

5.3.5 ... because DRAD small - set DRMIN

The Strömgren radius of the H^+ zone is estimated at the start of the calculation, and the smallest allowed zone thickness is then set as a very small fraction of this. The calculation will stop if the zone thickness falls below this smallest thickness. This can occur because of any of several logical errors within CLOUDY (adaptive logic is used to continuously adjust the zone thickness), although it can rarely occur for physical reasons as well. The smallest thickness can be reset to any number with the "DRMIN" command, see above.

5.3.6 ... because DR small rel to thick.

The depth into the cloud is stored as the double precision variable DEPTH and the zone thickness is stored as the double precision variable DRAD . If the zone size becomes too small relative to the depth (DRAD/DEPTH< 10^{-14}) then the depth variable will underflow such that DEPTH+DRAD=DEPTH. The calculation will stop in this case and give the above reason. This is a fundamental numerical problem with no clear solution.

5.3.7 ... because optical depth reached.

The default value of the largest allowed continuous optical depth is unphysically large, and can be reset with the "STOP OPTICAL DEPTH ..." command. The command specifies both the optical depth, and the energy at which it is to be evaluated. All absorption opacity sources included in the calculation contribute to the computed optical depths. If the calculation stops because the largest continuum optical depth is reached, then this line is printed. This line is also printed if the "STOP EFFECTIVE COLUMN DENSITY" command is used to stop the calculation, since this command is actually a form of the "STOP OPTICAL DEPTH" command.

5.3.8 ... because outer radius reached.

The default outer radius is unphysically large, but can be changed with the "RADIUS" or "STOP THICKNESS" commands. If the calculation stops because the outer radius set by one of these commands is reached, then this line is printed.

5.3.9 ... because column dens reached.

The default values of the largest allowed neutral, ionized, and total hydrogen column densities are unphysically large. They can be reset with the commands "STOP COLUMN DENSITY", "STOP NEUTRAL COLUMN DENSITY", or "STOP IONIZED COLUMN DENSITY". This message will be printed if one of these criteria stops the calculation.

5.3.10 ... because lowest Te reached.

The default value of the lowest temperature allowed is 4000K. This is reasonable when only optical emission lines are of interest. The limit can be changed with the "STOP TEMPERATURE" command. This message is printed if the calculation stops because the lowest temperature is reached.

5.3.11 ... because NZONE reached.

The default condition is for up to 300 zones to be computed. This can be reset with the "STOP ZONE" command. This message is printed if the calculation stops because the limiting number of zones is reached. A comment will be printed at the end of the calculation if it stops because it hits the default limit to the number of zones allowed, presently 300, since this was probably not intended.

5.3.12 ... because line ratio reached.

It is possible to set a limit to the largest value of an emission-line intensity ratio with the "STOP LINE" command. This message is printed if the calculation stops because the largest value of the ratio is reached.

5.3.13 ... because internal error - DR.

An internal logical error caused this message to be printed. Send the command lines, and the version number of CLOUDY to me. My internet address is gary@bowen.mps.ohio-state.edu.

5.4 Geometry

After saying why the calculation stopped, CLOUDY will say whether the geometry is plane parallel ($\delta r/r_{in} < 0.1$), a thick shell ($\delta r/r_{in} < 3$), or spherical ($\delta r/r_{in} \geq 3$), where r_{in} is the inner radius and δr is the thickness of the cloud.

5.5 Warnings, Cautions, Surprises, and Notes

The next, optional, messages fall into four categories: warnings, which begin with "W-"; cautions, which begin with "C-"; surprising results which begin with an explanation mark ("!"), and notes. CLOUDY tries to check that its range of validity was not exceeded in the calculation. Warnings are issued to indicate that the program has not treated an important process correctly. For instance, warnings occur if the temperature was high enough for the electrons to be relativistic or if the global heating — cooling balance is off by more than 20%. Cautions are less severe, and indicate that CLOUDY is on thin ice. Examples are when the optical depths in excited states of hydrogen change during the last iteration. Surprises begin with "!" and indicate that, while the physical process has been treated correctly, the result is surprising. An example is when induced Compton heating is more that 5 percent of the total Compton heating. Notes indicate interesting features about the model, such as maser effects in lines or continua, or if the fine structure lines are optically thick. The messages are usually self explanatory.

5.6 Optional Plot

If any of the optional plots are requested with the "PLOT xxx" command then they will appear next. The quantities plotted are described in the section of HAZY where the command is defined.

5.7 Final Printout

5.7.1 Emission-Line Spectrum

The final printout begins by reprinting the input commands. The box surrounding it gives both the version number of CLOUDY (at the top) and the log of the ionization parameter (the ratio of ionizing photon to hydrogen densities) at the bottom.

The line following the box summarizes some properties of the model and output. The first part of the line indicates whether the energy in the emission lines is given as the luminosity radiated by a spherical shell covering Ω sr (erg s⁻¹; $\Omega/4\pi$ is the covering factor) or the intensity produced by a unit area of gas (erg s⁻¹ cm⁻²). Which of the two choices is printed is determined by whether the luminosity of the continuum was

specified as the luminosity radiated by the central object into 4π sr or the intensity of the incident continuum (erg cm⁻² s⁻¹) at the illuminated face of the cloud. If the model is spherical and the incident continuum specified per unit area, then the emergent emission-line spectrum will be per unit area in units of the inner radius (that is, the total line luminosity radiated by a shell covering 4π sr will be the listed intensity $4\pi j$ times $4\pi r_{inner}^2$). The second part of this line indicates the density structure of the model (i.e., wind, constant density, constant pressure, constant gas pressure, power-law density distribution, etc). The next section tells whether the geometry was open or closed. The last part indicates which iteration this is.

The computed emission-line spectrum follows. Emission lines are divided into two groups. The first includes the effects of grain scattering and absorption, and is indicated by the header "Emergent Line Intensities". This first group is only printed if grains are present and the geometry is open (i.e., "SPHERE" not set). The intensities are the *total* intensities observed from the illuminated face, including both absorption and scattering by grains. The second group of lines is always printed, is usually the intrinsic intensity of the lines, and does not include the reddening effects of internal grains due to the photon's passage out of the nebula. This second group usually gives the total intrinsic intensity of the lines. Although reddening effects of internal (or external) dust are not taken into account, although photon destruction by background opacity sources during the transfer process is.

The spectrum is sorted into four large groups of columns, with each large group sub-divided into four smaller sub-columns. The first sub-column is either the spectroscopic designation of the ion producing the line or an indication of how the line is formed. The second sub-column is the line wavelength, with a 0 to indicate a continuum. The third sub-column is the log of the power in the line, in the units given in the header $(4\pi \text{ sr or cm}^{-2})$. The last sub-column is the intensity of the line relative to the reference line, usually H β , unless this is reset with the "NORMALIZE" command.

The following sections give overviews of the general treatment of line formation. A description of the entire line array, and a formal definition of how CLOUDY works, follows in latter sections.

Heating and cooling The total photoelectric heating, due to photoionization of hydrogen, is given by "BF H". The following entries, "BFHe", and "TotM", are the heating due to helium and metal photoionization. "ComH" and "H-H", indicate the heating due to Compton scattering and absorption by the H⁻ ion. "Comp 0" is the total cooling due to Compton scattering, and "eeff 0" is the electron-electron bremsstrahlung cooling. "H FB" and "H FF" are the free-bound and free-free cooling of hydrogen.

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Hydrogen lines The first two entries are the total intensities of $H\beta$ and $Ly\alpha$, as predicted by the 10-level H atom. These intensities are the results of calculations which include all collisional, radiative, and optical depth effects. The next ("CA B 4861") is the case B intensity of $H\beta$, computed from the actual model ionization and temperature structure, but assuming that $H\beta$ emits with its case B emissivity. "DU B 4861" is the case B intensity of $H\beta$ modified for grain destruction of Lyman lines, as described by Cota and Ferland (1988). For models of dusty low-density gas, such as an H II region, where collisional and radiative transfer effects are not important, this entry should be more reliable than the results of the ten level atom calculation when case B is a good assumption. The two may differ at the ~ 2% level. The entry "Q(H) 4861" is the intensity of H β predicted from the total number of ionizing photons, Q(H), assuming that each hydrogen-ionizing photon produces one hydrogen atom recombination (see, for example, Osterbrock 1988). "Q(H) 1216" indicates the Ly α intensity produced if each hydrogen ionizing photon results in one Ly α photon in the high density limit (i.e., no two-photon emission).

The lines starting with "TOTL" are the total intensities of the indicated lines, predicted by the 10-level atom, including all physical processes. A few of the entries suggest different contributions to the "TOTL" hydrogen lines. "LA X 1216" is an estimate of the intensity of Ly α produced by excitation of n = 2 by suprathermal electrons. "C 13 6563" and "C 14 4861" are the intensities of these Balmer lines 0" is the net produced by collisional excitation from the ground state. "CION cooling due to collisional ionization of hydrogen, and "2 NU 0" is the total two photon emission. The lines beginning "Strk" and "e sc" are the contributions to the lines from Stark broadening and electron scattering. "nFnu 4861" is the total diffuse continuous emission $\nu f_{\nu}(4861\text{\AA})$ at the wavelength of H β . This continuum includes two-photon, free-free, and free-bound emission from the nebula. "BA C 0" and "PA C 0" are the integrated intensities of the Balmer and Paschen continua respectively. The entries beginning with "rest" and "COOL" are indications of the cooling due to various sets of H lines. Entries marked "INWD" indicate the intensity of the fraction of the line emitted in the inward direction (that is, towards the source of ionizing radiation). This is only meaningful on second or later iterations.

Molecular cooling "H2 1 2" is the intensity of the H₂ lines near 2 μm , and "H2 d" is the cooling due to collisional dissociation of H₂. "H-FB" and "H-FF" are the free-bound and free-free continua of the H⁻ ion. "H2+" and "HEH+" are the cooling due to formation of H₂⁺ and HeH⁺.

Helium lines Ionized and singlet helium are each treated as ten-level atoms. Triplet helium is currently treated as an five level atom.

"HE I 4471" is the case B intensity of this He I line. "TOTL 5876" is the intensity of this line, as predicted by the model helium atom. "Ca B 5876" is the case B intensity of this line. This second entry is generally smaller than the "TOTL" intensity because of collisional excitation from 2^3S . "TOTL10830", "TOTL 3889", and "TOTL 7065" are the intensities of these lines, predicted by the model helium atom. "C HE 0" is the total cooling due to collisional excitation within the helium atom. "He I 2" and "DevB 2" are intensities of the $2\mu m$ He I line. The first is the case B prediction, and the second is the actual intensity. This was computed using expressions from Cota (1987; PhD Thesis). "He I-DevB" etc are sets of lines, the first being the case B intensity, and the second the actual intensity (the deviation from case B included). "HE2C 304" and "ESC r 304" are the produced and emitted intensities of the He II Ly α . "HeII 1640", 4686 are intensities from case B calculations. In general, case B is probably more accurate for HeII emission than the results of the present 10-level atom, because of the assumption of complete l-mixing. The entries marked "TOTL" are more accurate at high densities $(N \gg 10^8 \text{ cm}^{-3} \text{ or when collisional or})$ transfer effects are important.

Heavy elements A few notes on deciphering the heavy element lines follow. A more complete discussion is presented in section 6. In cases where the notation is unclear a careful examination of subroutine "LINES" (which enters the line fluxes into the arrays) or "COOLR" (which actually calculates the line intensities) should clarify the meaning. In general, the line wavelengths are given in Å, although the infrared fine structure lines are an exception. Often these IR lines have their wavelength given in microns (for instance, [O III] $\lambda 88 \ \mu m$), but sometimes it is given in microns or tenths of microns (this is because the wavelengths are integers). Notes on specific iso-electronic sequences follow.

Li - sequence. Examples include $C IV \lambda 1549$, $O VI \lambda 1034$, $Mg II \lambda 2798$, etc. A two level atom, with full treatment of optical depths and collisional excitation, is used. The intensity is the sum of both lines in the doublet.

Be - sequence. Examples include C III] $\lambda 1909$, O V] $\lambda 1215$, Si III] 1895, etc. A four level atom, solving for populations of the individual ${}^{3}P_{j}$ states, is used. The first printed intensity is the total intensity of the multiplet (both j=0,1 decays), and this is followed by the intensities of individual lines. The intensity of the permitted ${}^{1}P_{o}-{}^{1}S$ transition is also calculated. Optical depth and collisional effects on both the permitted and intercombination lines are included.

B-sequence. Examples include C II and O IV. The ground term is treated as a two level atom, with optical depth and collisional effects included. The ${}^{4}P{}^{-2}P_{o}$ lines are also predicted with a two level atom. The intensity printed is the total intensity of the multiplet.

 ${}^{3}P-ground term$. Examples include [O III] and [O I]. The infrared fine

structure lines are computed with full treatment of collisional and optical depth effects. A comment is printed at the end of the model if these lines mase or become optically thick. The populations of ${}^{1}D$ and ${}^{1}S$ are computed with a three-level atom. The intensity of the ${}^{1}D - {}^{3}P$ transition is only that of the individual line (i.e. 5007), not the doublet.

 ${}^{4}S^{o} - ground term$. Examples include [O II] and [S II]. They are treated as a five level atom. Intensities of all individual lines, as well as co-added multiplets, are given.

5.7.2 Page two

Cooling: This line indicates the fraction of the total cooling (defined here as in Osterbrock 1988; that is, the energy of the freed photoelectron) carried by the indicated emission lines. The designation of the line is given as in the emission-line spectrum, and this is followed by the ratio of the energy in the line to the total cooling. This is an important indication of the fundamental power-losses governing conditions in the model.

Heating: This line indicates the fraction of the total heating produced by various processes.

IONIZE PARMET to He/Ha The first line begins with the log of the two ionization parameters defined in the header. The next number is the log of an ionization parameter which is often used in spherical geometries, such as H II regions or planetary nebulae. It is defined as

$$U_{sph} = \frac{Q(H)}{4\pi R_s^2 N_H c} \tag{49}$$

where R_s is the Strömgren radius, defined as the point where the hydrogen neutral fraction falls to $H^{\circ}/H_{tot} = 0.5$. If no ionization front is present, then U_{sph} is evaluated at the outer edge of the computed structure. The next two numbers are the log of the number of hydrogen ionizing photons ($h\nu \ge 1$ Ryd) exiting the nebula, and the log of the energy in this ionizing continuum. The last two numbers are the equivalent quantities, for non-ionizing ($h\nu < 1$ Ryd) radiation. These are either per unit area or by a shell covering 4π sr. These have been corrected for the r^{-2} dilution if per unit area, are so are directly comparable with the numbers given at the start of the calculation.

The second line gives an indication of the energy budget of the nebula. The first number is the log of the total heating (in ergs s⁻¹, but again either into 4π sr or cm⁻²). The second number is the total cooling, in the same units. Cooling, as defined in Osterbrock (1988), is the total energy in collisionally excited lines and part of the

recombination energy, but *does not* include recombination lines. The percentage error in the heating–cooling match follows. The next number is the total Compton heating, in the same units as the heating-cooling balance. The number indicated by "WorkF" is an indication of the "work function" (that is, the energy needed to remove bound electrons from the atom or ion) of the cloud. (The "work function" and the total cooling do not add up to the total energy absorbed from the incident continuum because some recombination lines of helium and heavy elements contribute to both.) The next number ("F-F H") is the amount of energy deposited by free-free heating, and the last number (PRADMX) is the largest value of the ratio of radiation to gas pressure which occurred in the calculation.

The third line lists the column densities (cm^{-2}) of some ions and molecules. The first number ("H12") is the total hydrogen column density (both H^o and H⁺). The following two numbers are the column densities in H⁺ and H^o only. The last four numbers are column densities in four ion-molecules (H⁻, H₂, H₂⁺, and HeH⁺). The first number on the next line is the column density in OH, and the second is the "effective" column density; that needed to attenuate the incident continuum by the calculated amount at 1.0 keV, if the absorber were cold neutral gas.

The 5th line gives some average quantities. The first is the mean hydrogen density (cm^{-3}) . The next number is the mean electron temperature, weighted by the H⁺ density. The third number is the mean temperature of the O²⁺ zone. This is useful because it can be compared directly with the temperature indicated by the [O III] lines. The 4th number is the mean electron density, and is followed by the sound travel time (seconds) across the nebula. The 6th number is the emission measure, the integral over radius of the product $N_e N_p f dr$, where f is the filling factor. The last two numbers on this line are the mean electron temperature and electron density, weighted with respect to the C²⁺ density.

The next line mainly gives some quantities "deduced" from the predicted emission-line spectrum. The first ("He/Ha") number is the apparent helium abundance He/H, measured from the emission-line intensities using techniques similar to those described in Osterbrock (1988). The second number (i.e., "1.07*true"), is the ratio of this deduced abundance to the true abundance. The next two numbers are the apparent N/O abundance (deduced from the [N II] and [O II] spectra, as described by Wilkes et al. 1981) and the ratio of this to the true N/O abundance. The fifth number is the electron temperature of the [O III] zone, as indicated by the [O III] 5007/4363 ratio assuming emissivities at the low-density limit. The next number is the wavelength (in cm) where the nebula becomes optically thin to bremsstrahlung absorption. The last two numbers are the mean temperature and electron density of the S⁺ zone.

The next line gives mean temperatures and electron densities for the He⁺ and O⁺ zones. The next number is the average number of iterations needed to converge each zone. The next two numbers are the lowest and highest electron temperatures which

5.7 Final Printout

occurred in the model. The last number is related to the number of iterations needed to converge each zone.

The next line of the block gives the mean radiative acceleration, if the geometry is a wind model, followed by some timescales. The first is the time scale (s) to photoerode Fe (Boyd and Ferland 1987; this number is 0s if the γ -ray flux is zero). The next two are the Compton equilibrium timescale, and the thermal cooling timescale. Both are in seconds. The density weighted mean temperature, radius weighted mean density (gm cm⁻³), and mean molecular weight follow.

The next line gives the mean Jeans length (cm) and Jeans mass (in solar units), followed by the smallest Jeans length and mass which occurred in the calculation. The last quantity is the spectral index α_{ox} , defined as in the header, but for the transmitted continuum (attenuated incident continuum plus emitted continuum produced by the cloud).

The next, optional, lines give some information concerning grains in the calculation. These lines give the mean temperature, drift velocity, and potential, for all of the grain populations included in the calculation.

Optical Depths The first two lines give the optical depth of the nebula in various continua. These are the total optical depths, including the correction for stimulated emission, and will be negative if maser action occurs. The labels, and their interpretation, follows: COMP, Thomson scattering; H-, negative hydrogen ion at maximum cross section; R(1300), Rayleigh scattering at 1300Å; $H2^+$, H_2^+ ; HeTri, helium triplets. These are total optical depths, including, for instance, grain opacity if grains are present. The next line gives total optical depths for various hydrogen and helium ionization edges and lines. The next two large blocks are sets of optical depths in various emission lines, and the last set of lines are optical depths in the infrared fine structure lines.

Hydrogen and helium optical depths in continua and $n \rightarrow n-1 \alpha$ transitions follow. The first two lines are the optical depths assumed at the start of the present iteration, and the second pair of lines gives the newly computed total optical depths. Negative optical depths indicate maser action. For each of the pairs of lines, the first line is the optical depth at thresholds of the first seven levels of hydrogen. The second line gives optical depths in the first seven n- α transitions of hydrogen or helium.

Mean Ionization The two large blocks of output give the mean ionization, averaged over volume, and over radius. The numbers printed are the log of the mean ionization fraction in the various stages.

X-Ray Continuum The next line gives the photon fluxes $(cm^{-2} s^{-1})$ in various X-ray bands, if the continuum extends to X-ray energies. The units of the energy bands are keV. The numbers are the numbers of photons exiting the cloud, integrated over the energy bands. This is the net continuum, that is, the incident continuum, less attenuation, with diffuse re-emission from the cloud added on.

Normalized Continuum This block is a set of ordered pairs giving the emergent Balmer continuum, relative to the continuum which entered the cloud. The first number of each pair is the frequency in Rydbergs. The second is the ratio of the emergent continuum to the incident continuum (i.e., that which went into the cloud). In the absence of optical depth or diffuse emission effects, this block will be equal to 1.000 throughout.

Emergent Continuum This block gives ordered pairs of energy (in Rydbergs) and the emergent continuum. It is expressed as photon fluxes (phot $\text{Ryd}^{-1} \text{ cm}^{-2}$) corrected for r^{-2} , so as to be directly comparable with the continuum which went into the cloud.

Lyman continuum The last block of information gives the intensities of some of the emergent diffuse fields, and is only printed for open geometries. The first part is the energy in Rydbergs and the log of the product νf_{ν} for the Lyman continuum emerging from the illuminated face of the cloud (the side towards the central source of ionizing radiation). The number of Lyman continuum photons and the total energy in the Lyman continuum is then given. The end of the block gives the inward and outward diffuse fields in the Lyman, Balmer, and Paschen continua. These numbers are only meaningful for a plane parallel geometry.

6 THE EMISSION LINES

Description

Label λ

This section gives a complete list of all emission lines predicted by CLOUDY. In the following, the first column gives the four character label printed in the final array listing and the second column gives the wavelength of the line. The latter is usually in Å, although some fine structure lines are given in microns or tenths of microns, and continua are usually indicated by a wavelength of zero. The next item indicates whether the entry is a heat source (indicated by "h"), a coolant ("c"), or an intensity entered for information only ("i"). The last column of the table gives a brief description of the meaning of the line prediction. More information about individual lines can usually be had by examining the comments associated with the actual calculation of the line strength (in subroutine COOLR) or in subroutine LINES, where the line intensity is entered into the storage array.

The Emission Lines

Laber			Description
TOTL	4861	i	total H-beta from 10-level atom
TOTL	1216	i	total Ly-a from 10-level atom
TotH	0	i	total heating, all forms, information since individuals added later
BFH1	0	h	hydrogen photoionization heating, ground state only
BFHx	0	h	hydrogen photoionization heating, all excited states
BFHe	0	h	total helium photoionization heating, all stages
TotM	0	h	total heavy element photoionization heating, all stages
FF H	0	h	total free-free heating
ComH	0	h	Compton heating
H- H	0	h	H- heating
H-Hc		с	induced H- cooling
GraH	-	h	gas heating by grain photoionization
GraC		с	gas cooling by grain collisions
extH		h	"extra" heat added to this zone, from HEXTRA command
extC	0	с	"extra" cooling added to this zone, from CEXTRA command
pair	0	h	heating due to pair production
CA B	4861	i	H beta recombination, assuming case B
CA B	1216	i	case b intensity of Ly-alpha, no two photon
DU B	4861	i	simple H-beta, corrected as per Cota and Ferland 1987
Q(H)	4861	i	H-beta computed from $Q(H)$ and specified covering factor
Q(H)	1216	i	Ly-alpha from $Q(H)$, high-dens lim, specified covering factor
TOTL	6563	i	H-alpha emission from 10-level atom
TOTL	4861	i	H-beta emission from 10-level atom
TOTL	4340	i	H-gamma emission from 10-level atom
TOTL	4102	i	H-delta emission from 10-level atom

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P-alpha emission from 10-level atom
TOTL 12818 i
              P-beta emission from 10-level atom
TOTL 10938 i
             P-gamma emission from 10-level atom
TOTL 40512 i
             5-4 emission from 10-level atom
TOTL 26252 i
             6-4 emission from 10-level atom
TOTL 74578 i
              6-5 emission from 10-level atom
2 NU Oi
              2-photon emission from 10-level atom
TOTL 1216 i
             Ly-alpha from 10-level atom
TOTL 1026 i
             Lyman beta is special because of OI fluorescense
TOTL 973 i
             Ly-gamma emission from 10-level atom
TOTL 950 i
             Ly-delta emission from 10-level atom
TOTL 938 i
             Ly-epsilon emission from 10-level atom
LA X 1216 i
              la contribution from suprathermal secondaries
Ind2 1216 i
             "Ly alpha" produced by induced two photon
C13c 6563 c
             H-alpha collision cooling from ground state
C13h 6563 h
              H-alpha collision heating from ground state
C14c 4861 c
             H-beta collision cooling from ground state
C14h 4861 h
              H-beta collision heating from ground state
        0 с
             collision ionization cooling of hydrogen
CION
3bHt
        0 h
             this is the heating due to 3-body recombination
INWD 1216 i
              inward escaping Ly-alpha
INWD 6563 i
              inward escaping Balmer-alpha
INWD 4861 i
              inward escaping Balmer-beta
INWD 18751 i
              inward escaping Paschen alpha
Strk 1216 i
              Stark broadening contribution to line
Strk 6563 i
              Stark broadening contribution to line
Strk 4861 i Stark broadening contribution to line
Strk 18751 i Stark broadening contribution to line
Strk 40512 i Stark broadening contribution to line
Dest 1216 i portion of line lost due to absorp by background opacity
Dest 6563 i
             portion of line lost due to absorp by background opacity
Dest 40516 i portion of line lost due to absorp by background opacity
Dest 4861 i portion of line lost due to absorp by background opacity
Dest 18751 i portion of line lost due to absorp by background opacity
e sc 1216 i electron scattering escape contribution to line
e sc 6563 i
              electron scattering escape contribution to line
e sc 4861 i
              electron scattering escape contribution to line
e sc 18751 i
              electron scattering escape contribution to line
e sc 40512 i electron scattering escape contribution to line
e-e+ 511 i 511keV annihilation line
nFnu 4861 i
              diffuse cont-nu.fnu(4861) due to all computed emission processes
nFnu 1216 i
              diffuse cont-nu.fnu(1216) due to all computed emission processes
Inci 4861 i
              incident continuum at H-beta, no attenuation
Inci 1216 i incident continuum at Ly-alpha, no attenuation
```

TOTL 18751 i

BA C 0 i integrated Balmer continuum emission PA C 0 i Paschen continuum emission Grai 0 i total grain reradiation, both lines and incident continuum part of grain heating due to destruction of Ly alpha Grai 1216 i H FF 0 с H brems (free-free) cooling FF X 0 i part of H brems, in x-ray beyond 0.5KeV ComC 0 c total Compton cooling Expn 0 c expansion cooling, only non-zero for wind 0 C eeff electron - electron brems H FB 0 c H recombination cooling 0 с Hind cooling due to induced rec of hydrogen He3i 0 c cooling due to induced rec of fully ionized helium Cycn 0 c cyclotron cooling Cool 1216 c collisionally excited La cooling Heat 1216 h collisionally de-excited La heating Crst 960 c cooling due to n>2 Lyman lines Hrst 960 h heating due to n>2 Lyman lines Cool 6563 c cooling due to collisional excitation of Balmer alpha Heat 6563 h heating due to collisional de-excitation of Balmer alpha Crst 4861 c cooling due to n>3 Balmer lines Hrst 4861 h heating due to n>3 Balmer lines Cool 18751 c cooling due to collisional excitation of Paschen alpha Heat 18751 h heating due to collisional de-excitation of Paschen alpha Crst 0 c cooling due to higher Paschen lines Hrst 0 h heating due to higher Paschen lines H2 1 2 c H2 rotation lines from Lepp and Shull ApJ 270, 578. H2 d 0 c H2 dissociation by H atoms (not e) 0 c H-FB neg H ion free-bound emission 0 c H+ + H => H2+ + photon continuum cooling H2+ 0 c HEH+ HeH+ formation cooling 0 c He brems emission HeFF 0 c He ionization cooling HeIn HeFB 0 c He recombination cooling MeFB 0 c heavy element recombination cooling MeFF 0 c metal brems emission 0 i total brems emission ToFF 584 c Helium I 584, collisional excitation only HeTC 584 i Ly alpha escaping cloud, at present includes 626 esc 910 i He2p He I two photon emission from 10 level atom He I 504 i emission from recombination to grnd state He I 4471 i HeI 4471 recombination only, fit to Brocklehurst '72 TOTL 5876 i total 5876, from n-level atom Ca B 5876 i He I 5876 REC, simple fit to Brocklehurst TOTL 10830 i 10830 from n-level atom

6 THE EMISSION LINES

```
INWD 10830 i
              inward escaping HeI 10830
TOTL 3889 i
              3889 from n-level atom
TOTL 7065 i
             7065 from n-level atom
CcHE
     0 с
             total collisional He I cooling, from n-level atom
ChHE
        0 h total collisional de-exec He I heating, from n-level atom
He I
        2 i case B He I 2.06 micron
DevB
        2 i corrected He I 2.06 micron
He I 5016 i case B emission
DevB 5016 i case B corrected for Lyman line destruction
He I 3965 i case B emission
DevB 3965 i case B corrected for Lyman line destruction
He I 3614 i case B emission
DevB 3614 i case B corrected for Lyman line destruction
He I 3448 i case B emission
DevB 3448 i case B corrected for Lyman line destruction
HeII 228 i Lyman continuum
HE2C 304 c He II 304 collisionally excited
ESC
      304 i
              He II 304 escaping from cloud
He2C 911 i
             He II Balmer continuum escaping from cloud
TOTL 1640 i
              1640 predicted by 10-level atom
TOTL 4686 i
              4686 predicted by 10-level atom, only valid at high densities
TOTL 1216 i
             1216 predicted by 10-level atom, only valid at high densities
Ca B 1640 i
              He II 1640, case B corrected for density
DevB 1640 i
Ca B 4686 i
              He II 1640, corrected for density, deviations from case B
             He II 4686, case B
DevB 4686 i
             He II 4686, corrected for deviations from case B
Mion
     0 с
             cooling due to collisional ionization of heavy elements
C 1 1656 c Carbon I 1656, collision strength from van Regemoter
REC 1656 i C I 1656 recomb; n.b. coll deexcitation not included
C I 9850 c C I 9850, both of doublet; like 5007+4959
C 1 8727 c C I 8727; equivalent to 4363
C 1 4621 c 1S - 3P
С
  1 610 c C I 610 micron, only H0, H2 included in excitation
С
  1 370 c C I 370 micron, only H0, H2 included in excitation
С
     158 c C II 158 micron, both e- and H0, H2 included in excitation
 2
C 2 2326 c make correction for Balmer absorption
INWD 2326 i inward escaping C II 2326
Phot 2326 i
             photoproduction, Helfand and Trefftz
C 2 1335 c
             CII 1335
REC
     1335 i
             1335 recombination, coef from Ferland et al
C II 3134 c
              intercombination line with same upper state as 1335
C 2 4267 i C II 4267, rate from Ferland et al.
TOTL
     977 i
             total CIII] 1909, recombination + collisional excitation
C3 C
     977 c collisionally excited C III] 1909
```

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```
C3 R 977 i recombination contribution to C III] 1909
TOTL 1909 c
              CIII 1909 collision
INWD 1909 i inward escaping CIII] 1909
C 3 1907 i
             j-2 to ground
             j-1 to ground
C 3 1909 i
C3 R 1909 i C III 1909 recombination from Storey
Phot 1909 i C III] 1909 following relax following inner shell photoionization
C 3 2297 i C III 2297, diel rec coef from Stickland et al
C 3 4187 i C III 4187
C 3 4649 i diel contr from Nussbaumer and Storey, Ast Ap in press ('84)
C 4 1549 c C IV 1550
INWD 1549 i inward part of C IV 1549
DEST 1549 i part of line destroyed by photoionization of Balmer continuum
C4 r
        1 i recombination CIV 1549 from CV
C 4 4659 i C IV 4659, recombination
C 5
       40 c C V 40.3 A, collisionally excited, g-bar approx
C 6
       34 c C VI 33.7 A, collisionally excited, g-bar approx
C 6r
       34 i K-alpha due to recombination of stripped ion
N 1 5200 c
             Nitrogen I 5200
REC 5200 i
             5200 rec, both rad+di, 1/3 of total to doublets
N 1 1200 c
             collisionally excited part
N 2 6584 c
             N II 6584 alone
N 2 6548 c
             N II 6548 alone
REC
     6584 i N II 6584 alone, recombination contribution
N 2 5755 c
             N II 5755 from Seaton 75
Ν
  2
      122 c
             N II fine structure line
N 2
     203 c N II fine structure line
N 2 4239 i N II 4239 recombination, effective rec coef from Williams et al
N 2 5680 i N II 5680 recombination
N 2 2140 c N II 2140 intercombination line
N 2 1084 c N II 1084, CS guess from g-bar
N 3 1750 c N III 1750, collisionally excited
N 3
       57 c N III 57 micron fine structure line
N 3 990 c N III 989.8, collisionally excited
N 4 1486 c
             N IV 1486, collisionally excited
             N IV 765, collisionally excited
N 4
     765 c
N 4 1718 i
             N IV 1718, diel rec coef from Stickland et al
N 5 1240 c
             N V 1240, collisionally excited
N 6
       29 c
             N VI 29A, collisionally excited
N 7
             N VII 25A, collisionally excited
       25 c
       25 i
             recombination K-alpha from fully stripped ion
N 7r
0 1 6300 c
              Oxygen I 6300
D 1 6363 c
             Oxygen I 6363
O 1 5577 c auroral OI
```

```
0 1
     630 c
              O I fine structure line
0 1 1470 c
              O I fine structure line
0 1 7774 i
              estimate of rec coef, 50% of total O I rec
T OI
        0 с
             total collisional cooling due to 6-level OI atom
6lev 8446 i
             OI 8446 from six level atom
6lev 1304 i
             OI 1304 from six level atom
6lev 1039 i OI 1039 from six level atom
6lev 4368 i OI 4368 from six level atom
6lev
     13 i OI 1.3 micron from six level atom
6lev
       11 i OI 1.1 micron from six level atom
       29 i OI 2.9 micron from six level atom
6lev
6lev
       46 i OI 4.6 micron from six level atom
TOTL 3727 c O II 3727, all lines of multiplet together
TOTL 7325 c
              O II 7325, all lines of multiplet together
IONZ 3727 i
              line produced by photoionization of Oo; already included in TOTL
IONZ 7325 i
              line produced by photoionization of Oo; already included in TOTL
O II 3729 i
             five level atom calculations; D5/2 - S3/2
O II 3726 i D3/2 - S3/2 transition
O II 2471 c both 2P 1/2 and 3/2 to ground
0 II 7323 i
              P1/2-D5/2 and P3/2-D5/2 together
0 II 7332 i
             P1/2-D3/2 and P3/2-D3/2 together
     834 c O II 833.8 coll excit
O TT
0 2 4651 i
             O II 4651 recombination, coef from Williams et al
0 3 1663 c
              O III 1661+1666
              contribution to OIII 1664 due to inner shell (2s^2) ionization
Phot 1663 i
Augr 1663 i
              contribution to OIII 1664 due to K-shell ionization
Rec
    1663 i
              upper limit to rate coefficient for dielectronic recomb, NS84
O 3 5007 c O III
                   5007 alone, collisions, tot OIII is this times 1.333
0 3 4959 c 0 III
                    4959 alone, collisions, tot OIII is this times 4
LOST 5007 i
              O III 5007 lost through excit photo
TOTL 4363 c
              O III 4363, collisions from five level atom
Rec 4363 i
              O III 4363 recombination, coef from Burgess and Seaton
O 3 2321 c
              collisional excitation of 2321, 5-level atom
C EX 4363 i
              charge exchange, Dalgarno+Sternberg ApJ Let 257, L87.
C EX 5592 i
              charge exchange rate, D+S
0 3
     880 c
              O III fine structure line, collisions only
03
      520 c
              O III fine structure line, collisions only
              O III 834A, collisions only
03
      834 c
0 3 3341 i
              Burgess and Seaton O III RECOMB, 3341+3312+3299
              O IV 26 micron
04
       26 c
0 4 1402 c
              O IV 1402, collisions
CONT 1401 i
              inner shell photoionization, relaxation
0 4
      789 c
              O IV 789A
0 4 3412 i
              Burgess-Seaton O IV 3412 (whole multiplet twice as strong)
```

0 5 630 c O V 630, collisional excitation TOTL 1218 c O V 1214, collisional excitation 0 5 1218 i j=1 to ground 0 5 1214 i the other line 0 5 5112 i BS O V 5112, recombination 0 6 1035 c O VI 1035, collisional excitation 0 7 22 c O VII 21.6A, collisional excitation, g-bar 08 19 c O VIII 18.97A, collisional excitation, g-bar 19 i 0 8r recombination from fully stripped ion Ne 2 128 c Neon II 12.8 micron 156 c Ne 3 Ne III fine structure line Ne 3 361 c Ne III fine structure line Ne 3 3869 c Ne III 3869, of 3968+3869 doublet Ne 3 3968 c Ne III 3968, of 3968+3869 doublet Ne 3 3343 c NeIII auroral line Ne 3 1815 c NeIII auroral line Ne IV 2424, collisional excitation Ne 4 2424 c Ne 4 4720 c Ne IV N=3 lines, three level atom approx Ne 4 1602 c Ne IV N=3 lines, three level atom approx Ne 5 3426 c Ne V 3426 of 3426, 3346 doublet Ne 5 3346 c Ne V 3346 of 3426, 3346 doublet Ne 5 2976 c auroral line collisionally excited Ne 5 1575 c Ne 5 242 c Ne V 24.2, 14.3 micron Ne 5 143 c Ne V 24.2, 14.3 micron Ne 5 1134 c both components of 5S-3P 1140, 1131 doublet Ne 6 76 c Ne VI fine structure lines Ne 6 1007 c Ne VI] 1007, collisionally excited Ne 7 895 c Ne VII 895, collisionally excited Ne 8 774 c Ne VIII 774, collisionally excited Ne 9 13 c Ne 9 13.5A, collisionally excited Ne10 12 c Ne 10 12.13A, collisionally excited NeLr 12 i Ne Ly-alpha recombination from fully stripped ion Mg 1 4571 c Magnesium I 4571, O I data for coll strength and trans prob Emis 2798 c Mg II 2800 tot intensity, corrected for photoionization loss Cool 2798 c total cooling, including absorbed photons phot 2798 i fraction lost due to photoionization of upper level by Balm cont 4 c Mg 4 Mg IV 4.5 micron Mg 5 13 c Mg V 13.5 micron emission Mg 5 56 c Mg V 5.6 micron emission (Mg 7) 2571, 2893 Mg 5 2751 c Mg 6 1806 c MG VI Mg 7 2629 c (Mg 7) 2510, 2629 Mg 7 433 Mg 7 433 c Mg 8 435 c Mg 8 435

```
Mg 8
       3 c
              Mg 8 3.03 micron
              Mg 9 704.5
Mg 9
      705 c
Mg 9
      368 c
              Mg 9 368,1
Mg10
      615 c
             Mg 10 614.9
Mg11
       9 c
             Mg 11 9.17A
        7 c
Mg12
             Mg 12 7.11A
        7 i
             recombination from fully stripped ion
MgLr
Al 3 1860 c
             Aluminum; the line
     6 i recombination from fully stripped ion
AlLr
Si 2
       35 c Silicon II 35 micron
Si 2 2335 c SI II] 2336,
Si 2 1808 c SI II 1808, permitted resonance line, collisionally excited
Si 3 1207 c SI III 1207, collisionally excited
Si 3 1895 c Si III) 1895, collisionally excited
PHOT 1895 i photoproduction by inner shell removal
Si 4 1397 c
             Si IV 1397, collisionally excited
Si 6
     19 c SI VI 1.96 micron, collisionally excited
Si 7 2148 c
              SI VII, 2148, O III like, collisionally excited
       25 c
              Si VII 2.48, 6.49 micron, collisionally excited
Si 7
Si 7
       65 c
             Si VII 2.48, 6.49 micron, collisionally excited
Si 8 1446 c
              SI VIII 1446, OIII like, collisionally excited
Si 8
     61 c
              SI 8, 61.0A, collisionally excited
Si 9 1985 c
              SI IX 1985, 2150, collisionally excited
Si 9
     949 c
              collisionally excited
Si 9 1815 c
             collisionally excited
Si 9
        3 c
              SI 9, 3.86, 2.84 3P fine structure lines
Si 9
       2 c SI 9, 3.86, 2.84 3P fine structure lines
Si 9
      691 c both components of 5S-3P doublet
      55 c
Si 9
              SI 9 55.3A, collisionally excited
Si10 606 c SI 10 606A, actually group of 4 intercombination lines.
Si10 14300 c
              SI 10 1.43 micron, collisionally excited
Si11 583 c SI XI 582.9, collisionally excited
Si11
      44 c SI XI 43.7A, collisionally excited
Si12
       41 c SI XII 40.9A, collisionally excited
Si13
       7 c
             SI XIII 6.7A, collisionally excited
Si14
        6 C
              SI XIV 6.17A, collisionally excited
              recombination from fully stripped ion
SiLr
        6 i
S 1R 1807 i
              this is to check whether photoexcit of S II is ever important
S 2 6720 c
              S II 6731 + 6716 together
S 2 4074 c
              S II 4070 +4078 together
S 2 10330 c
              S II N=3 lines, all four lines together
S II 6731 i
              individual line from five level atom
S II 6716 i
              individual line from five level atom
S II 4070 i
             individual line from five level atom
```

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S II 4078 i individual line from five level atom S II 10323 i individual line from five level atom S II 10289 i individual line from five level atom S II 10373 i individual line from five level atom S II 10339 i individual line from five level atom S II 1256 c resonance line near NV, collisionally excited S 3 18 c S III fine structure 18.7 34 c S 3 S III fine structure 34 S 3 9532 c [S III] 9532 alone S 3 9069 c [S III] 9069 alone S 3 6312 c [S III] 6312, transauroral temperature sensitive S 3 3722 c [S III] 3722, same upper level as 6312 S 3 1198 c WL, other data, from Ho + Henry Ap.J. 1984 S 3 1729 c S III intercombination line with no atomic data (wild guess) S 4 105 c S IV 10.5 micron, collisionally excited S 4 1406 c S IV 1406, collisionally excited S 5 1198 c S V 1198, collisionally excited S 5 S V 786.5, collisionally excited 786 c 933 c S VI 933+944, collisionally excited S 6 S 9 1715 c S IX 1715, 1987, collisionally excited S X 1213, 1197, collisionally excited S 10 1213 c S XI 1615, 1826, collisionally excited S 11 1826 c S 12 520 c S XII 520, group of four intercombination lines all together S 12 7611 c S XII 7625, WL from Moore NBS, collisionally excited S 13 488 c S XIII 488.4, 1909 like, collisionally excited S LR 5 i S 16 4.7A Ly a recombination from fully stripped ion 7 c Ar 2 Argon II 7 micron Ar 3 7135 c Argon III 7136 Ar 3 7751 c Argon III 7751 22 c Ar 3 Argon III 21.8, 9 micron lines 9 c Ar 3 Argon III 21.8, 9 micron lines Ar 4 4740 c Argon IV 4711 + 4740 together, 4740=90% Ar 4 7335 c [AvIV] auroral line Ar 5 7007 c Argon V, 3P lines, 7007, collisionally excited Ar 5 6435 c Argon V, 3P lines, 6435, collisionally excited Ar 5 Argon V fine structure lines, 13.09, 7.903 micron line 131 c 79 c Argon V fine structure lines, 13.09, 7.903 micron line Ar 5 Ar 6 Ar VI 4.53 micron 4 c Ar14 4413 c Ar XIV 4413, predicted lambda, not observed(??) Ar15 409 c collisionally excited Ar 18 ly a recombination 3.7A from fully stripped ion ArRr 4 i Ca 2 3933 c coll excit calcium k+h Ca 2 8579 c infrared triplet Ca 2 7306 c forbidden line

Phot 3933 i fraction H Ly-alpha destruction of excited levels Phot 7306 i fraction H Ly-alpha destruction of excited levels Ca2K 3934 i Ca2H 3969 i individual lines from five level atom individual lines from five level atom Ca2X 8498 i individual lines from five level atom Ca2Y 8542 i individual lines from five level atom Ca2Z 8662 i individual lines from five level atom CaF1 7291 i individual lines from five level atom CaF2 7324 i individual lines from five level atom Rec 3933 i reccombination contribution to CaII emission Ca 4 32 c Ca IV 3.2 micron Ca 5 4 c Ca V 4.16, 11.47 micron Ca 5 11 c Ca V 4.16, 11.47 micron Ca 5 6087 c Ca V optical and uv lines, collisional excitation, 3-level atom Ca 5 5311 c Ca V optical and uv lines, collisional excitation, 3-level atom Ca 5 2414 c Ca V optical and uv lines, collisional excitation, 3-level atom Ca 5 3997 c Ca V optical and uv lines, collisional excitation, 3-level atom CaLr 3 i Calcium Ly a recombination from fully stripped ion Fe 2 48 i emission from Netzer's 3-level atom 7 i Fe 2 emission from Netzer's 3-level atom 3 i Emis emission from Netzer's 3-level atom net cooling due to UV lines 3 i Cool TOT 0 с total of all UV+optical FE II cooling sum of all IR cooling from 6D ground state FETR 0 с Fe 3 0 с sum of 3p and 3g states together Fe 3 5270 c Fe III 5270, predictions cop-out from garstang et al 78 Fe 3 4658 c Fe III 5270, predictions cop-out from garstang et al 78 Fe 3 1122 c FeIII 1122 entire multiplet Fe 5 3892 c Fe V 3892+3839 Fe 6 0 c all of 2G lines together first Fe 6 5177 c Fe VI 5177, approximate correct Fe 7 6087 c FE VII 6087 Fe 9 171 c FE 9 171.1 Fe 9 245 c FeIX 245 j=1 fast decay Fe 9 242 c FeIX 242 j=1 slower decay Fe10 352 c FE 10 352.1 Fe10 6374 i total (coll, pumped) Coll 6374 c collisional contribution Pump 6374 i pumped by continuum fluorescense 352 6374 c collisions of E1 line Fe11 7892 i total intensity of line Coll 7892 c contribution from collisional excitation contribution from continuum fluorescense Pump 7892 i IR fine structure line Fe11 6 c

Fe11 2649 c collisional excitation Fe11 1467 c collisional excitation Fe11 354 c Fe 11 353.8 Fe12 1242 c Fe 12, 1242, 1349 together, collisional excitation Fe12 2170 c Fe 12, 2170, 2406 together, collisional excitation Fe12 2568 c Fe12 2904, 2567, 3567, 3073 together, collisional excitation Fe12 357 c Fe 12 357.3, collisional excitation Fe13 363 c Fe 13 363.3, collisional excitation Fe14 347 c Fe 14 262.3, 347, collisional excitation 262 c Fe 14 262.3, 347, collisional excitation Fe14 Fe14 5303 i total intensity of line Coll 5303 c contribution from collisional excitation Pump 5303 i continuum fluorescense 347 5303 c collisional excitation of E1 line Fe15 284 c Fe 15 284.1, collisional excitation Fe16 343 c Fe 16 343.5, collisional excitation Fe17 17 c 2p5 3s 17.096, 17.051, 16.775A 15 c 2p5 3d 15.451, 15.261, 15.013A Fe17 Fe18 975 c Fe XVIII 974.A, collisional excitation lines from Kato, collisional excitation lines from Kato, collisional excitation Fe18 104 c 108 c Fe19 Fe19 592 c fe19 from loulergue et al '85 Fe19 7082 c fe19 from loulergue et al '85 Fe19 1118 c fe19 from loulergue et al '85 Fe19 1328 c fe19 from loulergue et al '85 Fe20 120 c fe19 from loulergue et al '85 Fe21 142 c triplet at 129, 142, 146A, collisional excitation Fe21 1354 c next two 3p ground state lines, collisional excitation Fe21 2304 c collisional excitation Fe22 130 c collisional excitation Fe22 149 c collisional excitation Fe23 133 c collisional excitation Fe22 846 c Fe 22 845.6A Fe23 263 c Fe 23 1909-like 262.6 Fe24 255 c Fe 24 255, 192 doublet all in one, collisional excitation Fe25 Fe 25, He like, 1.85A, collisional excitation 2 c Fe26 2 c Fe 26, H like, 1.79A, collisional excitation Totl 2 i total intensity of K-alpha line FeLr 2 i recombination from fully stripped ion total hot iron Ka; Auger "hot" iron, plus recom TotH 2 i Auger production of "cold" iron, less than or 17 times ionized AugC 2 i

7 MACHINE ENVIRONMENT

CLOUDY is designed to run in single precision on IEEE 32-bit computers such as SUNs, Decstations, 80X86 or 680X0-derivative machines, as well as VAXs. It has been developed with double precision disabled, indefinites set, and stack memory enabled, on The Ohio Supercomputer Center (OSC) CRAY Y-MP, and has been tested on a VAX 8650, Sun Sparcstation, Decstation 3100, and Northgate 486 PC. Calculations on all machines produce essentially identical results.

The floating point environment should be set to ignore floating point underflow but crash on any other floating point error. Floating point underflow is an unavoidable consequence of the attenuation of radiation as a beam of light is extinguished by an absorbing medium; underflow error-checking should be disabled. This is the default condition for most UNIX machines and VAXs, and code is included in the driver for CLOUDY to disable underflow error-checking on IBM, CDC, SUN, and UNIX machines.

Floating point overflow or division by zero *must never* occur, nor should library function domain errors (i.e., the log of a negative number); I would appreciate hearing about these errors; I can't fix it if I don't know it is broken. My internet address is gary@bowen.mps.ohio-state.edu; please send the input file and version number.

VAX A problem can arise when running CLOUDY on a VAX, and this makes the use of the "/g_floating" option on the DEC FORTRAN compiler necessary. Several portions of CLOUDY having to do with determining the ionization balance of the elements are written in double precision. The neutral fraction can become very small when the gas is highly ionized, and it is necessary to have exponents which extend beyond the conventional $10^{\pm 38}$ range of these machines. This portion of the code is written in double precision, which by the IEEE convention also has an increased exponent size. A VAX does not obey this convention (they were developed before it was) unless the "/g_floating" option is used on the compile step. CLOUDY checks to see that the double precision is working correctly and will print a note if it is not. On some VAXs the "g_floating" option brings a severe time penalty. If this is the case, then it is not necessary to use the "g_floating" option, but CLOUDY will not work for many conditions. Floating point overflow may or may not occur if "/g_floating" is not specified.

CRAY It is not necessary to use double precision on a Cray. The double precision disable option can safely be set on the compile step. The code has been tested with both stack memory and indefinites enabled on the Ohio Supercomputer Center (OSC) CRAY Y-MP.

SUN Unix The code has been extensively tested on a Sun Sparcstation IPC. The Sun Fortran compiler cannot compile the entire code in a single pass. It is necessary to break the code up into a half-dozen or more large pieces (being careful to divide the files to keep subprograms together), with each piece of length $\ll 10^4$ lines. If each piece is called "part1.f", "part2.f", etc, then they can be compiled separately with compile commands

```
f77 -fnonstd -c part1.f
f77 -fnonstd -c part2.f
f77 -fnonstd -c part3.f
f77 -fnonstd -c part4.f
```

and then linked with the command

f77 -fnonstd -o c.out part1.o part2.o part3.o part4.out

where "c.out" is the name of the executable file.

The execution-time warning messages saying that IEEE exceptions underflow and inexact occurred and have not been cleared are normal for Suns' implementation of IEEE arithmetic. Overflow or division by zero must not occur.

It is *essential* that the "-fnonstd" option be specified on both the compile and link steps. This option enables the correct error handling for underflow, division by zero, overflow, and operand range error. Besides setting a mode where the code will crash upon performing an illegal operation, it will speed up the execution time by factors of from three to ten.

Decstation The test cases presented in section 25 have been computed on a Decstation 3100. The agreement with results of other machines was good, although testing on this machine has not been as extensive as on the others mentioned above.

8 PROBLEMS

8.1 Floating Point Errors

CLOUDY has been tested on machines ranging from 386 PCs to CRAY Y-MPs. Floating point errors do not occur. The logic within the code is designed to identify problems, and complain, but not fail. The logic is only as good as the tests they were designed to pass. It is inevitable that circumstances will occur for which the logic now in the code is not sufficient. It is possible that the code will fail when these circumstances occur. I would be grateful for reports of any such failures, since they inevitably identify shortcomings in the code, and lead to its improvement. My e-mail address is gary@bowen.mps.ohio-state.edu.

8.2 No Temperature Convergence

A temperature failure occurs when the heating-cooling balance is not within a certain tolerance, set by the "TOLERANCE" command, after 20 tries. Normally CLOUDY will punt after an excessive number of temperature failures occur. The limit to the number of failures is reset with the "FAILURES" command, which sets the variable LIMFAL. The default value is 20. (When CLOUDY stops because of excessive failures it first produces a map of heating-cooling space to give an indication of where the equilibrium temperature should have been.)

It has been my experience that temperature failures most often occur for temperatures near $1-4 \times 10^3$ K, and near 10^5-10^6 K, where the cooling function permits more that one thermal solution (see, for example, Williams 1967). Figure 3 shows a typical cooling function, computed for parameters given in an example shown in section 25 below. A peak is reached at a temperature near 10^3 K. This occurs because the fine-structure lines are major coolants and have Boltzmann factors near unity. As a result their cooling rate is proportional to the Coulomb focusing factor $T^{-1/2}$, and the cooling rate *decreases* until the temperature is high enough for optical forbidden lines to become important coolants. A similar phenomenon occurs if the solution needs to jump over the ~ 10^5-10^6 K peak in the cooling function.

When failures occur because more than one temperature solution is possible, the reported failures are a physical (not numerical) problem. CLOUDY will try to deal with this problem by forcing the temperature to values below the peak in the cooling function. Increasing the number of allowed failures (with the "FAILURES" command) to prevent the code from stopping prematurely is permissible as long as the global energy balance is preserved. A warning will be issued at the end of the calculation if the heating-cooling balance is not preserved.

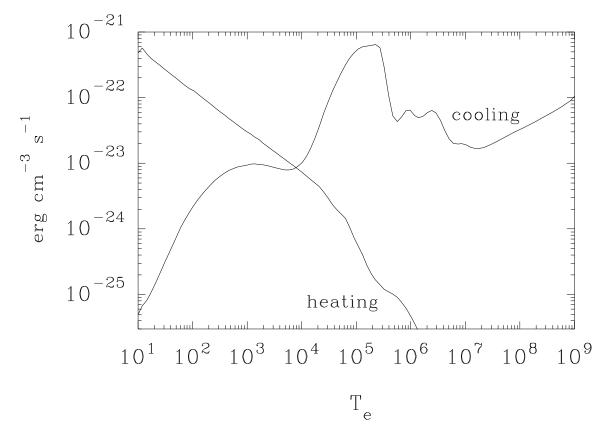


Figure 3: This figure shows a typical cooling function for low density gas. The temperature is shown on the x-axis, and the cooling rate (erg cm⁻³ s⁻¹) is indicated by the dashed line, and the heating (same units) by the solid line. The map was produced using one of the examples given in section 25 below. cooling

8.3 Map Output

If an excessive number of temperature failures occur (the default limit is 20) then the program stops and produces a map of the heating and cooling as a function of temperature. The limit to the number of failures is reset with the "FAILURES" command. The map is described here.

The programs steps through increasing temperatures and prints the heating, cooling, and ionization of the gas. From this information it should be possible to determine the temperature where the equilibrium thermal solution should have been. Each solution is completely self-consistent. Both the attenuated radiation field and collisional ionization contribute to the ionization balance at each temperature. All processes contribute to the thermal balance, including collisional ionization. The map is at constant density.

The first column gives the temperature. Column 2 and 5 give the volume heating and cooling, both in units erg s⁻¹ cm⁻³. Columns 3 and 6 are pointers to the main source of heating and cooling, and columns 4 and 7 give the fraction of the total heating or cooling due to these agents. Column 8 gives the cooling derivative, 9 is the electron density (cm⁻³) and the remaining columns give the hydrogen and helium ionization fractions.

8.4 Thermal Stability

Note also that the thermal solution may be unstable when the temperature derivative of the net cooling function is negative. Possibly unstable solutions are indicated by a "u" just before the equilibrium temperature in the zone printout. (The temperature derivative is for isochoric, not isobaric, conditions.) Comments are printed at the end of the calculation if possibly unstable thermal solutions are present in the calculation.

8.5 Negative Populations of H, He

It is possible that the code will stop because negative level populations were predicted for atoms or ions of hydrogen and helium. This is not supposed to occur, but sometimes happens because of numerical instabilities in the matrix inversion routine.

8.6 I can't fix it if I don't know its broken.

Machines are grower faster much more rapidly than people are getting smarter. Reliability in the face of complexity is the major challenge to the development of any large-scale computer code. There can be little doubt that CLOUDY contains bugs. The code is well tested in many simple limits, and behaves in the correct manner. Simulations of HII regions, planetary nebulae, and other simple objects, are in good agreement with predictions of other photoionization codes.

Bugs can be discovered by strange behavior in situations where the code has not been tested. The discovery of the existence of these bugs is itself a major challenge. If problems arise or the code crashes then it is likely that a problem has been isolated. I would appreciate learning about such problems since they identify shortcomings which usually lead to improvements in the code (or the documentation). My e-mail address is gary@bowen.mps.ohio-state.edu.

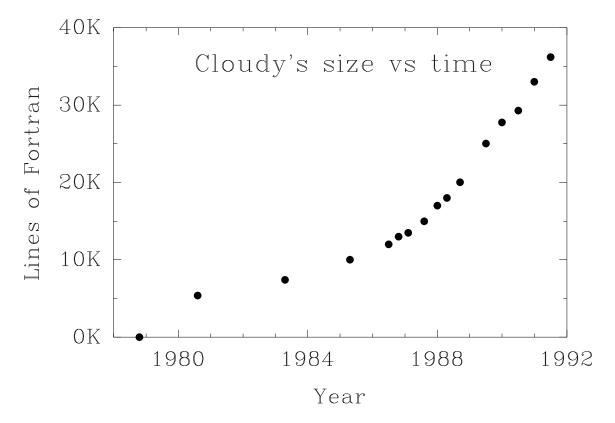


Figure 4: This figure shows the size of the code, indicated by the number of lines of FORTRAN, as a function of time. size

9 MAJOR REVISIONS TO CLOUDY

This section outlines some of the major versions of CLOUDY, and gives an indication of the direction development will take in the next few years. Its development began in August of 1978, at the Institute of Astronomy, Cambridge, and has been continued at The University of Kentucky and The Ohio State University. Figure 4 shows the evolution of the code, as indicated by its size as a function of time.

9.1 Major Past Versions

- 67 August 1987. Hydrogen atom goes to LTE in limit of large electron densities. Many small bugs uncovered as result of careful comparison with Netzer's ION.
- 68 Cambridge, Fall 1987. Development work in progress.
- 69 December 1987. Hydrogen atom goes to LTE in limit of large photon densities. Ferland and Rees (1988).

- 70 September 1988. He II Lyα transfer improved. Improved form of escape probabilities with explicit damping constants. H⁻ and improved free-free heating. Many high excitation metal lines transferred. (Rees, Netzer, and Ferland 1989; Ferland and Persson 1989).
- 71 December 1988. Photon array rewritten, now Compton exchange problem is exact for black bodies with temperatures between 2.7 K and 10^{10} K. He II Ly α radiation pressure included.
- 72 January 1989. Static version, minor bug fixes.
- 73 1989. Major rewrite of helium treatment. Dust changed to two populations, scattering and absorption included. Default radius and thickness increased by ten orders of magnitude. He⁺ goes to LTE. Development work on getting helium to go to LTE. IR power law for default AGN continuum now ν^{+2.5} below 100 micron break. No ANUMM array, all continuum one array. TABLE STAR. COOLR broken up. Helium to LTE for high electron density.
- 74 1990 January. Hydrogen double precision, many bug fixes. 10 tables among the continua. Kurucz (1989) atmospheres. Improved dust treatment, including photoionization and charge.
- 75 1990, JILA. Cosmic abundances changed to Grevesse and Angers. Major bug in constant pressure for HII regions, PNs, etc; did not affect BLR. Calculation of νf_ν(Hβ) was incorrect. Molecules at low temperatures. HDEN now N(H°) + N(H⁺) + N(H⁻) + 2N(H₂) + 2N(H₂⁺). Improved Rayleigh scattering treatment. Dielectronic recombination for sulphur (guess). Many changes in dust; Orion paper (Baldwin et al. 1990).
- 76 1990, static version from end of JILA visit.
- 77 through Nov 1990. OPTIMIZE option added using Bob Carswell's code. Gaunt factor for brems input spectrum. Reflected continuum predicted. Frequency partition adjusted. X-ray optical depth now at 0.5 kev. Read in table of points from previous calculation. OPSAV deleted, now single pointer OPSV for all opacities. Numerical array to 100MeV. Hummer Ly-alpha escape destruction prob. TAUTOT arrays now both in and outward directions. Bound compton included for all ionization levels. Mean ionization arrays rewritten to make sense. Bug in wind velocity fixed, result now exact. C, O outward diffuse fields changed to OTS.
- 78 Through May 91. Continuum escape probability formal H-only opacity. H rec, cooling over wide range of temp. "ABUNDANCES NO DUST" no longer

changes abundances of depleted elements. OI-Ly β treatment is now six-level atom. Default table AGN changed. Continuum normalization rewritten. Milne relation for diffuse fields of H, all He. Fe Ka divided into hot and cold. Beams paper (Ferland, Peterson, Horne, et al.) Many high ionization lines included as OTS and outward ionization sources.

- 79 Summer 91. H molecules completed, C, N, O molecules included. Continuum binning changed for Ca, Fe L-shell ionization potentials. Extensive testing.
- **80.05**, **80.06** July 91, static versions. Version 80.06 included several small bug fixes, and the new [NeV] IR collision strengths.
- 81 Yet newer collision strengths for [NeV] IR lines (10x larger).

9.2 Future Improvements

- Helium atom goes to LTE for high radiation densities.
- Helium collision data update.
- Define departure coefficients for helium as in Mihalas.
- Hydrogen and helium transition probabilities as a function of temperature and density.
- Molecule network goes to LTE for all temperatures.
- Transfer Ly α correctly (incomplete redistribution).
- Transfer other hydrogen lines correctly (complete redistribution).
- Opacity Project photoionization cross sections, recombination rate coefficients.
- Heavy elements go to LTE via psuedo states.
- Include all hydrogen, helium lines in radiative acceleration.

9.3 Known Modes for CLOUDY 80.06

- Gaunt factors taken from Hummer subroutine, not defined in very far IR.
- HeII 10-level atom predictions do not agree with case B at low density. (l-mixing not a good assumption.)
- HeII line radiation pressure not reliable.

• 2s level of hydrogen not exactly unity in radiation-LTE limit. Induced two-photon emission.

9.4 Making a Revision

- Compile with array bounds checking on Cray. Run all test cases on Cray, VAX, Sun, and PC. Confirm no differences.
- Compile line list from LINES.
- Compile index.
- Pass HAZY through spelling checker.
- Update all comparison tables; confirm OK.
- Change labels in HAZY.
- Confirm table of contents ok.
- Check that driver and main subroutine in HAZY are still accurate.
- Compile sample driver, check that results agree with sample input stream.
- Summarize changes from VERSION, for "past major revisions" above.

10 CLOUDY AS A SUBROUTINE

CLOUDY is designed to also be used as a subroutine of other, much larger, codes. When used this way, a series of subroutine calls, described next, are used to initialize the code, specify the initial conditions, drive the code, and examine the predictions.

It is also possible to drive the code by accessing its common blocks directly. In fact, this was the preferred method before version 80. The major problem with this approach, besides its inconvenience, is that the code and its common blocks are constantly changing, so that the main driver code will also have to be changed to keep up with CLOUDY. The following subroutines access the common blocks themselves, and (it is hoped) their use will not change with time.

10.1 Initializing the Code

Several variables must be initialized at the beginning of the calculation. This is done by calling subroutine CDINIT.

CALL CDINIT

CDINIT must be called every time a new calculation is to be performed, *before* calling any of the following subroutines.

10.2 Entering Commands

The input stream used to specify the initial conditions for the calculation consists of a series of 80 character free format command lines. They must start in column 1, and contain meaningful information across all 80 columns. These command lines are entered by successive calls to routine CDREAD.

```
CHARACTER*80 LINE
WRITE(LINE,'(''constant pressure'')')
CALL CDREAD( LINE , NLEFT )
HDEN = 3.5
WRITE(LINE,'(''hden='',F5.1)') HDEN
CALL CDREAD( LINE , NLEFT )
```

The first argument of CDREAD is the line image, an eighty character variable. The line image it stores must obey all the rules for normal command lines. It is assumed to end with column 80 or one of the special characters outlined in the section on command line format. The second integer variable in the call to CDREAD is the

*

number of command lines which can still be entered. It is not now possible to read in more than 100 command lines because of limits to the size of the character arrays used to store them. This limit is stored as the variable NKRD which occurs in several parameter statements throughout the code. If more than 100 lines are read in by calling CDREAD then CDREAD will stop after explaining why. It will be necessary to increase NKRD throughout the code if more than 100 command lines are needed.

10.3 Controlling Output

CLOUDY normally speaks what's on its mind. However, it does have a quiet mode in which nothing at all is printed. This quiet mode is set by the logical argument to subroutine CDTALK.

```
    set no output at all
CALL CDTALK( .FALSE. )
    have the code produce the normal printout
CALL CDTALK( .TRUE. )
```

The default is for CLOUDY to produce output, and CDTALK does not have to be called if this is desired. However, it does need to be called with the logical variable false if the quiet mode is desired.

10.4 Calling the Code

CDDRIV is a subroutine with a single logical variable. The following shows an example of its use.

LOGICAL OK CALL CDDRIV(OK)

If the calculation was successful then the logical variable (in this example given the name "OK") is set .TRUE. by the code. If problems occurred and the results cannot be trusted then the variable is set .FALSE.. If output was turned off (with CDTALK) then it will probably be necessary to turn output on and recompute the model to find out what went wrong.

10.5 Reading the Emission-Line Array

The predicted line intensities or luminosities are stored within a set of common blocks which also contain the line identifiers, a four character label and integer wavelength. These are normally printed at the end of the calculation. It is also possible to obtain the line formation by calling subroutine CDLINE.

```
CHARACTER*4 LABEL
LOGICAL OK
*
LABEL = 'TOTL'
LENGTH = 1216
CALL CDLINE( LABEL , LENGTH , RELINT , ABSINT , OK )
```

The first variable is the line label, the four character string usually used to identify the line. The second integer variable gives the wavelength of the line. Both of these must exactly match the label and wavelength used by CLOUDY to identify the line (see Section 6). If CDLINE finds the line then the logical variable which is the last argument in the call to CDLINE is set to .TRUE., and this variable is set to .FALSE. if the line is not found. The third variable (RELINT in the above example) is the relative intensity of the line (relative to the normalization line, usually H β). The log of the intensity (erg cm⁻² s⁻¹) or luminosity (erg s⁻¹) of the line is returned as the next variable (ABSINT in the above example).

10.6 Reading the Column Density Array

The predicted column densities can be accessed by calling the subroutine CDCOLM.

```
CHARACTER*4 LABEL
*
LABEL = 'CARB'
ION = 3
CALL CDCOLM( LABEL , ION , COLUM )
```

where COLUM is the predicted column density. The label must agree with the first four characters used in the printout. The integer variable ION is the spectroscopic designation of the level of ionization, i.e., 1 indicates CI, 3 indicates CIII, etc.

10.7 Example Call as a Subroutine

The following is an example of a very simple call as a subroutine. The normal output will be produced on Fortran unit 6.

PROGRAM MAIN LOGICAL OK CHARACTER*80 LINE

- *
- initialize the code

CALL CDINIT

```
*
      write a series of command lines into character variable LINE,
*
      then feed into code with CDREAD
*
      WRITE(LINE, '(''hden 4 '')')
      CALL CDREAD(LINE , NLEFT )
      WRITE(LINE,'(''black 5 '')')
      CALL CDREAD(LINE , NLEFT )
      WRITE(LINE, '(''stop zone 1 '')')
      CALL CDREAD(LINE , NLEFT )
      WRITE(LINE, '(''ionization -2 '')')
      CALL CDREAD(LINE , NLEFT )
*
      now call the main driver, output will be produced
*
      CALL CDDRIV( OK )
*
      STOP
      END
```

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12 GLOSSARY OF SYMBOLS

As far as possible, the notation used by HAZY follows standard texts (Osterbrock 1988; Mihalas 1978). This is a summary of some of the symbols used.

Symbol	Description	Units	Page
А	radiative rate	s^{-1}	
\mathbf{b}_n	departure coefficient	-	
С	collisional rate	s^{-1}	
D_{ul}	line destruction probability	-	
f(r)	filling factor	-	
\mathbf{g}_i	statistical weight	-	
G	energy gains, heating	${ m erg}~{ m cm}^3~{ m s}^{-1}$	
Ι	intensity	$\mathrm{erg} \mathrm{s}^{-1} \mathrm{sr}^{-1}$	
J	mean intensity	$erg s^{-1} sr^{-1}$	
N(cr)	cosmic ray density	cm^{-3}	
q	collisional rate coefficient	$\mathrm{cm}^3~\mathrm{s}^{-1}$	
$\dot{\mathbf{P}}^*(\mathbf{x})$	LTE relative population	cm^3	
\mathbf{P}_{ul}	line escape probability	-	
P _c	continuum escape probability	-	
Т _и	energy density temperature	Κ	
T _{color}	color temperature	Κ	
Ug	grain potential	volt	
${ m Q}^{g}_{abs}$	grain absorption efficiency	-	
Q(H)	hydrogen ionizing photons	s^{-1}	
V	velocity	${ m cm~s^{-1}}$	
V_g	grain potential	eV	
$\alpha(T)$	recombination coefficient	$\mathrm{cm}^3~\mathrm{s}^{-1}$	
α_{ν}	continuous absorption cross section	cm^{-2}	
α_{lu}	line absorption cross section	cm^{-2}	
β	recombination cooling coef	$\mathrm{cm}^3 \mathrm{s}^{-1}$	
η	photon occupation number	_	
γ	one sided escape probability		
Γ	photoionization rate	s^{-1}	
κ	opacity	cm^{-1}	
Λ	energy loss, cooling	$erg cm^3 s^{-1}$	
ϕ	photon flux	cm^{-2} s ⁻¹	
φ σ	scattering cross section	cm^{-2}	
Σ	projected grain area	cm^2	
τ	optical depth	-	
ν	frequency	Ηz	

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HAZY

a brief introduction to CLOUDY 80.06 Computational Methods and Test Cases

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CLOUDY 80.06

G.J. Ferland Astronomy Department The Ohio State University Columbus OH 43210 August 4, 1991

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13 INTRODUCTION

This section outlines the computational methods used in version 80.06 of CLOUDY. Parts are modified from Ferland and Mushotzky (1984), Ferland and Rees (1988), Ferland and Persson (1989), Rees, Netzer, and Ferland (1989), Baldwin et al. (1991), and Fabian and Ferland (1991). The code has been designed to be as general as possible (but limited to non-relativistic regimes which are not Compton-thick) while remaining computationally expedient. Similar discussions of hydrogen line formation, focusing on the density range $N \leq 10^{11}$ cm⁻³ appropriate to quasar emission-line clouds, can be found, for instance, in Mathews, Blumenthal, and Grandi (1980) and Drake and Ulrich (1980). Discussions of line formation and ionization and thermal equilibria are presented by Osterbrock (1988), Davidson and Netzer (1979), Kwan and Krolik (1981), Halpern and Grindlay (1980), Weisheit, Shields, and Tarter (1981), Kallman and McCray (1982), Hubbard and Puetter (1985), Vernazza, Avrett, and Loeser (1981), and Avrett and Loeser (1988).

14 THE CONTINUUM

Under most circumstances the continuum produced by the central object is the only source of heat and ionization for the emission-line clouds. Supplemental heating due to cosmic rays, dissipation of turbulence, neutrons, or an arbitrary heat source can also be added, however. This section describes how this continuum, and continuous opacities, are treated.

14.1 Continuum Range

The energy interval 1.001×10^{-5} Ryd— 7.354×10^{6} Ryd is divided into ~ 500 energy bins with nearly logarithmically increasing widths. The low energy limit to the continuum is stored as the variable EMM and the high energy limit as EGAMRY. These are the two elements of the common block BOUNDS.

14.2 Continuum Pointers

The function IPOINT converts energy (Rydberg) into pointers to the cell containing the specified energy. It has a single argument, the energy in Rydberg, and returns the pointer to the appropriate cell. IPOINT will stop if the energy does not lie within the continuum bounds of the code.

14.3 Continuum Arrays

Several vectors deal with aspects of the attenuated incident and diffuse continua. All store these fluxes in units photons $cm^{-2} s^{-1} cell^{-1}$ and they all map one-to-one with one another.

ANU The energy (in Rydbergs) of the center of each cell is stored in the vector ANU.

WIDFLX The width of each cell (Rydbergs) is stored in the vector WIDFLX.

FLUX The attenuated incident continuum is stored in the vector FLUX.

OTSCON and OTSLIN Two vectors, OTSCON and OTSLIN, store the local on-the-spot (OTS) photon fluxes for continua and lines. Both are totally local rates, and are reevaluated for every zone.

DIFFUS The diffuse continuum (total local emission due to all processes, *per unit volume* with no filling factor) is stored in DIFFUS.

REFLEC The "reflected" continuum (defined elsewhere) is stored as REFLEC. The reflected continuum is updated for each zone, and the contents of REFLEC is the integrated quantity.

CONDIF The vector CONDIF stores the outward diffuse continuum which is not included in the evaluation of the photon heating rates. These are largely fields which are treated as sources of ionizing radiation in other ways.

OUTCON OUTCON stores the many lines and continua which are carried outward and treated as sources of ionizing radiation. Only weak sources of ionizing radiation are carried in this array; strong continuum sources are treated by more exact methods, and their OTS fluxes stored in OTSCON or OTSLIN.

CONEMS CONEMS is the outward continuum which is carried without further interaction with the gas. This is not a directly observed quantity.

CORIND Boltzmann factors, the ratio $\exp(-h\nu/kT)$, are stored in the vector CORIND, which is evaluated in routine BOLTGN.

14.4 Continuous Opacities

The cloud is divided into a large number of concentric shells (zones) and the attenuated and diffuse continua and physical conditions are then determined within each.

A correction must be made to account for the attenuation of the continuum across the zone (Netzer and Ferland 1983). Assuming that the continuum varies across the zone as

$$\frac{I(\nu, dr)}{I_o(\nu)} = \exp(-\kappa(\nu)f(r)\,dr) \tag{50}$$

then the intensity averaged over a zone with thickness dr is

$$\left\langle \frac{I(\nu, dr)}{I_o(\nu)} \right\rangle = \frac{1 - \exp(-\kappa(\nu)f(r)\,dr)}{\kappa(\nu)f(r)\,dr} \tag{51}$$

where $\kappa(\nu)$ is the absorption opacity and f is the filling factor. The coefficients giving this ratio as a function of energy are stored in the vector TAUMN, and are evaluated in subroutine RADINC. The continuum stored in FLUX is multiplied by these factors in the same subroutine.

The main opacity sources in the ultraviolet continuum are generally photoelectric and free-free (inverse brems) absorption, electron scattering (of both bound and free electrons), and the damping wings of Lyman lines (Rayleigh scattering). The main reemission mechanisms are generally free-free (brems), free-bound, and two photon emission. Grains can also be added as an option. Continuous absorption and reemission by all ground states, and many excited states, of all 166 ionization stages of the 13 elements in the calculation are explicitly included. Great care is taken to ensure that each absorption mechanism is balanced by a reemission process, and vice versa, so that energy balance in the strict thermodynamic limit can be achieved.

14.4.1 Rayleigh scattering

Clouds with neutral hydrogen column densities greater than $\sim 10^{23}$ cm⁻² are optically thick to Rayleigh scattering at wavelengths near Ly α , and this process is a major scattering opacity source at short wavelengths for grain-free environments.

Rayleigh scattering cross sections given by Gavrila (1967) are used, joined with expressions for the radiative damping wings of Lyman lines (Mihalas 1978). For wavelengths longward of 1410Å a power-law fit to the Gavrila's quantal calculations is used;

$$\sigma_{Ray} = 8.41 \times 10^{-25} \epsilon^4 + 3.37 \times 10^{-24} \epsilon^6 + 4.71 \times 10^{-22} \epsilon^{14} \ cm^2 \tag{52}$$

where $\epsilon \equiv \nu/cR_{\infty}$ is the photon energy in Rydbergs. This fit is accurate to typically a percent, with occasional errors as large as 4 percent.

For wavelengths between 1410Å and the Lyman limit radiative broadening of the Lyman lines is assumed (Mihalas 1978);

$$\sigma_{Ray} = \sum_{i=2}^{4} \left(\frac{e^2 f_{1,i}}{mc} \right) \frac{\Gamma/4\pi}{\left(\nu - \nu_{1,i}\right)^2} \ cm^2 \tag{53}$$

where Γ is the reciprocal lifetime of the upper level *i* and the sum is over the first four Lyman lines. This expression gives cross sections in excellent agreement with Gavrila (1967) for these wavelengths.

14.4.2 Free-free opacity

The main opacity source in the infrared-radio spectral region for many conditions is free-free opacity with a cross section given by

$$\alpha_{\nu}(ff) = 3.69 \times 10^8 \,\bar{g}_{III}(\nu, T) \,f(r) \,\nu^{-3} \,T^{-1/2} \left\{ 1 - \exp(-h\nu/kT) \right\} \sum_A \sum_z z^2 \,N_A^{+z} \,cm^2$$
(54)

(see, for example, Mihalas 1978). The sum is over all ions N^{+z} of element A. The temperature averaged gaunt factor $\bar{g}_{III}(\nu, T)$ is taken from Hummer (1988; see also Karzas and Latter 1961). H⁻ free-free opacities are included as well (see below).

14.4.3 Bound-free opacity

Continuum optical depths for photoabsorption from level n are given by

$$d\tau_n(\nu) = \alpha_\nu(n) \ N_n \left[1 - \exp(-h\nu/kT)/b_n \right] \ f(r) \ dr \quad , \tag{55}$$

where b_n is the departure coefficient for level n and α_{ν} is the absorption cross section.

14.5 Attenuation of the Incident Continuum

Continuous opacities are stored in two vectors which map one-to-one with FLUX and ANU. The vector SCATOP stores the scattering opacity, while the vector OPAC stores the absorption opacity. Continuous optical depths accumulated up to the current zone are stored in three vectors which map one-to-one with FLUX and ANU. The vectors TAU, TAUABS, and TAUSCT store the total continuous optical depths, absorption optical depths, and scattering optical depths, respectively.

In an open geometry scattering is assumed to attenuate the incident continuum as

$$I = I_o \left(1 + 0.5 \ d\tau_{scat} \right)^{-1} \quad . \tag{56}$$

Scattering does not affect the continuum in a closed geometry. Absorption is assumed to attenuate the incident continuum as

$$I = I_o \exp\left(-d\tau_{abs}\right) \tag{57}$$

for both geometries.

14.6 Recombination Equilibrium

A modified version of the "on-the-spot" (OTS) approximation is used in the treatment of sources of diffuse ionizing radiation. Were no other opacity sources present, then, for a closed geometry which is optically thick in the Lyman continuum, all recombinations of hydrogen or helium to the ground state would produce ionizing photons which would be quickly absorbed by other atoms of the recombined species. In this case OTS is an excellent approximation (Van Blerkom and Hummer 1967; Bässgen, Bässgen, and Grewing 1988). However, other opacity sources are present, and these compete in absorbing protons produced by recombinations, making the recombination process more efficient than the OTS approximation would suggest. The recombination coefficients for all states of hydrogen and helium are modified by the presence of other opacity sources, such as grains, free-free or H⁻ absorption, and the heavy element opacities, in the following manner. The net effective recombination rate coefficient (cm³ s⁻¹) to level n, $\hat{\alpha}(T_e, n)$, is written in terms of the spontaneous radiative recombination rate coefficient $\alpha(T_e, n)$, the escape probability for continuum photons described above, and the opacities (cm⁻¹) κ_n and κ_o for the level n and other opacity sources respectively, as

$$\hat{\alpha}(T_e, n) = \alpha(T_e, n) \left\{ P_c(n) + [1 - P_c(n)] \left(\frac{\kappa_o}{\kappa_o + \kappa_n}\right) \right\} \quad , \tag{58}$$

and $P_c(n)$ is the continuum escape probability defined below (equation 71). In general, $P_c(n)$ varies between 0 and 0.5 for an optically thick open geometry (see, for example Davidson 1977), $P_c(n) \sim 1$ if the gas is optically thin, and $P_c(n) \sim 0$ for ground states if the gas is optically thick and the geometry is closed. All computed opacity sources are included in κ_o .

These recombination continua produce a flux of on-the-spot photons, ϕ_{OTS} (cm⁻² s⁻¹). The OTS photoabsorption rate Γ_{OTS} (s⁻¹), used to determine the ionization or heating rate for the gas or grain constituents, is then $\Gamma_{OTS} = \alpha \phi_{OTS}$ where α is the photoabsorption cross section for the individual species. The OTS flux is related to the spontaneous recombination rate coefficient by

$$\phi_{OTS} = \alpha(T_e, n) N_e N_{ion} \left[\frac{1 - P_c(\tau)}{\kappa_o + \kappa_n} \right] \quad cm^{-2} \ s^{-1} \tag{59}$$

where N_{ion} is the ion in question. These are stored in the vectors OTSCON and OTSLIN.

14.7 Continuum Normalization

The continuum renormalization is performed in routine CONORM. The incident continuum can either be specified as a luminosity radiated into 4π sr, or as a surface flux, per unit area of cloud at the illuminated face. In most cases there is no ambiguity. For those where there is, the continuum is assumed to be the relevant quantity radiated into 4π sr if the resulting ionization parameter lies between 10^{10} and 10^{-15} , and a surface flux otherwise.

14.8 Continuum Generation

The continuum is generated by the function "FFUN". FFUN has a single argument, the energy in Rydbergs, and it returns the number of photons per unit area, time, and

Rydberg, at that energy. FFUN sums over all the specified continua and applies the appropriate normalization factors. Another function, FFUN1, evaluates each individual continuum, and is normally called by FFUN.

The units, and their conversion to other measures of the continuum, are

$$\phi_{\nu}(\nu) = FFUN(\nu) \quad photons \ cm^{-2} \ s^{-1} \ Ryd^{-1}$$
 (60)

$$FLUX(\nu) = \phi_{\nu}(\nu) \,\delta\nu_i = FFUN(\nu) \times WIDFLX(\nu) \quad photons \ cm^{-2} \ s^{-1} \tag{61}$$

$$f_{\nu}(\nu) = FFUN(\nu) h\left(\frac{\nu}{\nu_{912}}\right) \quad erg \ cm^{-2} \ s^{-1} \ Hz^{-1} \quad .$$
(62)

14.9 Energy Units; The Rydberg

Continuum energies are usually given in Rydbergs. One Rydberg is approximately equal to the ionization potential of hydrogen, which is

$$R_H \equiv 2.178728 \times 10^{-11} \ erg = 13.59842 eV = 911.76340 \text{\AA} = 109677.576 \ cm^{-1} \ . \tag{63}$$

This was the Rydberg unit used by CLOUDY before 1988, and is not the more commonly used R_{∞} , for infinite mass nuclei.

At present the energy scale is being converted to R_{∞} . In this unit, the wavenumber corresponding to R_{∞} is

$$R_{\infty} = \frac{2\pi^2 m_e e^4}{ch^3} = 109737.312 \ cm^{-1} \ , \tag{64}$$

the wavelength in vacuum is

$$1/R_{\infty} = 911.26708 \mathring{A} , \qquad (65)$$

the frequency is

$$c R_{\infty} = 3.289842 \times 10^{15} \, s^{-1} \,, \tag{66}$$

and this corresponds to an energy

$$1 Ryd = chR_{\infty} = 2.17992 \times 10^{-11} erg = 13.60583 \, eV \quad . \tag{67}$$

Thus the ionization potential of hydrogen is actually 0.99946 Ryd. This difference is significant since it enters as the third power in the photon phase-space conversion factor $2h\nu^3/c^2$.

Another commonly used unit is the "atomic unit", also called the Hartree, which is equal to two Rydbergs (i.e., $2R_{\infty}$).

To convert from	Code Variable	to	multiply by
$photons/s/cm^2$	FLUX	$f_{ u}$	$\nu_{Ryd} h \nu_1(erg)$
$ m photons/Ryd/s/cm^2$	FLUX/WIDFLX	$ u f_{ u}$	$ u_{Ryd}^2 h u_1(\mathrm{erg})$
energy, T	ANU, TE	$h\nu/kT$	1.57890(5)*ANU/TE

Table 15: Continuum Conversion Factors

14.10 Conversion Factors

Table 15 gives conversion factors between various common units of continuous emission.

15 LINE AND CONTINUUM TRANSFER

Optical depths and escape probabilities are computed for *all* permitted and intercombination lines which are significant coolants. The cooling is usually distributed among many lines in high density models, and these lines are usually optically thick.

15.1 Thermalization Length

Radiative transfer will affect the thermal equilibrium of the gas when the collision timescale approaches an effective lifetime $\tau \sim (A_{ul}/N_{scat})^{-1}$, where A_{ul} is the transition probability and N_{scat} is the number of scatterings a line photon undergoes before escape. For permitted metal lines (which often have optical depths $\sim 10^4 - 10^6$) line thermalization becomes important at densities $N > 10^{15}/\tau \sim 10^{10}$ cm⁻³. These effects are important for hydrogen at considerably lower densities. Additionally, continuum transfer affects the ionization and thermal equilibrium of the gas at all densities.

15.2 Optical Depths

The line center optical depth for a transition u - n, where u is the upper level, is given by (Mihalas 1978)

$$d\tau_{n,u} = \alpha_{\nu} \left(N_n - N_u g_n / g_u \right) f(r) dr$$
(68)

where f(r) is the filling factor. The absorption cross section α_{ν} is related to the oscillator strength f by

$$\alpha_{\nu} = \frac{\pi^{1/2} e^2 \lambda f}{m_e c v} \phi_{\nu} \tag{69}$$

 with

$$v^2 = 2kT/m_A + v_{turb}^2 \tag{70}$$

the line-width (cm s⁻¹), as determined by the local electron temperature. The micro-turbulent velocity v_{turb} is assumed to be zero unless it is reset with the "TURBULENCE" command.

15.3 Mean vs Line Center Optical Depths

CLOUDY tries to work with line center optical depths throughout (see, for example, Mihalas 1978). In many places routines or approximations using *mean* optical depths are encountered (eg, Hummer and Kunasz 1980). The line center optical depth is $\pi^{1/2}$ times smaller than the mean optical depth.

15.4 The Continuum Escape Probability Function

Recombination to level n_o produces radiation capable of ionizing levels $n \ge n_o$. The transport of this radiation can be treated with variations of the "on-the-spot" approximation (Van Blerkom and Hummer 1967; 1968; Davidson and Netzer 1979; Netzer and Ferland 1984; Osterbrock 1988; Bassgen et al. 1988). If hydrogen is the dominant opacity and the photoelectric cross section varies as $(\nu/\nu_o)^{-3}$, then the probability of escape of a photon is given by

$$P_{c}(\tau, h\nu_{o}/kT) = \frac{\int_{1}^{\infty} x^{-1} E_{2}(\tau_{o}x^{-3}) \exp\left(-h\nu_{o}(x-1)/kT\right) dx}{\int_{1}^{\infty} x^{-1} \exp\left(-h\nu_{o}(x-1)/kT\right) dx}$$
(71)

where $\tau_{\rm o}$ is the optical depth at threshold, which has energy $h\nu_{\rm o}$, and $x \equiv h\nu/h\nu_{\rm o}$. No simple approximation is obvious, and the function is integrated numerically.

Figure 5 shows P_c . The escape probability decreases as the optical depth increases in the expected nearly exponential manner. It also decreases with decreasing $h\nu_o/kT$. Physically, as the gas temperature increases relative to the threshold energy, recombining photons are created further from threshold, where the optical depth of the gas is smaller. For small $h\nu/kT$ and large optical depths, the escape probability is several orders of magnitude larger than that suggested by the optical depth at threshold alone. For large $h\nu/kT$ the escape probability is nearly $E_2(\tau)$, as expected.

15.5 The Line Escape Probability Function

At low densities, line scattering for a two level atom is coherent in the atom's reference frame, and the line profile function is described by the incomplete redistribution function. At high densities the Stark effect can broaden the line, while, when the radiation density is high, scattering within excited states can broaden resonance lines such as $Ly\beta$ (line interlocking), destroying the coherence of the scattering process. In these cases complete redistribution more closely describes the scattering process. CLOUDY uses two escape probability functions to take these processes into account.

Line transfer can be described by either complete or partial redistribution. Which is the case is determined by the detailed processes affecting the level populations and line transport. In this work the lines are divided into two groups; strong resonance lines which are treated with partial redistribution with a Voigt profile, and subordinate lines, which are treated with complete redistribution in a Doppler core.

15.5.1 Background opacity

The ratio of continuous to line opacity is parameterized as

$$X_c = \frac{\kappa_c N_c}{\kappa_l N_l + \kappa_c N_c} \tag{72}$$

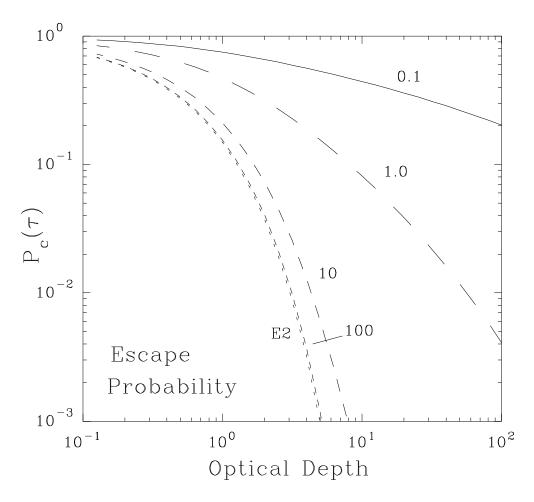


Figure 5: Continuum escape probability function. The continuum escape probability P_c is shown as a function of the optical depth at threshold, for a variety of values of the ratio $h\nu/kT$, where $h\nu$ is the energy at threshold. For small $h\nu/kT$ recombining photons are emitted far from threshold and escape freely, even for large optical depth. conesc

where κ is the opacity and the N's the number of absorbers.

15.5.2 Incomplete redistribution

Incomplete redistribution is assumed for resonance transitions such as C IV $\lambda 1549$ and the Ly α transitions of hydrogen and helium. Two studies of line formation using this approximation are those of Bonilha et al. (1979) and Hummer and Kunasz (1980). Both studies suggest escape probabilities of the form

$$P_l(\tau) = \{1 + b(\tau)\tau\}^{-1} \quad , \tag{73}$$

but there is substantial disagreement in the form and value of the factor $b(\tau)$, sometimes by more than a factor of 2. (This is after due allowance for the different definitions of line opacities in the two papers.) CLOUDY uses the Hummer and Kunasz results.

The damping constant a is given by

$$a = \frac{\Gamma}{4\pi\Delta\nu_D} = \frac{\lambda\sum A}{4\pi\nu_{Dop}} \tag{74}$$

where Γ is the sum of the A's from the upper level, and $\Delta \nu_D$ is the Doppler width in frequency units (Mihalas 1978) and v_{Dop} is the Doppler width in cm⁻¹. The code stores the ratio $\Gamma \lambda/4\pi$ in the vectors DAMPLN, HDAMP, HE1DMP, and HE2DMP. The *a*'s are then evaluated in the routines deriving the escape probabilities.

The escape and destruction probability functions used for HI, HeI, and HeII Ly α and strong resonance lines such as CIV λ 1549 is that described by Hummer and Kunasz (1980). Their tabulated values were fitted by interpolation.

15.5.3 Complete redistribution

Lines arising from excited states (hydrogen Balmer, Paschen, etc.) and Lyman lines with $n_{upper} > 2$ are treated assuming complete redistribution in a Doppler core (i.e., the damping constant *a* is assumed to be zero). In this case, if the total optical depth of the slab is *T*, then the escape probability at a depth τ from the illuminated face is given by;

$$P_l(\tau, T, X_c) = [1 - X_c F(X_c)] \frac{1}{2} [K_2(\tau, X_c) + K_2(T - \tau, X_c)] \quad , \tag{75}$$

and the destruction probability is

$$D_l(X_c) = X_c F(X_c) \quad . \tag{76}$$

The function

$$F(X_c) = \int_{-\infty}^{+\infty} \frac{\phi(x)}{X_c + \phi(x)} dx \quad , \tag{77}$$

where $\phi(x) \approx \pi^{-1/2} \exp(-x^2)$ is the Voigt function, is interpolated from the tables presented by Hummer (1968). The function

$$K_2(\tau, X_c) \equiv \frac{1}{1 - X_c F(X_c)} \int_{-\infty}^{+\infty} \frac{\phi^2(x)}{X_c + \phi(x)} E_2\left[(X_c + \phi(x)) \tau \right] dx$$
(78)

is evaluated numerically.

15.5.4 Level populations and emission

The radiative line de-excitation rate is given by

$$\left(\frac{dN_u}{dt}\right)_{rad} = N_u A_{u,l} \left(P_l + D_l\right) - N_l A_{u,l} \eta \gamma_{u,l} \tag{79}$$

where η is the photon occupation number of the external radiation field and $\gamma_{u,l}$ is the escape probability described by Castor (1970).

The emission from a transition between the level n to a lower level l is then simply

$$4\pi j(nl) = N_n \ A_{nl} \ h\nu_{nl} \ P_l(\tau_{nl}) \ f(r)$$
(80)

where $P_l(\tau_{nl})$ is the line escape probability (Elitzur et al. 1983; Elitzur 1984). The local cooling rate due to the line is related to the volume emissivity of the line by

$$\Lambda_{ul} = 4\pi j(h\nu) = N_u A_{u,l} f(r) P_l(\tau, T, X_c) h\nu = (N_l C_{l,u} - N_u C_{u,l}) f(r) h\nu$$
(81)

and the local flux $(cm^{-2} s^{-1})$ of "on-the-spot" (OTS) photons caused by line loss (used to compute heating or photoionization rates for the sources of the background opacity) is

$$\phi_{\text{OTS}} = \frac{N_u A_{u,l} D_l(X_c)}{\kappa_c N(c)} \quad . \tag{82}$$

The ratio of inward to total line intensity is then given by

$$\frac{4\pi j(in)}{4\pi j(total)} = \frac{K_2(\tau, X_c)}{[K_2(\tau, X_c) + K_2(T - \tau, X_c)]}$$
(83)

15.5.5 Stark broadening

Distant collisions with charged particles broaden the upper level of lines, and in the limit of very high densities this will make the scattering process completely non-coherent even for Ly α (i.e., complete redistribution obtains). CLOUDY closely follows the treatment of Puetter (1981) in treating Stark broadening. For transitions described by incomplete redistribution a total escape probability $P_{l, tot}$ given by

$$P_{l, tot} = \min\left(P_{inc} + P_{Stark} , P_{com}\right) \tag{84}$$

is defined, where the escape probabilities are those for incomplete, Stark, and complete redistribution respectively. The total effective escape probability is not allowed to exceed the complete redistribution value for $\tau > a^{-1}$.

15.5.6 Net escape probability

If τ is the optical depth in the direction towards the source of ionizing radiation and T is the total optical depth then the escape probability entering the balance equations is

$$P_l(\tau, T) = \{P_l(\tau) + P_l(T - \tau)\}/2 \quad . \tag{85}$$

In general the total optical depth T is only known after the first iteration, so more than one iteration must be performed when radiative transfer is important. The optical depth scale is usually well defined after the first iteration, so that reliable results are often obtained in two iterations, but more iterations may be required under some circumstances. A warning will be printed after the last zone calculation if the optical depth scale has not yet converged.

15.6 The Optical Depth Arrays

The terms open and closed geometry are defined in section 2.2 above. The treatment of transfer in these two limits is described here.

15.6.1 Open geometry

This is the default. During the first iteration the escape probability is defined using only optical depths accumulated in the inward direction. This optical depth is initialized to TAUMIN, a very small number, at the start of the calculation. At the end of the first iteration the total optical depth is set to the optical depth accumulated in the inward direction. At the end of subsequent iterations the total optical depth is defined as a mean of the new and old inward optical depths.

15.6.2 Closed expanding geometry

This is the default if the "SPHERE" command is entered. In this case it is assumed that line photons do not interact with the "other" side of the expanding spherical nebula. The treatment of the optical depths is entirely analogous to that described for an open geometry, since the presence of the distant material has no effect on line transfer.

15.6.3 Closed static geometry

This is assumed if the "SPHERE STATIC" command is entered. In this case line photons from all parts of the spherical shell do interact. As a result, the optical depth scale is poorly defined on the first iteration, and more than one iteration is required. On second and later iterations the total line optical depth is set to twice the optical depth of the computed structure, and the optical depth at the illuminated face of the shell is set to half of this. The optical depth scale is only reliably defined after at least a second iteration.

15.6.4 Wind

The model is a large velocity gradient ($v \sim R$ Sobolev approximation) wind. The effective optical depth is given by;

$$\tau_{lu}(R) = \kappa_{lu} \left(N_l - N_u \frac{g_l}{g_u} \right) R \frac{v_{thermal}}{v_{expansion}}$$
(86)

where $v_{thermal}$ and $v_{expansion}$ are the thermal and expansion velocities respectively. Iteration is often not required in this type of model since the line optical depth is entirely defined locally. Iteration will be required if the geometry is optically thin in the ionizing continuum (matter bounded), since the code assumes that the cloud will be radiation bounded on the first iteration. A comment will be printed at the end of the calculation if another iteration is needed.

15.6.5 Hydrogen

Several arrays are defined to store information related to the hydrogen optical depth scale and escape probabilities. The escape probability for the transition u—l is stored as the element HESC(u,l), while the effective transition rate (the spontaneous rate multiplied by the escape probability) is stored in HESC(l,u). The optical depth for the center of the zone is stored in HTNEXT(u,l); this includes corrections for stimulated emission so it may be negative. (A comment is printed if a level inversion occurs.) The fraction of the escapes which occur in the inward direction is stored in HFRCIN(u,l). The Stark contribution to the total escape probability is stored in PESTRK(u,l); PESTRK(l,u) contains this escape probability multiplied by the spontaneous transition rate for the u—l transition. The array HDEST contains the corresponding arrays of destruction rates.

15.6.6 Helium

The treatment of singlet and ionized helium is entirely analogous to that of hydrogen. Many of the variables have similar names.

15.6.7 The heavy elements

The arrays defining the heavy element optical depths, escape probabilities, and inward escaping fractions, are stored in common block TAU. Each emission line is represented by a vector with dimension four. The first element of the vector is the optical depth in the inward direction (i.e., towards the illuminated face of the cloud), and is incremented in subroutine TAUINC. The second element is the total optical depth through the cloud, computed in the previous iteration. The third element of the vector is the escape probability for the line, and the last element is the fraction of the line escaping in the inward direction. The escape probabilities are evaluated in METESC.

The correction for stimulated emission is neglected in the optical depth scale for UV lines of heavy elements. As a result the optical depths must be greater than zero, and the escape probability must be less than unity. This approximation is reasonable for ultraviolet transitions at nebular temperatures.

15.6.8 Fine structure lines

The vector FSTAUS contains information concerning the "fine structure" lines; defined here as lines arising within levels of split ground terms. These forbidden lines may become optically thick, and may mase under some circumstances. The first element in FSTAUS is the optical depth in the inner direction. The second element is the total optical depth, as computed in the previous iteration. Both include the correction for stimulated emission, and can be negative. The third element is the escape probability evaluated by the function ESCFS,

$$P_l(\tau) = \frac{1 - \exp\left(-\tau\right)}{\tau} \tag{87}$$

which will be greater than unity if a population inversion occurs and $\tau < 0$. The next element of the array is the opacity in the transition, as computed by the section of the code which does level populations. This opacity includes the correction for stimulated emission and will be negative if a population inversion occurs. The last element is a

pointer to the line frequency. This is used to take continuum pumping into account. The escape probabilities are evaluated in METESC.

16 THE MODEL HYDROGEN ATOM

CLOUDY is designed to model environments which range from the low density limit to LTE. Hydrogen is treated as a ten-level atom. Level 2s and 2p are treated separately, while $3 \leq n \leq 6$ are treated assuming full *l*-mixing. The atom is completed with three supplemental levels chosen to mimic the average properties (averaged over level population assuming LTE at $T_e \sim 10^4$ K) of levels 7–10, 11–20, and 21–100 respectively; inclusion of these levels is necessary because recombination (both collisional and radiative) to high-*n* levels can eventually populate the lower levels which produce the observed lines. The atomic data for the upper three levels are given in Cota (1987).

Tests in the low-density, or nebular, limit show that the model atom predicts level populations and emissivities which are in much better than 1% agreement with Seaton (1959), who also assumed a well *l*-mixed hydrogen atom but considered many more levels. The three pseudo-states are well-coupled to the continuum for many conditions of interest; their main effect is to increase the populations of low levels by radiative and collisional deexcitation, and hence affect the ionization balance.

Pressure shielding lowers the ionization potential of the atom to include typical energies within the level representing $21 \le n \le 100$ when the density is greater than $N_e \sim 6 \times 10^{14} (T/10^5 K) \text{ cm}^{-3}$ (Mihalas 1978). As a result the population of the highest level will be overestimated, and hence the neutral hydrogen density, by a small amount. This effect is compensated for by not counting the three pseudo-states in the summation over level populations to determine the neutral hydrogen fraction in the charge-conservation equation.

Departure coefficients, rather than actual level populations, are used in the solution of the hydrogen level populations. The LTE relative population density for level n is stored in the vector PLTE and is given by

$$P_{n}^{*} = \frac{N_{n}^{*}}{N_{e}N_{p}} = \frac{g_{n}}{g_{e}g_{p}} \left(\frac{h^{2}}{2\pi m kT}\right)^{3/2} \exp(\chi_{n})$$
(88)

$$= \frac{g_n}{g_e g_p} 4.14158 \times 10^{-16} T^{-3/2} \exp(\chi_n) \ cm^3 \tag{89}$$

where $g_e = 2$, $g_p = 1$, and $g_n = 2n^2$ are the statistical weights, N_n^* is the LTE population of level $n \, (\text{cm}^{-3})$, and the other symbols have their usual meaning. Here

$$\chi_n = \frac{I_n}{kT} = \frac{15.789 \times 10^4 Z^2}{n^2 T} \tag{90}$$

where I_n is the ionization threshold for level n and Z is the nuclear charge. The departure coefficients are stored in the vector HBN and are related to the LTE relative

population density by

$$b_n = N_n / P_n^* N_e N_p \tag{91}$$

where N_n is the actual population of the level.

Boltzmann factors for transitions between levels are stored in the array

$$HLBOLT(l, u) \equiv \exp\left(\chi_u - \chi_l\right) \tag{92}$$

which is evaluated in subroutine HCOLST. Boltzmann factors for levels relative to the continuum are stored in the vector

$$HCBOLT(n) \equiv \exp(-\chi_n)$$
 . (93)

16.1 Recombination Rates and Cooling

State specific rates for radiative recombination and radiative recombination cooling are needed for the temperature range $10 \text{K} \leq T_e \leq 10^{10} \text{K}$. The methods and assumptions used to derive these for hydrogenic ions is described here.

16.1.1 Formalism

The Milne relation for the state-specific radiative recombination rate coefficient (cm^3 s⁻¹) to a level n can be expressed as (Brown and Mathews 1974; Gould 1978; Mihalas 1978);

$$\alpha_n(T) = \left(\frac{2\pi mk}{h^2}\right)^{-3/2} \frac{8\pi}{c^2} \frac{g_n}{g_e g_{ion}} T^{-3/2} \int_{h\nu_o}^{\infty} \nu^2 \alpha_\nu(n) \exp\left(-h\left(\nu - \nu_o\right)/kT\right) d\nu \tag{94}$$

= $4.12373 \times 10^{11} \frac{g_n}{g_e g_{ion}} T^{-3/2} \int_{h\nu_o}^{\infty} \nu^2 \alpha_\nu(n) \exp\left(-h\left(\nu - \nu_o\right)/kT\right) d\nu_{Ryd} (95)$

where the g's are the statistical weights of the constituents, $h\nu_{Ryd}$ is the photon energy in Rydbergs, $h\nu_o \sim z^2/n^2$ is the ionization potential in Rydbergs, $\alpha_{\nu}(n)$ is the photoionization cross section, and the other symbols have their usual meanings.

In implementing this formalism the fact that, for hydrogen, the energy scale is shifted by the ratio of the reduced mass of the nucleus to an infinite mass was explicitly taken into account. If the energy of level n of hydrogen is n^{-2} R_H, then the coefficient appearing in the exponential is 157807, not the commonly quoted 157890. This does affect the results slightly since the energy scale enters as an exponential in equation 94.

Hydrogenic photoionization cross sections are required over a very wide range of energy since recombination coefficients over a wide range of temperature are needed. Cross sections $\alpha_{\nu}(n)$ were calculated using a program based on routines developed by Hummer (1988) and Storey and Hummer (1990, and private communication). The program generates the cross section values at arbitrary photon energies for all hydrogenic (n,l) states, as well as for the total n, employing analytic expressions and some very accurate expansions and numerical procedures. The calculations were carried out at a number of different mesh sizes to check for convergence. The results are typically accurate to better than 0.1 percent.

The recombination cooling rate coefficient (erg cm³ s⁻³) is given by

$$kT\beta(T,n) = \left(\frac{2\pi mk}{h^2}\right)^{-3/2} \frac{8\pi}{c^2} \frac{g_n}{g_e g_{ion}} T^{-3/2} \int_{h\nu_o}^{\infty} \nu^2 \sigma_\nu(n) h\left(\nu - \nu_o\right) \exp\left(-h\left(\nu - \nu_o\right)/kT\right) d\nu$$
(96)

Again, the integration is carried out numerically.

16.1.2 Results

The numerical results are presented in Tables 16 and 17. The first column of the table gives the log of the temperature, columns 2 through 7 give the total recombination coefficient for $1 \le n \le 6$ summed over *l* states. Columns 8, 9 and 10 give the total recombination coefficient for levels 7–10, 11–20, and 21–1000 respectively. The last column gives the case B sum, $2 \le n \le 1000$. A very large temperature range is considered for completeness; actually, at very low temperatures three-body recombination predominates for most densities (Bates et al. 1963), while at very high temperatures other processes (i.e., Compton scattering, collisions) dominate the balance and the neutral fraction is vanishingly small.

Table 16: Hydrogen recombination coefficients State Specific and Case B Recombination Coefficients¹

State Specific and Case B Recombination Coefficients ¹										
$\log(T_e)$	1	2	3	4	5	6	7 - 10	11 - 20	21—	case B
0.5	9.258-12	5.087 - 12	3.512 - 12	2.684 - 12	2.172 - 12	1.825 - 12	5.303 - 12	7.495 - 12	2.950-11	5.758 - 11
1.0	5.206 - 12	2.860 - 12	1.974-12	1.508 - 12	1.220-12	1.025 - 12	2.974 - 12	4.176 - 12	1.335 - 11	2.909 - 11
1.5	2.927 - 12	1.608 - 12	1.109 - 12	8.465 - 13	6.842 - 13	5.737 - 13	1.658 - 12	2.285 - 12	5.638 - 12	1.440 - 11
2.0	1.646-12	9.028-13	6.216 - 13	4.732 - 13	3.811-13	3.183-13	9.081-13	1.193 - 12	2.173 - 12	6.971 - 12
2.5	9.246-13	5.055 - 13	3.460-13	2.613-13	2.084 - 13	1.720-13	4.753-13	5.656 - 13	7.476-13	3.282-12
3.0	5.184-13	2.805 - 13	1.888-13	1.395-13	1.085-13	8.717-14	2.260-13	2.316-13	2.273-13	1.489-12
3.5	2.890-13	1.517-13	9.779-14	6.884-14	5.099-14	3.912-14	9.264-14	8.016-14	6.177-14	6.430-13
4.0	1.582-13	7.699 - 14	4.555 - 14	2.965 - 14	2.053-14	1.487-14	3.203-14	2.381 - 14	1.535 - 14	2.588-13
4.5	8.255-14	3.461-14	1.812-14	1.076-14	6.953-15	4.775 - 15	9.492 - 15	6.277 - 15	3.568 - 15	9.456-14
5.0	3.882-14	1.316-14	6.059-15	3.314-15	2.022 - 15	1.331-15	2.495 - 15	1.517 - 15	7.897-16	3.069-14
5.5	1.545 - 14	4.196 - 15	1.736 - 15	8.918-16	5.219-16	3.335-16	5.999 - 16	3.444-16	1.690-16	8.793-15
6.0	5.058 - 15	1.146 - 15	4.392 - 16	2.160-16	1.229-16	7.694 - 17	1.347 - 16	7.434 - 17	3.510 - 17	2.245 - 15
6.5	1.383-15	2.760 - 16	1.005 - 16	4.807-17	2.685 - 17	1.660 - 17	2.854 - 17	1.535 - 17	7.088-18	5.190 - 16
7.0	3.276-16	6.031-17	2.129 - 17	1.000-17	5.523 - 18	3.385-18	5.756 - 18	3.044-18	1.399-18	1.107-16
7.5	7.006-17	1.227 - 17	4.251-18	1.976-18	1.083-18	6.606-19	1.115-18	5.836-19	2.709 - 19	2.221 - 17
8.0	1.398 - 17	2.377 - 18	8.139-19	3.759-19	2.052 - 19	1.248-19	2.097 - 19	1.090-19	5.179-20	4.267-18
8.5	2.665 - 18	4.455-19	1.515 - 19	6.970-20	3.796-20	2.303-20	3.862-20	2.000-20	9.743 - 21	7.960-19
9.0	4.940-19	4.435-19 8.175-20	2.769-20	1.271-20	6.913-21	4.190-21	7.015-21	3.625-21	1.819-21	1.457-19
9.5	9.001-20	1.481-20	5.005-20	2.294-21	1.247-21	7.552-22	1.263-21	6.518-22	3.382-22	2.636-20
10.0	1.623-20	2.662-21	8.985-22	4.116-22	2.235-22	1.354-22	2.263-21	1.167-22	6.267-23	4.737-21

 1 The entry 9.258-12 indicates a rate coefficient of $9.258\times 10^{-12}~{\rm cm}^3~{\rm s}^{-1}.$

Table 17: Recombination cooling coefficients State Specific and Case B Recombination Cooling Coefficients¹

	State Specific and Case B Recombination Cooling Coefficients									
$\log(T_e)$	1	2	3	4	5	6	7 - 10	11 - 20	21 -	case B
0.5	4.025 - 27	2.211 - 27	1.527 - 27	1.167 - 27	9.441 - 28	7.929 - 28	2.303 - 27	3.245 - 27	1.076-26	2.295 - 26
1.0	7.158 - 27	3.932 - 27	2.713 - 27	2.072 - 27	1.676-27	1.406 - 27	4.072 - 27	5.667 - 27	1.442 - 26	3.595 - 26
1.5	1.273 - 26	6.985 - 27	4.815 - 27	3.671 - 27	2.962 - 27	2.479 - 27	7.119-27	9.559 - 27	1.755 - 26	5.514 - 26
2.0	2.262 - 26	1.239-26	8.507 - 27	6.451 - 27	5.171 - 27	4.293 - 27	1.203 - 26	1.481 - 26	1.870-26	8.236 - 26
2.5	4.015 - 26	2.184 - 26	1.483-26	1.107 - 26	8.708 - 27	7.074 - 27	1.872 - 26	1.958-26	1.689-26	1.187 - 25
3.0	7.099 - 26	3.785 - 26	2.488 - 26	1.784-26	1.341 - 26	1.039-26	2.480 - 26	2.081 - 26	1.296-26	1.629-25
3.5	1.241 - 25	6.245 - 26	3.796 - 26	2.505 - 26	1.740-26	1.255 - 26	2.632 - 26	1.776-26	8.745 - 27	2.082 - 25
4.0	2.094 - 25	9.195 - 26	4.856-26	2.845 - 26	1.795 - 26	1.198-26	2.236 - 26	1.277 - 26	5.443 - 27	2.395 - 25
4.5	3.234 - 25	1.112 - 25	4.923-26	2.557 - 26	1.483 - 26	9.305 - 27	1.600 - 26	8.219 - 27	3.240 - 27	2.376 - 25
5.0	4.173 - 25	1.056-25	3.990-26	1.891 - 26	1.034 - 26	6.240 - 27	1.022 - 26	4.955 - 27	1.882 - 27	1.981 - 25
5.5	4.149 - 25	7.981 - 26	2.698 - 26	1.208-26	6.389 - 27	3.771 - 27	6.026 - 27	2.839 - 27	1.071 - 27	1.390-25
6.0	3.121 - 25	4.961 - 26	1.572 - 26	6.827 - 27	3.549 - 27	2.073 - 27	3.273 - 27	1.523 - 27	5.885 - 28	8.316-26
6.5	1.843 - 25	2.616-26	8.015 - 27	3.429 - 27	1.768 - 27	1.028-27	1.614 - 27	7.468 - 28	3.080 - 28	4.307 - 26
7.0	9.016-26	1.204 - 26	3.628 - 27	1.541 - 27	7.917 - 28	4.591 - 28	7.194 - 28	3.321 - 28	1.547 - 28	1.967-26
7.5	3.847 - 26	4.978 - 27	1.487 - 27	6.296 - 28	3.229 - 28	1.870 - 28	2.928 - 28	1.350-28	7.626 - 29	8.109 - 27
8.0	1.490-26	1.897 - 27	5.644 - 28	2.385 - 28	1.222 - 28	7.077 - 29	1.107 - 28	5.104 - 29	3.799 - 29	3.092 - 27
8.5	5.397 - 27	6.811 - 28	2.023 - 28	8.541 - 29	4.375 - 29	2.533 - 29	3.962 - 29	1.826-29	1.924-29	1.115 - 27
9.0	1.867 - 27	2.346 - 28	6.959 - 29	2.937 - 29	1.504 - 29	8.706-30	1.362 - 29	6.274 - 30	1.006-29	3.872 - 28
9.5	6.261 - 28	7.849 - 29	2.327 - 29	9.820 - 30	5.028 - 30	2.910 - 30	4.551 - 30	2.097 - 30	5.410 - 30	1.316-28
10.0	2.057 - 28	2.575 - 29	7.633 - 30	3.220 - 30	1.649-30	9.543 - 31	1.492 - 30	6.876-31	2.978 - 30	4.436-29

¹The entry 4.025-27 indicates a rate coefficient of 4.025×10^{-27} erg cm³ s⁻¹.

As tests, these predictions of the recombination rate coefficients are compared with those of Seaton (1959), Ferland (1980), Hummer and Storey (1987), and Martin (1988). (Note that the total recombination rate given by Hummer and Storey is the sum of radiative and net three-body recombination. For this comparison their results for a density of 10^2 cm⁻³ were used to minimize the contribution of the second process.) The agreement with all of these results is good, usually much better than 1 percent. Seaton (1959) calculates the recombination cooling coefficients. The present results agree with his to better than 5 percent. Figure 6 shows the recombination cooling coefficient for several states.

16.1.3 Rational approximations

It is not numerically expedient to compute these rate coefficients on-the-fly in large scale ionization/thermal structure calculations. The rate coefficients were fitted with a high-order rational approximation. The recombination rate coefficient is expressed as

$$\alpha(T,n) = 10^{F(T,n)} T^{-1}$$
(97)

with

$$F(T,n) = \frac{a_n + c_n x + e_n x^2 + g_n x^3 + i_n x^4}{1 + b_n x + d_n x^2 + f_n x^3 + h_n x^4}$$
(98)

and $x \equiv log(T)$. The coefficients are listed in Table 18. These approximations reproduce the numerical results with a mean error well below 0.1 percent. For levels below n = 20 the largest error is also under 0.1 percent, although errors as large as 1.4 percent occur for the highest sum at temperatures below 100K.

Recombination cooling coefficients were fitted to equations of the form

$$kT\beta(T,n) = 10^{F(T,n)}$$
 (99)

where F(T,n) is given above, and the fitting coefficients are listed in Table 19. The errors in fitting these coefficients is larger, typically 0.5 percent, but sometimes as large as several percent.

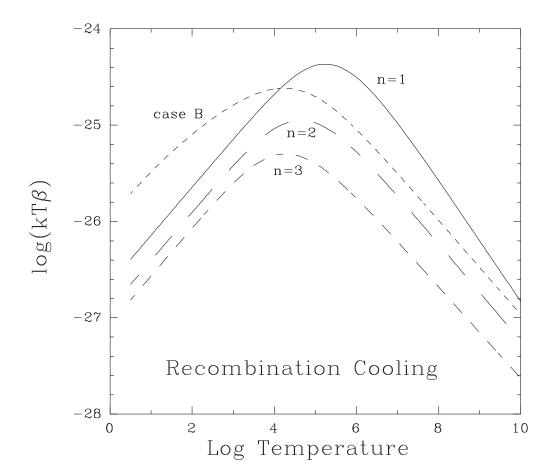


Figure 6: The recombination cooling for several states is shown as a function of temperature. recool

Table 18: Expansion for recombination coefficients

	1											
n	а	b	С	d	е	f	g	h	i			
1	-10.7815	-0.388896	4.68469	0.0640438	-0.874235	-5.10248-03	0.081411	2.47761-04	-3.87713-03			
2	-11.0434	-0.393514	4.84334	0.0692118	-0.956856	-5.49930-03	0.092159	3.06273-04	-5.02483-03			
3	-11.2031	-0.424576	5.25370	0.0819237	-1.126131	-6.81708-03	0.114221	4.11653.04	-6.77511 - 03			
4	-11.3145	-0.439393	5.45398	0.0853755	-1.166601	-7.40060-03	0.118057	4.03664-04	-6.48848-03			
5	-11.4062	-0.436467	5.46028	0.0863856	-1.184309	-7.37118-03	0.119145	4.12342-04	-6.75160-03			
6	-11.4846	-0.442457	5.56951	0.0899756	-1.241026	-7.54870-03	0.125443	4.48713-04	-7.53579-03			
$\overline{7}$	-11.0213	-0.442776	5.37057	0.0943866	-1.252699	-7.44688-03	0.125435	4.88629-04	-8.30273-03			
8	-10.8751	-0.450383	5.39988	0.1022072	-1.341072	-7.17252-03	0.129801	5.52029-04	-9.92535-03			
9	-10.2096	-0.048286	0.85490	0.0453455	-0.474956	-1.01818-03	0.0	0.0	0.0			

Table 19: Expansion for recombination cooling coefficients

n	а	b	С	d	е	f	g	h	i
1	-26.6447	-0.405110	11.2923	0.0672574	-1.991084	- 5.08026-03	0.166268	2.05287-04	-7.13575-03
2	-26.9067	-0.416447	11.7104	0.0763838	-2.268984	-5.84929-03	0.196781	2.75885-04	-9.96306-03
3	-27.0620	-0.458344	12.8931	0.0899256	-2.651639	-7.48544-03	0.242675	3.39807-04	$-1.17865 \cdot 02$
4	-27.1827	-0.491379	13.8557	0.1022522	-3.023330	-8.56775-03	0.282237	4.14455-04	-1.46965-02
5	-27.2784	-0.519318	14.6735	0.1110161	-3.294623	-9.30673-03	0.310205	4.64233-04	-1.67032-02
6	- 27. 3596	-0.549712	15.5609	0.1195189	-3.566337	-9.84556-03	0.335160	5.12181-04	-1.88737-02
7	-26.9011	-0.562123	15.6545	0.1207284	-3.563036	-9.75175-03	0.332549	5.16213-04	-1.91249-02
8	-26.7582	-0.536972	14.9208	0.1093810	-3.253752	- 8.32192-03	0.293805	4.56629-04	-1.75719-02
9	-26.1477	-0.467188	12.6143	0.0821541	-2.411906	-8.17803-03	0.272395	5.99744 - 04	-2.00967-02

16.2 The Collisional Rate Equations

Considering only collisional terms, the departure coefficient for level n is given by

$$\frac{db_n}{dt} = \sum_l b_l C_{nl} + \sum_u \frac{P_u^*}{P_n^*} b_u C_{un} - b_n \left\{ \sum_l C_{nl} + \sum_u \frac{P_u^*}{P_n^*} C_{un} + C_{n\kappa} \left(1 - b_n^{-1} \right) \right\}$$
(100)

where the sums are over upper and lower levels. The collision rates (s^{-1}) are denoted by C_{ij} . The first term on the RHS represents collisional excitation to n from lower levels, the second is collisional deexcitation to n from higher levels, and the last term accounts for destruction processes. These include collisions to lower levels, upper levels, and the continuum. The factor multiplying the collisional ionization rate $C_{n\kappa}$ accounts for collisional ionization less three-body recombination. Note that this is often a net recombination process for the atom since, under many circumstances, $b_n < 1$.

Figure 7 shows a test case where collisional processes are dominant. All of the radiative processes discussed below are actually included, but the intensity of the external continuum is set to a very low (and hence negligible) value. As a result collisional and spontaneous radiative processes are dominant. The electrons are given a temperature of 50,000K, and the level populations and ionization of the gas are determined by solving the full set of equations of statistical equilibrium. The model is of a very thin cell of gas which is optically thin in the lines and continuum. Departure coefficients for the ground state, 2s, 2p, and 4 are shown.

As is well-known, the ground state is overpopulated relative to its LTE value when upward collisional processes are much slower than downward radiative processes; it is only when the collisional rates approach the radiative rates that b_1 approaches unity. The 2s level also has a large overpopulation for much the same reason; it is highly metastable and accumulates a large overpopulation until 2s - 2p collisions become fast enough to mix the two l levels. The more highly excited levels ($n \ge 3$) have a behavior very similar to that of n = 4, which is shown in the figure; they are underpopulated relative to their LTE value when radiative decays to lower levels are competitive with collisional processes. It is only at a density of $N_H > 10^{18}$ cm⁻³ that collisional processes completely dominate the rate equations, and the atom reaches LTE. The mean departure coefficient at a density of 10^{19} cm⁻³ is $\bar{b}_i = 1.0007 \pm 0.0022$ for the entire ten-level atom, and the largest single deviation from unity is 0.7% (for the ground state).

16.3 The Radiative Rate Equations

The photoionization rate (s^{-1}) from level *n*, stored in the vector HGAMNC(n), is given by

$$\Gamma_n = 4\pi \int_{\nu_o}^{\infty} \frac{J_{\nu}}{h\nu} \alpha_{\nu} d\nu$$
(101)

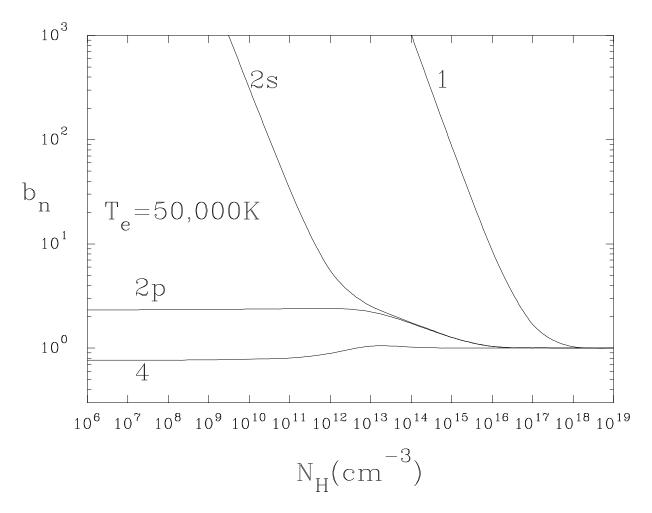


Figure 7: The equilibrium populations of the ground state and levels 2s, 2p, and 4 of the ten level hydrogen atom are shown as a function of the total hydrogen density N_H . The radiation field is set to a very low intensity, and the column density is kept small enough for optical depth effects to be negligible. A constant electron temperature of 5×10^4 K is assumed, so the gas is primarily collisionally ionized and excited. Levels 2sand 2p do not mix until a density of nearly 10^{14} cm⁻³ is reached, and do not come into LTE until the density is nearly 100 times higher. The entire atom is nearly in LTE at densities greater than 10^{18} cm⁻³. hbnvsn

and the induced recombination rate coefficient $(cm^3 s^{-1})$ by

$$\alpha(ind) = P_n^* 4\pi \int_{\nu_o}^{\infty} \frac{J_{\nu}}{h\nu} \alpha_{\nu} \exp(-h\nu/kT) d\nu \quad .$$
 (102)

This is evaluated at each zone by direct integration over the numerically binned continuum. Under most circumstances the population of the highest two pseudo-states is completely controlled by collisions; photoionization from these is neglected.

Spontaneous radiative recombination rate coefficients are computed as described above. The rate coefficients are evaluated in subroutine HTRANS and are stored in HREC(n,1) and have units $\text{cm}^3 \text{ s}^{-1}$. These recombinations produce ionizing radiation, and a recombination efficiency is defined to take this into account. These efficiencies are stored in the array HREC(n,i). Elements HREC(n,3) are the escape probabilities, computed including only the single-flight absorption due to the geometry, while the escape probabilities stored in HREC(n,2) include both this as well as destruction by the background absorbing continuum.

The full set of radiative balance equations can be written as

$$\frac{db_n}{dt} = \sum_l \frac{P_l^*}{P_n^*} b_l A_{nl} \frac{g_n}{g_l} \eta_{nl} \gamma_{nl} + \sum_u \frac{P_u^*}{P_n^*} b_u \left(A_{un}P_{un} + A_{un}\eta_{un}\gamma_{un}\right) + \left(\alpha(rad) + \alpha(ind)\right) / P_n^* - b_n \left(\sum_l \left(A_{nl}P_{nl} + A_{nl}\eta_{nl}\gamma_{nl}\right) + \sum_u A_{un} \frac{g_u}{g_n}\eta_{un}\gamma_{un} + \Gamma_n\right)$$
(103)

where the continuum occupation number in the transition ij is given by

$$\eta_{ij} \equiv J_{\nu}(ij)/(2h\nu_{ij}^3/c^2) = \left(\exp(h\nu/kT_{ex}) - 1\right)^{-1} \quad . \tag{104}$$

Here $J_{\nu}(ij)$ is the mean intensity of the net continuum at the line frequency, and T_{ex} is the excitation temperature of the continuum at the level frequency.

Two escape probabilities enter in equation 103. The first is the two-sided function which accounts for line scattering and escape

$$P(\tau, T) = (P(\tau) + P(T - \tau)) / 2$$
(105)

where τ is the optical depth at the center of the zone and T is the total optical depth. The second escape probability $\gamma_{ij}(\tau)$ accounts for the fraction of the primary continuum which penetrates to an optical depth τ and induces transitions between levels *i* and *j* (Castor 1970; Elitzur et al. 1983; Elitzur 1984). The terms in equation 103 correspond to induced upward transitions from lower levels, spontaneous and induced downward transitions from higher levels, spontaneous and induced capture to the level from the continuum, and destruction of the level by radiative transitions and photoionization. The product $A_{ul} P_l$ is stored in the array HEMIS(u,l). The continuum occupation number is stored in HJBAR(u,l), which is evaluated in HEVAL. The term $\eta A \gamma$ is stored as HCONT(u,l). The term $\sum_{u} A_{un} (g_u/g_n) \eta_{un} \gamma_{un}$ is stored in HBUL(n).

Figure 8 shows a test case which, in contrast with that shown in Figure 7, is dominated by radiative transitions. Again, the full set of equations coupling the levels are solved, but spontaneous and induced processes are more important than collisions for many values of the radiation density. The model is of a very thin cell of gas, so that all lines and continua are optically thin, has a density of $N_H = 10^{10}$ cm⁻³, and an electron temperature of 5×10^4 K. The gas is exposed to a black body continuum with a color temperature of $T_{color} = 5 \times 10^4$ K, but the intensity of this continuum is varied. This intensity is parameterized by an energy density temperature defined by $T_u \equiv (u/a)^{1/4}$ where u and a are, respectively, the actual radiation energy density and Stefan's radiation density constant.

A radiation field given by Planck's law (i.e., $T_u \equiv T_{color}$) forces the ionization and level population of an atom or ion to LTE in much the same way that high electron densities do. As Figure 8 shows, at very low values of T_u (low photon densities) the ground and n = 2 states are overpopulated for much the same reason that this occurs at low electron densities; the downward spontaneous radiative rates are fast relative to the induced (upward and downward) rates. At very low T_u (< 500K), $n \ge 3$ levels are underpopulated since they decay at a rate much faster than the induced rates (for $T_e = 5 \times 10^4$ K these levels have $h\nu \ll kT$, so induced processes will be fast relative to spontaneous rates when $T_u = T_{color}$ and the atom is in LTE). As T_u increases, fluorescence from the ground state over-populates excited states (because the ground state is itself overpopulated) and b_4 exceeds unity. Finally, in the limit where $T_u = T_{color}$, the departure coefficients reach unity and the atom goes to LTE. (The actual mean departure coefficient for the entire 10-level atom is $\bar{b}_i = 1.013 \pm 0.029$). Note that the vast majority of the neutral hydrogen population is in excited states when the atom approaches LTE at these temperatures.

16.4 Thermal Emission

16.4.1 Continuous emission

Diffuse emission (free-free and free-bound) by the model hydrogen atom is computed using the stored photoabsorption cross sections and detailed balance (i.e., the Milne relation; see Mihalas 1978).

Free-bound continua of $1 \le n \le 9$ levels of hydrogen and helium are treated as follows. The Milne relation for the emissivity $4\pi j$ (erg cm³ Hz⁻¹ s⁻¹) can be expressed

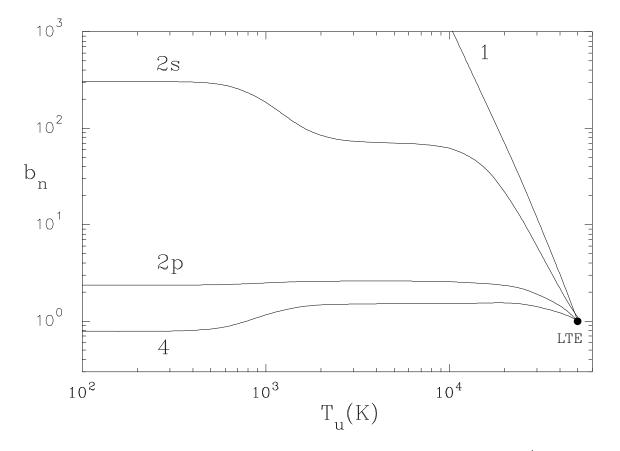


Figure 8: The calculations are for a constant temperature ($T_e = 5 \times 10^4$ K) optically thin gas exposed to black body radiation with a color temperature of $T_{color} = 5 \times 10^4$ K, but with various values of the energy density, parameterized as $T_u = (u/a)^{1/4}$, where uis the actual radiation density. The hydrogen density ($N = 10^{10}$ cm⁻³) is low enough for radiation to be the main agent affecting level populations for most values of T_u . Fluorescence from the ground state drives the population of n = 4 above its LTE value for many radiation densities. Induced processes, mainly transitions between adjacent levels, drive the atom to LTE when T_u reaches 5×10^4 K. hbnvsu

16.4 Thermal Emission

as (Brown and Mathews 1970)

$$4\pi j = h\nu \left(\frac{2\pi mk}{h^2}\right)^{-3/2} \frac{8\pi}{c^2} \frac{g_n}{g_e g_{ion}} T^{-3/2} \nu^2 \alpha_\nu(n) \exp\left(-h\left(\nu - \nu_o\right)/kT\right)$$
(106)

where the statistical weight of level n is $g_n = 2n^2$ for H^o and He⁺, and $g_n = n^2$ for helium singlets.

The code actually works with units similar to photons $\text{Ryd}^{-1} \text{ s}^{-1} \text{ cm}^{-2}$. The photon emissivity (photons $\text{cm}^3 \text{ s}^{-1} \text{ Ryd}^{-1}$) is then

$$\phi(T,n) = \left(\frac{2\pi mk}{h^2}\right)^{-3/2} \frac{8\pi}{c^2} \frac{g_n}{g_e g_{ion}} T^{-3/2} \nu^2 \alpha_\nu(n) \exp\left(-h\left(\nu - \nu_o\right)/kT\right) (107)$$

$$= 4.12373 \times 10^{11} \frac{g_n}{g_e g_{ion}} T^{-3/2} \nu_{Ryd}^2 \alpha_{\nu}(n) \exp\left(-h\left(\nu - \nu_o\right)/kT\right) \quad (108)$$

where the g's are the statistical weights of the constituents, ν_{Ryd} is the photon energy in Rydbergs, $h\nu_o \sim z^2/n^2$ is the ionization potential in Rydbergs, $\alpha_{\nu}(n)$ is the photoionization cross section, and the other symbols have their usual meanings. Equation 107 is evaluated directly using the stored photoionization cross sections. A similar approach is used for other absorption opacities, such as brems and H⁻. Detailed balancing between absorption and emission mechanisms is necessary if LTE is to be achieved.

Free-free emission is computed for all energies considered by the code, and free-bound emission for energies greater than ~0.009 Ryd (the ionization edge of the n=7 pseudo-state). This emission per unit volume (erg s⁻¹ cm⁻³) is stored in the array DIFFUS, and this diffuse continuum is carried outward in the array CONDIF.¹⁰

A test case with a hydrogen gas at a temperature of 10^4 K and a density of 10^7 cm⁻³ (to suppress two photon emission) was computed, and is shown in Figure 9. The input stream used to derive the figure is given as one of the examples in section 25. As can be seen from the figure, the predicted diffuse continuum is generally within 10 percent of the exact value (Ferland 1980). The main source of error is the treatment of highly excited states in the model hydrogen atom.

Figure 10 shows another series of test cases in which a very high density gas with cosmic abundances is irradiated with a 50,000K blackbody radiation field in strict thermodynamic equilibrium. The input stream used to derive the figure is as follows;

```
title test hydrogen atom emission in LTE limit
black 50,000 lte
constant temper 50,000
```

¹⁰The total transmitted/emitted continuum can be output by use of the "PUNCH CONTINUUM" command.

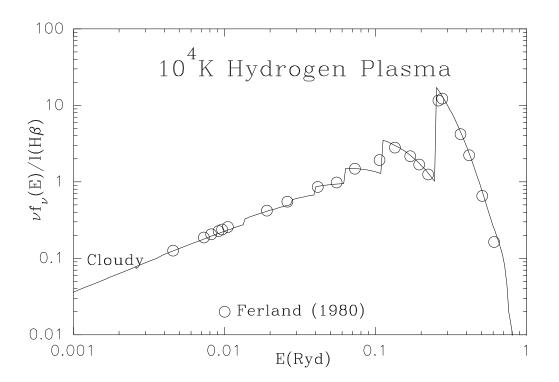


Figure 9: The predicted thermal emission from the 10-level hydrogen atom is shown as the computed flux divided by the intensity of H β . The gas is optically thin and contains only hydrogen. The circles indicate the filter-averaged continuum predicted by Ferland (1980). The input stream used to derive the figure is shown in section 25. hemis

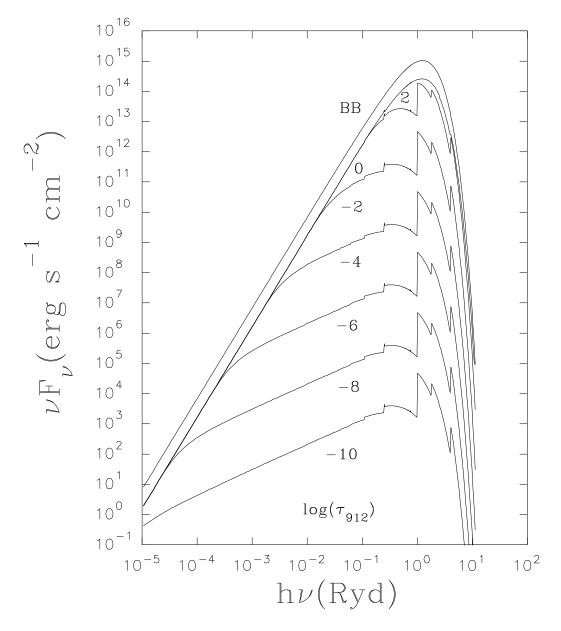


Figure 10: The emission from a dense slab of gas with cosmic abundances is shown as a function of the optical depth at the Lyman limit. The log of this optical depth is indicated on the figure. The top curve is for emission given by Planck's law. The continuous emission goes to the blackbody limit in the case of large continuum optical depths. conlte

hden 20 stop lyman optical depth -2 ;stop at Lyman contin tau print short punch reflected continuum ;output the reflected continuum

As can be seen from the figure, the predicted continuum goes to the blackbody limit.

17 H^- AND MOLECULES

An ion-molecule network, initially based on Black (1978) but heavily revised (Hollenbach and McKee 1979; 1989), is included in CLOUDY. The network presently includes H^- , H_2 , H_2^+ , H_3^+ , HeH^+ , OH, OH^+ , CH, CH^+ , O_2 , O_2^+ , CO, CO^+ , H_2O , H_2O^+ , H_3O^+ , and CH_2^+ .

17.1 The H⁻ Balance; Radiative Processes

Although only a trace amount of hydrogen is in the form of H^- , the opacity provided by this ion is large, and helps couple energy in the near infrared continuum to moderately ionized gas. The methods and approximations employed to include heating and cooling by H^- are described here. Other discussions can be found in Lambert and Pagel (1968), Vernazza, Avrett, and Loeser (1981), and Lites and Mihalas (1984).

The equilibrium density of H^- is determined by assuming statistical equilibrium, and balancing production and destruction mechanisms. Great care is taken in including both forward and back reactions, to ensure that the present treatment of $H^$ is capable to going to LTE in the limit of high radiation or particle densities.

In much of the following discussion comparison will be made between the predicted H^- population and its LTE value. The LTE relative population density of H^- is

$$P^*(H^-) = \frac{N_{H^-}^*}{N_e N_{H^o}} = \frac{g_{H^-}}{g_{H^o} g_e} \left(\frac{h^2}{2\pi m kT}\right)^{3/2} \exp(\chi_{H^-}/kT) \ (cm^3) \ , \tag{109}$$

where g_i is the statistical weight of the constituents, $(g_{H^-} = 1; g_{H^o} = 2; \text{ and } g_e = 2)$, $\chi_{H^-} = 0.055502$ Ryd is the binding energy of the negative hydrogen ion, and other constants have their usual meaning.

17.1.1 Radiative attachment

This is the most important creation mechanism for H^- at low densities, when three-body processes are negligible;

$$H^{\circ} + e^{-} \Rightarrow H^{-} + \gamma \quad . \tag{110}$$

For temperatures greater than 10^4 K the rate coefficient is evaluated by numerically integrating the photodetachment cross section over frequency;

$$\alpha_{rad}(T) = P^*(H^-) \int_{\nu_o}^{\infty} \alpha \nu \, \frac{8\pi\nu^2}{c^2} \, \exp(-h\nu/kT) \, d\nu \quad (cm^3 \, s^{-1}) \tag{111}$$

where cross sections computed by Wishart (1979) and spline interpolation are used. These cross sections are in excellent agreement with the velocity operator bound-free cross sections tabulated by Doughty et al. (1966). The energy interval between the photodetachment threshold at 0.055502 Ryd and ~ 1.8 Ryd is divided into roughly 100 cells with logarithmically increasing width, and the integration is carried out as a straightforward sum.

This method is not numerically expedient for very low temperatures, where the energy bandwidth of the integral is small, and a much finer frequency grid would be required. Rather, the integration was carried out using spline interpolation and 32 point gaussian quadrature, integrating over factors of two in $h\nu/kT$. The results were then fitted with a set of power-laws. The rate coefficients (cm⁻³ s⁻¹) can be approximated by:

$$\alpha(T_e) = \begin{cases} 8.934 \times 10^{-18} T_e^{0.505} & 1K \le T_e < 31.62K \\ 5.159 \times 10^{-18} T_e^{0.664} & 31.62K \le T_e < 90K \\ 2.042 \times 10^{-18} T_e^{0.870} & 90K \le T_e < 1200K \\ 8.861 \times 10^{-18} T_e^{0.663} & 1200K \le T_e < 3800K \\ 8.204 \times 10^{-17} T_e^{0.393} & 3800K \le T_e \le 10^4 K \end{cases}$$
(112)

These approximations fit the exact numerical results with a mean deviation of 0.7 percent, and the largest error of 2.05 percent, over the indicated temperature range.

Tests show that the numerical radiative attachment rates computed here are in very good agreement with the approximation given by Hutchings (1976), who used the cross sections computed by Doughty et al. (1966), for temperatures $500K \leq T \leq 2500K$. (Notice that there is a typographical error in the approximation for the radiative attachment rate given by Palla, Salpeter, and Stahler 1983.) It is also within 10% of the value given by Dalgarno and Kingston (1963), which was based on earlier calculations of the photodetachment cross section.

Continuum occupation numbers can be large in the infrared. The induced radiative attachment rate coefficient is

$$\alpha_{ind}(T) = P^*(H^-) \int_{\nu_o}^{\infty} \alpha_{\nu}(bf) \, \frac{4\pi J_{\nu}(\tau)}{h\nu} \, \exp(-h\nu/kT) \, d\nu \ (cm^3 \, s^{-1}) \tag{113}$$

where the mean intensity of the depth-dependent continuum is $J_{\nu}(\tau)$. This expression is used for all temperatures.

17.1.2 Photodetachment

Photodetachment,

$$H^- + \gamma \Rightarrow H^o + e^- \tag{114}$$

is the dominant H^- destruction mechanism for many conditions. The rate is evaluated in the standard manner;

$$\Gamma(H^{-}) = \int_{\nu_o}^{\infty} \alpha_{\nu}(bf) \frac{4\pi J_{\nu}(\tau)}{h\nu} d\nu \quad (s^{-1}) \quad .$$
(115)

The integral is evaluated as a sum over the numerically binned continuum. The incident continuum is then attenuated by optical depth increments

$$d\tau_{H^{-}} = \alpha_{\nu}(bf) N_{H^{-}} \{1 - \exp(-h\nu/kT)/b_{H^{-}}\} f dr$$
(116)

where b_{H^-} is the departure coefficient for H^- , $b_{H^-} \equiv N(H^-)/N^*(H^-)$, f is the filling factor, and $N^*(H^-)$ is the LTE H⁻ density.

17.1.3 Photodetachment by hard photons

The H⁻ photoabsorption cross section increases above ~ 3/4 Ryd, energies where excitation of $n \geq 2$ levels is possible. Cross sections which include this process are taken from Broad and Reinhardt (1976). These calculations do not extend to high energies, so we scale high-energy hydrogen cross sections by the ratio of H⁻ to H^o cross sections at 18Å in order to take absorption of x- and γ - rays into account.

The cross section for $(\gamma, 2e^-)$ absorption is much smaller than (γ, e^-) (Broad and Reinhardt 1976), and this latter process is neglected.

17.1.4 The approach to LTE; high radiation densities

As a test of the assumptions and methods, the approach to LTE under conditions determined by radiative attachment (spontaneous and induced) and photodetachment are first considered. Tests in which gas with temperature T_e is exposed to black body radiation fields with color temperature T_{color} are computed. The color and gas temperatures are set equal, $T_e = T_{color}$, and the intensity of the radiation field is varied up to the black body limit. The intensity of the radiation field is parameterized by the equivalent energy density temperature $T_u = (u/a)^{1/4}$, where u is the energy density (erg cm⁻³; see above) and a is the Stefan's radiation density constant. The equilibrium population of H⁻ was computed, including all process mentioned below, but with the hydrogen density small enough (typically $\sim 10^5 \text{ cm}^{-3}$) for radiative processes to be most important. The H^- population is expressed as a departure coefficient, and the results are shown in Figure 11, for tests in which $T_{color} = 0.5, 1, \text{ and } 2 \times 10^4 \text{ K}$. When $T_u = T_{color}$, and the radiation field is in strict thermodynamic equilibrium, radiative processes must hold H⁻ in LTE and departure coefficients of unity are expected. The computed departure coefficients for the three temperatures are 0.9998, 0.9996, and 1.0030, respectively. As the Figure shows, when T_u is lowered below T_{color} , the intensity of the radiation field falls below its thermodynamic equilibrium value, and the population of H^- increases. This is because the photodetachment rate (which is proportional to the intensity of the radiation field) is no longer in balance with the radiative attachment rate (which is proportional only to the electron density).

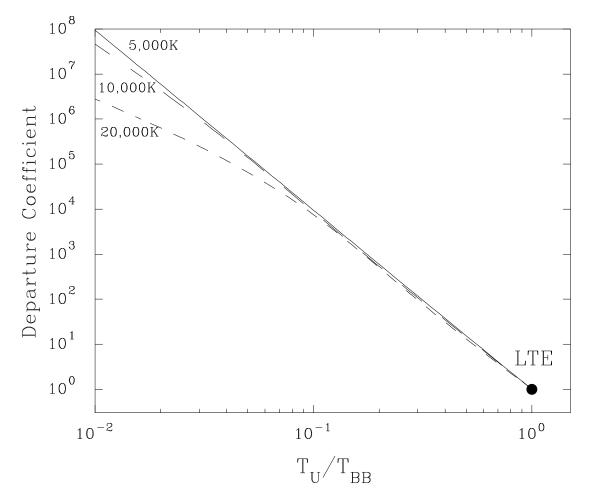


Figure 11: Departure coefficients for H⁻ are shown. The figure shows tests in which the hydrogen density was held fixed at a low density (typically $N_H \sim 10^5 \text{ cm}^{-3}$), and the gas irradiated by black bodies with color temperatures of 5, 10, and 20 ×10³K. Gas temperature and color temperatures were equal. The intensity, characterized by the energy density temperature T_u . was varied up to its LTE limit. The H⁻ departure coefficient is within 0.2% of unity when $T_u = T_{color}$. hmivsu

17.2 The H⁻ Balance; Collisional Processes

17.2.1 Associative detachment

The most important H_2 formation mechanism in grain-free environments, and a significant H^- destruction mechanism, is associative detachment,

$$H^- + H^o \rightleftharpoons H_2 + e^- \tag{117}$$

where rate coefficients from Bieniek and Dalgarno (1979) are used. The reverse reaction rate coefficient C_R , for electron collisional dissociation of H_2 , is related to the forward rate coefficient C_F by detailed balance;

$$C_R = C_F \frac{P^*(H^-)}{P^*(H_2)} \quad . \tag{118}$$

17.2.2 Electron collisional detachment

For typical BLR temperatures and ionization fractions, the process

$$H^- + e^- \rightleftharpoons H + 2e^- \tag{119}$$

is a competitive H^- destruction mechanism. Rates taken from the compendium of Janev et al. (1987) are used. The reverse process, electron three-body recombination with neutral hydrogen, is included via detailed balance;

$$C_R = C_F P^*(H^-) \quad . \tag{120}$$

17.2.3 Collisional ionization by suprathermal electrons

The total suprathermal collisional ionization rate is computed using approximations from Shull and Van Steenberg (1985). Ionization of H⁻ by suprathermal electrons is scaled from the H^o rates using cross sections at 20 eV given by Janev et al. (1987). This energy was chosen as representative of the mean energy of the secondary electron shower. The majority of these collisions are of the form $e^- + H^- \Rightarrow H(1s) + 2e^-$, although $e^- + H^- \Rightarrow H^+ + 3e^-$ collisions occur roughly 1% of the time.

17.2.4 Mutual neutralization

Neutral hydrogen can charge transfer with the negative ion through

$$H^- + H^+ \rightleftharpoons H + H^* \quad . \tag{121}$$

The rate coefficients given in Janev et al. (1987) are used. By far the largest rate coefficients are for collisions which populate hydrogen in the n = 3 level. These rates

are based on both experimental and theoretical data (see, for example, Peart et al. 1985).

The reverse reaction is included using detailed balance; if the rate coefficient for the forward reaction is C_F then the reverse reaction rate, and its rate coefficient C_R , are given by

$$H(1s) N(i) C_R = b_i P^*(H^-) N_e N_p C_F$$
(122)

where N(i) and b_i are the population and departure coefficient of hydrogen in the i^{th} level.

17.2.5 Charge neutralization with heavy elements

The process

$$H^- + A^+ \rightleftharpoons H^o + A^o \tag{123}$$

is considered by Dalgarno and McCray (1973), who give rate coefficients for very low temperatures and ionization levels. Judging from the curves given by Peterson et al. (1971), upon which the Dalgarno and McCray rates are based, the approximation they give should still be valid (although very uncertain) at temperatures of general interest ($\sim 0.5 - 1.0 \times 10^4$ K). Here A⁺ is all singly ionized species, which are assumed to be neutralized at the same rate.

17.2.6 Neglected processes

Collisional detachment by protons $(p^+ + H^- \Rightarrow H + p^+ + e^-)$, which has a negligible rate coefficient according to Janev et al. (1987), is neglected, as is collisional detachment by atomic hydrogen $(H^- + H \Rightarrow 2H + e^-)$, which has no reliable rate coefficient according to Lites and Mihalas (1984).

17.2.7 The approach to LTE; high hydrogen densities

A series of models in collisional equilibrium were computed. Radiative processes were also included, but the incident radiation field, a 10^4 K blackbody, was given a negligible intensity (an ionization parameter of $U = 10^{-12}$). Three temperatures, 0.5, 1, and 2×10^4 K, were considered to span the temperature range typical of regions with significant H⁻ population. The hydrogen density was varied between 10^8 and 10^{18} cm⁻³ to confirm the approach to LTE at high densities. The results of these calculations are shown in Figure 12. For the majority of the calculations hydrogen is largely neutral, and for the smaller temperatures a significant fraction of the hydrogen was in the molecular form (H₂ and H₂⁺). The calculation confirms that the departure coefficients are within 2% of unity at the highest densities computed.

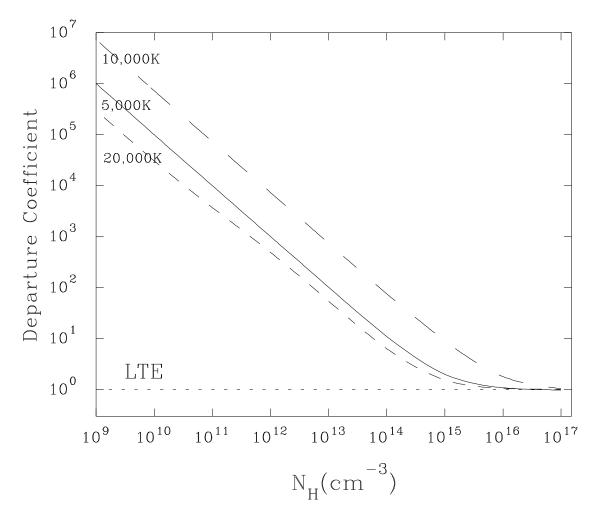


Figure 12: Departure coefficients for H^- are shown. These are tests in which the radiation density was low, but the total hydrogen density varied. Three gas temperatures, spanning typical temperatures where H^- is significant, are shown. Collisions bring $H^$ to LTE at high densities. hmivsn

Hydrogen Molecules 17.3

A complete ion-molecule network, initially based on Black (1978) but since heavily revised (see, for example, Hollenbach and McKee 1989; Lenzuni, Chernoff, and Salpeter 1991), is included in CLOUDY. The network includes H^- , H_2 , H_2^+ , and HeH^+ , and its solution is performed in subroutine HMOLE. The set of balance equations for the first three species are solved simultaneously, using the matrix:

$$\begin{pmatrix} H \ conservation \\ H^{-} \ balance \\ H_{2} \ balance \\ H_{2}^{+} \ balance \\ H_{3}^{+} \ balance \end{pmatrix} \begin{pmatrix} N(H^{\circ}) \\ N(H_{2}) \\ N(H_{2}^{+}) \\ N(H_{3}^{+}) \end{pmatrix} = \begin{pmatrix} N(H^{\circ}) \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$
(124)

17.4The heavy elements

The heavy element molecule network described by Hollenbach and McKee (1989) has been incorporated into CLOUDY. The network should now be exact for situations where the heavy element molecular fraction is small. The heavy element molecules are not now included in the atomic abundances, so the treatment is approximate for predominantly molecular situations.

$$\begin{pmatrix} C \ conservation \\ O \ conservation \\ CH \ balance \\ CH^+ \ balance \\ OH \ balance \\ OH \ balance \\ OH^+ \ balance \\ CH_2^+ \ balance \\ CO \ balance \\ H_2O \ balance \\ H_2O^+ \ balance \\ H_2O^+ \ balance \\ H_3O^+ \ balance \\ O_2 \ balance \\ O_2 \ balance \\ O_2^+ \ balance \\$$

18 HELIUM

The helium atom is presently under construction. The following outlines the treatments of the various ions.

18.1 The Helium Ion

He⁺ is treated as a ten level atom, entirely analogous to the hydrogen atom. Full l-mixing is assumed, and 2s and 2p are treated independently.

18.2 The Helium Singlets

The He singlets are treated as a ten level atom, entirely analogous to the hydrogen atom. Full l-mixing is assumed, and 2s and 2p are treated independently.

18.3 The Helium Triplets

The helium triplets are presently treated as a five level atom.

18.4 Ionization Equilibria

The ionization equilibria of the various ions/atoms is accurate for all photon and electron densities. The balance goes to LTE in the high photon-electron density limit.

18.5 Line Emission

Line intensities predicted by the 10-level atoms are indicated by the label "TOTL". These include all optical depth and collisional effects. The model atoms describing the ion and singlets assume complete l-mixing among the sublevels. The predictions are exact in the context of this approximation, but this approximation is not valid at low densities. The greatest problem is HeII 4686, for which the complete l-mixing assumption results in an intensity much smaller than the low density limit approximation.

For now the line emissivities predicted by the atoms are probably not as accurate as simple case B assumptions for low density conditions where optical depth and collision effects are not important. Case B predictions are labeled "Ca b". At high densities $(N_e \ge 10^6 \text{ cm}^{-3})$ the predictions of the 10-level atom are probably better than case B predictions.

19 THE HEAVY ELEMENTS

The treatment of the ionization equilibrium of the other 11 elements is fairly conventional (see, for instance, Halpern and Grinday 1980; Kallman and McCray 1982). The treatment of the metals is presently more approximate than that of hydrogen and helium when high densities $(N_H > 10^{10} \text{ cm}^{-3})$ are considered. The majority of the heavy elements are treated considering only the ground term and continuum for each ionization stage. In all cases, collisional ionization from ground (using data from Shull and van Steenberg 1982) and a net three-body recombination coefficient (see, for example, Burgess and Summers 1976) are included. Photoionization rates are modified for induced recombination as described by equation 102. All published charge transfer rate coefficients are also included (e.g., Butler, Heil, and Dalgarno 1980; Butler and Dalgarno 1980).

This treatment is approximate at high densities for two reasons. First, net radiative recombination coefficients, which have been summed over all levels (Aldrovandi and Pequignot 1972; Aldrovandi and Pequignot 1974; Gould 1978), are used. These sums are correct only in the low density limit; at high densities levels can undergo collisional ionization before radiative decays to the ground state occur. A second problem is that substantial populations can build up in highly excited states when the density and temperature are high. When this occurs the partition function of the atom or ion is no longer equal to the statistical weight of the ground state. As a result the ionization equilibrium of the heavy elements is approximate at high densities (N $\gg 10^{10}$ cm⁻³), with uncertainties probably at the ~ 0.5 dex level.

19.1 Ionization Potentials

Figure 13 shows the ionization potentials of the heavy elements included in the calculations. The upper panel shows energy range of interest for photoionization by stars. The dotted lines show the ionization potentials of hydrogen, atomic, and ionic, helium. The lower panel shows the energy range of interest for photoionization by X-ray continua.

19.2 Low Temperature Dielectronic Recombination

Dielectronic recombination through low-lying autoionizing states is known for be the dominant recombination mechanism for many ions of second-row elements (i.e., Nussbaumer and Storey 1983). Unfortunately, these have not been computed for most third-row elements or iron. This constitutes a major uncertainty in understanding the ionization balance of these elements. For those elements where a dielectronic

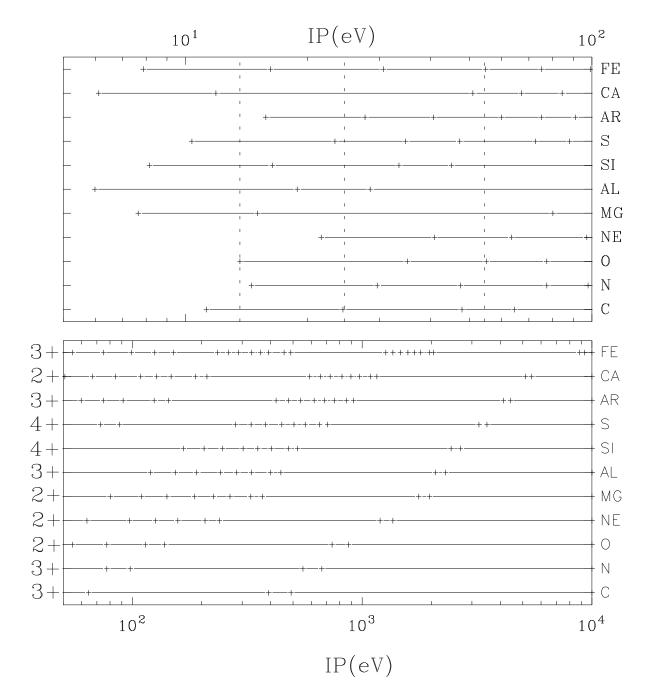


Figure 13: The ionization potentials of the heavy elements considered by the code are shown. The ionization potentials of hydrogen and helium are indicated by the dotted lines. The upper panel shows the energy range of interest for conventional nebulae, and the lower panel shows the energy range of interest for relatively hard continua. ionpot

recombination rate coefficient has not been computed, the mean of the rate coefficient for C, N, O, and Ne is used instead.

19.3 Carbon

Low temperature dielectronic recombination rate coefficients are taken from Nussbaumer and Storey (1983).

19.4 Nitrogen

Low temperature dielectronic recombination rate coefficients are taken from Nussbaumer and Storey (1983).

19.5 Oxygen

Low temperature dielectronic recombination rate coefficients are taken from Nussbaumer and Storey (1983).

19.5.1 The O I Model atom

A partial Grotrian diagram for the O I atom considered in the Ly β -O I fluorescence problem is shown in Figure 14. Rates for fluorescence between the two transitions are computed as in Netzer et al. (1985).

19.6 Neon

Low temperature dielectronic recombination rate coefficients are taken from Nussbaumer and Storey (1987).

19.7 Magnesium

Low temperature dielectronic recombination rate coefficients for recombination to the atom are taken from Nussbaumer and Storey (1986). Rate coefficients have not been computed for recombination to the ions.

19.8 Aluminum

Low temperature dielectronic recombination rate coefficients for recombination to the atom and first ion are taken from Nussbaumer and Storey (1986). Rate coefficients have not been computed for recombination to other ions.

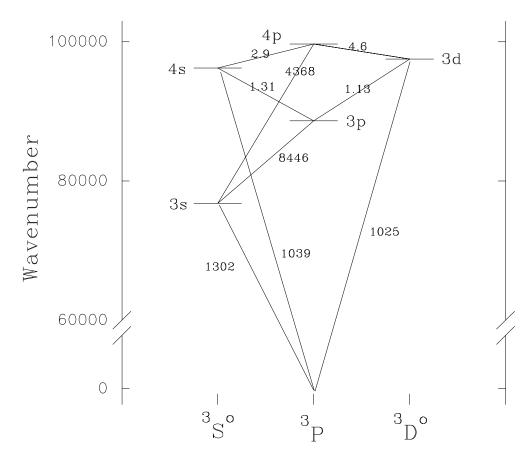


Figure 14: The levels of O^ included in the calculation of the OI– Ly β pumping problem are shown. oigrot

19.9 Silicon

Low temperature dielectronic recombination rate coefficients for recombination to the atom and first two ions are taken from Nussbaumer and Storey (1986). Rate coefficients have not been computed for recombination to other ions.

19.10 Sulphur

Low temperature dielectronic recombination rate coefficients have not been computed for this element.

19.11 Argon

Low temperature dielectronic recombination rate coefficients have not been computed for this element.

19.12 Calcium

Low temperature dielectronic recombination rate coefficients have not been computed for this element.

19.12.1 The Ca II Model atom

The Ca II ion is treated as a five-level atom plus continuum. The model atom is shown in Figure 15, and is similar to that described by Shine and Linsky (1974). Collision strengths for j-mixing collisions are from Saraph (1970). Collision and radiative data for the 4s - 4p transition are taken from the compendium of Mendoza (1983), and all other collision data are from Chidichimo (1981) and Saraph (1970). Radiative data for the 3d - 4p and 4s - 3d transitions are from Black, Weisheit, and Laviana (1972); these are in good agreement with the calculations of Osterbrock (1951). The compendium by Shine and Linsky (1974) provides photoionization cross sections for excited levels, which are adopted here. Recombination contributions to the population of individual levels are included by dividing the excited state recombination coefficient among the excited levels considered, according to their statistical weight and the rules of LS coupling.

All Ca II transitions (including the forbidden lines) can become quite optically thick. Radiative transfer is treated with the escape probability formalism, assuming incomplete redistribution, including destruction by background opacities.

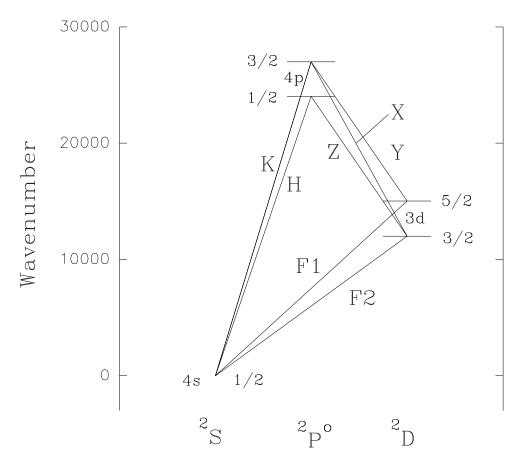


Figure 15: The five levels of Ca⁺ included in the calculations are shown. The wavelengths of the predicted lines are K (3934), H (3969), X (8498), Y (8542), Z (8662), F1 (7291), and F2 (7324). ca2grot

19.13 Iron

Low temperature dielectronic recombination rate coefficients have not been computed for this element.

19.13.1 Fe $\mathbf{K}\alpha$ Emission

The intensity of the Fe K α line is predicted including both recombination and fluorescence. Figure 16 show the assumed fluorescence yield and K α energy. The line predictions are separated into "cold" iron (iron with M-shell electrons present) and "hot" iron (those ionization states producing lines with energies greater than ~6.4 keV). This includes the recombination and collisional contribution. The "TOTL" Ky α is the sum of the two.

19.14 Heavy Element Opacities

Figure 17 shows a calculation of the opacity of a solar gas with very low ionization.

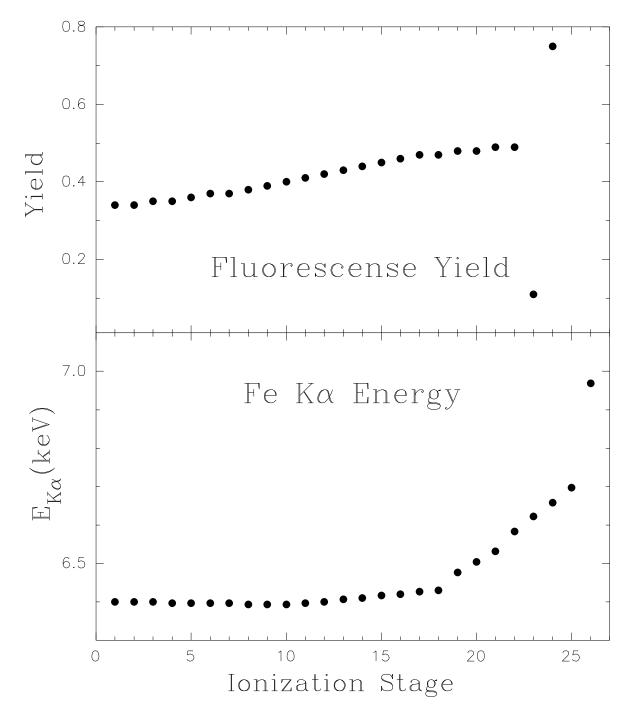


Figure 16: The fluorescence yield and energy of the emitted Fe K α photon are shown as a function of ionization stage. feka

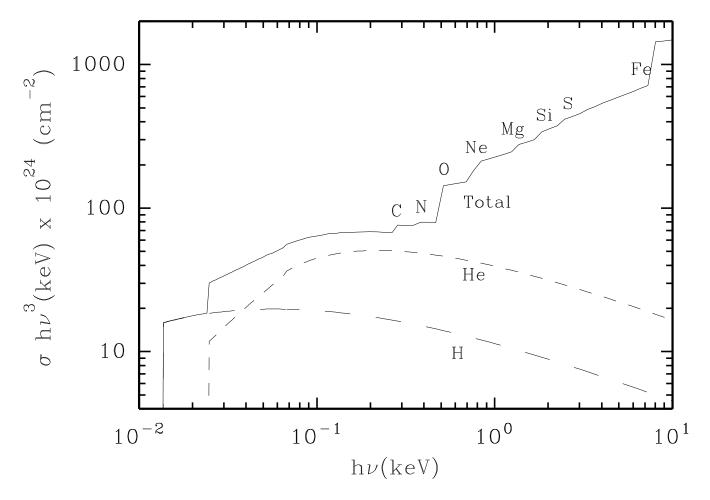


Figure 17: The opacity of a neutral gas with solar abundances is shown as a function of energy. The curve is scaled to allow direct comparison with conventional calculations of opacity at X-ray energies (i.e., Morrison and McGammon 1983). hevopc

20 THERMAL EQUILIBRIUM

20.1 Introduction

Strict thermodynamic equilibrium (TE) is reached when all heating and cooling processes are in detailed balance. The approach to this equilibrium as T_u and N increase is discussed here.

Heating or cooling can be defined relative to either the ground state or continuum, and this difference has caused some confusion in the literature. CLOUDY defines heating and cooling relative to the continuum, as in Osterbrock (1988). Note that, in this scheme of bookkeeping, photoionization contributes an amount of heat given by $h(\nu - \nu_o)$, where $h\nu_o$ is the ionization potential of the atom or ion, and emission of a recombination line *does not* constitute a cooling process. Heating and cooling rates are computed in cgs units (ergs, not Rydbergs) throughout CLOUDY.

20.2 Thermal Stability

The criterion for thermal stability used by CLOUDY is that the net cooling (i.e., cooling minus heating) have a positive temperature derivative (Field 1965). This can be expressed as

$$\frac{d\left(\Lambda - G\right)}{dT} > 0. \tag{126}$$

The code will print a "u" next to the temperature in the zone results, and make a comment in the end, if possibly thermally unstable solutions were found.

The criterion used by the code is that the derivative *at constant density* (isochoric) be positive. The more traditional criterion is that the derivative *at constant pressure* (isobaric) be positive (Field 1965).

20.3 Compton Energy Exchange

The net volume heating rate (erg s⁻¹ cm⁻³) due to Compton energy exchange is given by

$$G_{Comp} - \Lambda_{Comp} = \frac{4\pi N_e}{mc^2} \left\{ \int \sigma_h J_\nu h\nu \left[1 + \eta_\nu \right] d\nu - 4kT \int \sigma_c J_\nu d\nu \right\}$$
(127)

(see, for instance, Levich and Sunyaev 1970; and Krolik, McKee, and Tarter 1981). The two terms in braces are the heating and cooling terms respectively, while the factor in brackets in the first term accounts for heating due to both spontaneous and stimulated Compton scattering. Induced Compton heating is important when η_{ν} is large at frequencies where $h\nu \geq kT$; in fact it is, at most, a few percent effect in most circumstances.

The terms σ_h and σ_c appearing in equation 127 are the effective energy exchange (scattering) cross section for energy exchange, and differ from the Thomson cross section for energies $h\nu \sim m_e c^2$, where the Klein-Nishina cross section must be used. The numerical fits to Winslow's (1975) results, as used by Krolik, McKee, and Tarter (1981) and kindly provided by Dr. C.B. Tarter, were used. Defining

$$\alpha = \left\{ 1 + \nu_R \left(1.1792 \times 10^{-4} + 7.084 \times 10^{-10} \nu_R \right) \right\}^{-1}$$
(128)

and

$$\beta = \left\{ 1 - \alpha \nu_R (1.1792 \times 10^{-4} + 2 \times 7.084 \times 10^{-10} \nu_R) / 4 \right\} \quad , \tag{129}$$

where ν_R is the photon frequency in Rydbergs, the Compton energy-exchange rate coefficients are then $\sigma_h = \sigma_T \alpha$ and $\sigma_c = \sigma_T \alpha \beta$. Tests show that these are in excellent (much better than 1 %) agreement with Guilbert's (1986) calculations for $h\nu < 10$ MeV, the energies where Guilbert's calculations are valid.

The total Compton heating-cooling rates are evaluated zone by zone in subroutine HIGHEN. The coefficients for the heating and cooling terms, i.e., α and the product $\alpha\beta$, are calculated in subroutine PNTSET at the beginning of the calculation and stored in the vectors $\text{CSIGH}(\nu)$ and $\text{CSIGC}(\nu)$. The heating is determined by summing over the continuum;

$$G_{Comp} = \frac{N_e}{mc^2} \sigma_T \left(h\nu_{Ryd}\right)^2 \sum \alpha_i \phi_i \nu_i^2 \left(1 + \eta_i\right)$$
(130)

where ϕ_i is the photon flux, stored in the vector variable FLUX, η_i is the photon occupation number, σ_T is the Thomson cross section, and ν_i is the photon energy in Rydbergs, stored in the vector variable ANU. The heating and cooling rates are stored as the variables CMHEAT and CMCOOL.

Tests in which Compton energy exchange was the dominant physical process affecting the temperature were made, and the results are shown in Figure 18. A series of models in which the gas was irradiated by black body continua in strict thermodynamic equilibrium (i.e., $T_u = T_{color}$) and various hydrogen densities, were computed. Over the temperature range 3 K $\leq T_{color} \leq 10^{10} K$ the computed equilibrium electron temperature equaled the color temperature within much better than 1% ($\langle T_e - T_{color} \rangle / T_{color} = -0.00073 \pm 0.0019$).

The input stream for the two limiting cases (temperatures of 10^{10} K and 3K respectively) follow;

```
title Compton limit; high temperature limitblackbody 9.5 lte% lte sets blackbody in strict T.E.hden 10% low enough for Compton to dominatestop zone 1
```

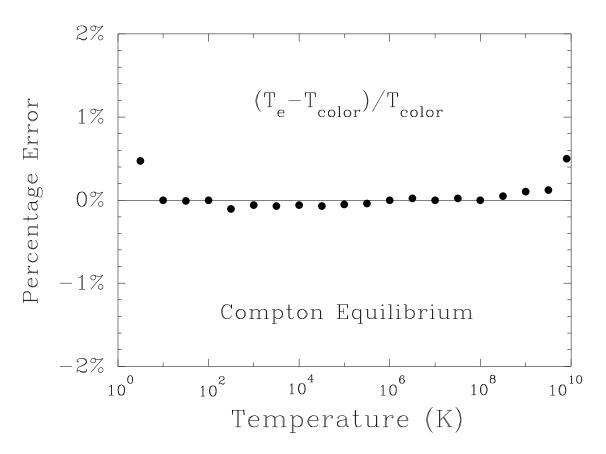


Figure 18: Thermal equilibria in the Compton Limit. These calculations are for blackbody continua of various temperatures, given as T_{color} along the x-axis. The energy density temperature T_u is set equal to T_{color} so that strict thermodynamic equilibrium is expected. The hydrogen density is adjusted to maintain ionization parameters $U \sim 10^{10}$, so that the thermal equilibrium equations are dominated by the Compton exchange problem. The deviation of the computed equilibrium temperature T_e from the asymptotic Compton temperature T_{color} is shown. The code gives reliable results (errors $\ll 1\%$) within its intended temperature bounds of 10 K and 10^9 K. compton

```
print short
tolerance 0.0001
                             % set fine tolerance to check temp exactly
title Compton limit; low temperature limit
black linear 3 lte
                             % set to 3K
lowest temperature linear 2K % allow equil temp below 10K
                             % must have some ionizing radiation
brems 5
ionization parameter -5
                             % but not too much
hden -10
                             % set HDEN but does not matter
eden -2
                             % add some free electrons
stop zone 1
print short
tolerance 0.0001
```

For a blackbody radiation field with $T_u \neq T_{color}$ the Compton temperature will not be exactly equal to T_{color} because induced scattering will not contribute the required amount of heating-cooling. Note also that when $T_u > T_{color}$ induced Compton heating drives T_e above T_{color} . The intended temperature range of validity for CLOUDY is 10 – 10^9 K. Over this more limited range the computed Compton temperature, for conditions in which strict TE is expected, is generally equal to the color temperature within three significant figures (see figure 18). At temperatures $\gg 10^9$ K the electrons become relativistic; CLOUDY was not intended for these conditions. For temperatures $T \ll 10$ K the computed temperature fails high because the energy bandwidth of the continuum array does not extend below 1.001×10^{-5} Ryd. As a further test, the models presented by Krolik, McKee, and Tarter (1981) were recomputed with excellent agreement (typically within 3%) with their computed Compton temperatures.

20.4 Free-free Heating-Cooling

The volume free-free heating rate is given by

$$G_{ff} = 4\pi \int_{\nu_l}^{\infty} N_e \ \alpha_\nu(ff) J_\nu \ d\nu \tag{131}$$

where the free-free cross section $\alpha_{\nu}(ff)$ is given by equation 54 and ν_l is the low energy limit of the code (1.001 × 10⁻⁵ Ryd). The continuum J_{ν} is the sum of the attenuated incident radiation field and the OTS line fields. Diffuse reemission, mainly free-free emission, *is not* included in this integral, as discussed below. The heating rate is evaluated in routine FREEHT.

The cooling by free-free emission, and the subsequent absorption of this radiation, must also be treated. These diffuse continua are treated by defining a critical

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frequency ν_c as follows. Gas at a depth R into the cloud is transparent to photons with energies above a critical frequency ν_c such that

$$\tau_c = \int \kappa(\nu_c) \, dr = \int_0^R \, \alpha_\nu(ff, \, \nu_c) \, N_e \, dr = 1 \tag{132}$$

and optically thick at lower frequencies. The critical frequency ν_c is evaluated in routine TAUFF; the energy in Rydbergs is stored as TFF, while the variable NTFF points to the cell in the continuum array.

The free-free cooling rate is then given by

$$\Lambda_{ff}(\tau) = \int_{\nu_c}^{\infty} N_e \alpha_{\nu}(ff) \ 4\pi B_{\nu}(T_e) \ d\nu = \Lambda_{ff}(0) \times \exp(-h\nu_c/kT)$$
(133)

where $\Lambda_{ff}(0)$ is the optically thin cooling rate and $B_{\nu}(T_e)$ is Planck's function. This is equivalent to assuming that, for $\nu < \nu_c$, where the cloud is optically thick, free-free heating and cooling exactly balance, as suggested by Kirchhoff's law and detailed balance considerations. The rate is evaluated in routine COOLR and is stored as the variable HBREMS.

20.5 Photoelectric Heating, Recombination Cooling

The net heating rate due to photoelectric heating less spontaneous and induced recombination cooling of level n is given by

$$G_{\kappa} = G_{n,\kappa} - \Lambda_{ind,n} - \Lambda_{spon,n} \tag{134}$$

where the volume heating rate due to photoionization is

$$G_{n,\kappa} = N_n \int_{\nu_o}^{\infty} \frac{4\pi J_{\nu}}{h\nu} \alpha_{\nu} h \left(\nu - \nu_o\right) d\nu \quad , \tag{135}$$

the volume cooling rate due to induced recombination is

$$\Lambda_{ind,n} = N_e \ N_p \ 4\pi \ P_n^* \int_{\nu_o}^{\infty} \frac{J_{\nu}}{h\nu} \alpha_{\nu} \ \exp(-h\nu/kT) \ h(\nu - \nu_o) \ d\nu \quad , \tag{136}$$

and the cooling rate due to spontaneous radiative recombination is

$$\Lambda_{spon,n} = N_e \ N_p kT\beta(T,n) \quad . \tag{137}$$

The cooling rate coefficient $\beta(T, n)$ is evaluated as described above (see also Hummer and Seaton 1963).

20.6 Collisional Ionization - Three-Body Recombination

The net volume heating rate due to collisional ionization less three-body recombination is approximately given by

$$G_{n\kappa} - \Lambda_{n\kappa} = \sum_{n} P_n^* N_e N_p C_{n\kappa} h\nu_o (1 - b_n)$$
(138)

where $C_{u\kappa}$ is the collisional ionization rate. This equation is approximate since the energy of the freed electron is ignored relative to the ionization potential χ_n of the level. This approximation is reasonable since the term $(1 - b_n)$ is only large for very low levels, in which $\chi_n > kT$. Far from thermodynamic equilibrium this is usually a net cooling process since departure coefficients for excited states are ~ 1 while the ground and n = 2 states often have $b_n \gg 1$.

20.7 Line Cooling

The net heating due to line collisional deexcitation less excitation is given by

$$G_{line} - \Lambda_{line} = \sum_{n=1}^{9} \sum_{u=n+1}^{10} P_n^* N_e N_p C_{un} h \nu_{un} (b_u - b_n)$$
(139)

where C_{un} is the downward collision rate. Far from thermodynamic equilibrium collisions involving the ground state tend to cool the gas (since $b_1 \gg 1$) and those between levels with $n \geq 3$ tend to heat the gas (since b_n tends to increase with n).

20.8 H⁻ Heating and Cooling

The calculation of the heating and cooling rates due to H⁻ are described here.

20.8.1 H⁻ bound-free

The volume heating rate due to spontaneous absorption (photodissociation) is

$$G_{H^{-}} = N(H^{-}) \int_{\nu_o}^{\infty} \frac{4\pi J_{\nu}}{h\nu} \alpha_{\nu} h(\nu - \nu_o) d\nu \quad (ergs \ s^{-1} \ cm^{-3})$$
(140)

where symbols have their usual meaning. The volume cooling rate due to induced radiative attachment is

$$\Lambda_{ind,H^{-}} = N_e N_{H^o} P^*(H^{-}) \int_{\nu_o}^{\infty} \alpha_{\nu} \, \frac{4\pi J_{\nu}}{h\nu} \exp(-h\nu/kT) \, h(\nu - \nu_o) \, d\nu \quad (ergs \ s^{-1} \ cm^{-3}) \,,$$
(141)

while the volume cooling rate for spontaneous radiative attachment is

$$\Lambda_{spon,H^{-}} = N_e N_{H^o} 8\pi \ P^*(H^{-}) \int_{\nu_o}^{\infty} \alpha_{\nu} \ \frac{\nu^2}{c^2} \ \exp(-h\nu/kT) \ h(\nu - \nu_o) \ d\nu \quad .$$
(142)

20.8.2 H⁻ free-free

Free-free heating and cooling by H^- is also significant, although less so than bound-free heating. This is included, making the appropriate correction for stimulated emission, using the cross sections given by Vernazza et al. (1981; see also Bates et al. 1975).

Under most circumstances H^- bound-free heating and cooling is much more important than H^- free-free processes. This is surprising at first sight, since standard opacity curves comparing bound-free and free-free opacities (Bates et al.1975; Mihalas 1978) show that the two are comparable. These curves are for strict thermodynamic equilibrium, with H^- departure coefficients of unity. Like the ground state of hydrogen, the departure coefficient for H^- is often many orders of magnitude larger than unity, so that the H^- bound-free opacity and the resulting heating greatly exceeds the H^- free-free opacity.

20.9 Equilibrium Calculations

Figure 19 shows the results of a series of calculations in which the full set of statistical and thermal equilibrium equations are solved for thin cells of hydrogen gas with various densities. The ionizing continuum is, in all cases, a black body with $T_{color} = 5 \times 10^4 K$, and the energy density of the radiation field is varied, up to the thermodynamic equilibrium limit, $T_u = T_{color}$.

Although the gas temperature in the thermodynamic equilibrium limit does not depend on the gas density, the physical processes which drive the gas to this temperature do. Thermal equilibria calculations were performed with three densities chosen to span a fairly wide range. For low densities $(N_H = 10^5 \text{ cm}^{-3})$ the gas remains highly ionized for all values of T_u shown and the temperature in thermodynamic equilibrium is set by the balance between Compton and inverse-Compton scattering. The intermediate density case $(N_H = 10^{10} \text{ cm}^{-3})$ reaches thermodynamic equilibrium with $\sim 3/4$ of the heating-cooling set by Compton scattering and the remainder due to free-free and free-bound processes. The high density $(N_H = 10^{15} \text{ cm}^{-3})$ case reaches its thermodynamic equilibrium temperature with a balance between free-free (1/3 of the total) and free-bound (2/3 of the total) processes. In all cases the level populations and electron temperature are within $\sim 1\%$ of their expected thermodynamic equilibrium values when $T_u = T_{color}$.

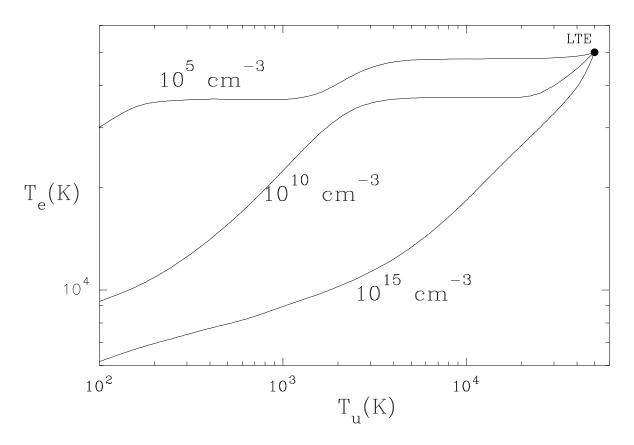


Figure 19: Thermal equilibrium calculations for an optically thin gas with various hydrogen densities are shown as a function of the energy density in the radiation field, parameterized as T_u . Ionization is by a $5 \times 10^4 K$ black body. A combination of Compton scattering, free-free, and free-bound transitions drive the gas to thermodynamic equilibrium when T_u reaches $5 \times 10^4 K$. hlte

21 GRAIN PHYSICS

The following discussion outlines some physical processes relating to grains. It is adopted from Baldwin et al. (1991), and was written in collaboration with P.G. Martin.

Several grain populations, types of graphite and "astronomical silicates", are available. Usually one of each type, for a total of two, are selected. Optical properties like opacity of the species are based on a realistic power-law size distribution. Other properties (like potential and temperature) are computed for a mean grain size rather than calculated for each individual size.

21.1 Grain Opacity

Grains are not normally included in the calculation. When enabled with the "grain" command, the default mixture has interstellar medium (ISM) properties. Grains more similar to those seen in Orion or planetary nebulae are also available.

21.1.1 ISM grains

The optical constants for the default (ISM) grain species are from the calculations of Martin and Rouleau (1990), which extend the work of Draine and Lee (1984) to ionizing energies where the grains are strongly absorbing. These opacity calculations were based on the Mathis, Rumpl, and Nordsieck (1977) power law size distribution to simulate interstellar extinction in diffuse clouds.

21.1.2 Orion grains

Grains within the Orion Nebula have a relatively large ratio of total to selective extinction and an exceptionally grey opacity in the ultraviolet, both indicative of a deficiency in small grains and a larger mean grain size. To account for this, a second set of opacity functions are included, the Orion group. For this the value of the smallest size (a_{-}) in the Mathis et al. (1977) size distribution was increased from 0.0025μ m to 0.03μ m. While this simple adjustment of the size distribution is not entirely adequate for explaining the details of the visible and near ultraviolet Orion extinction curve (Mathis and Wallenhorst 1981), it should be an improvement for the ionizing ultraviolet portion, which is most important.

The Orion extinction curve is designed to simulate the large R grains observed in this HII region. Relative to ISM standard grains the total amount of grain material was preserved, so that σ_a in the infrared and in the EUV and x-ray regions remains unchanged. The main differential effect is to lower the cross section through a broad peak at 1 Ryd.

21.1.3 PN grains

Infrared opacities for the silicate component are taken from unpublished work by K. Volk. Ultraviolet silicate cross sections, and the graphite constituent, are standard ISM.

21.1.4 Extinction

The ISM extinction properties, both effective scattering (subscript s) and absorption (subscript a), are shown in Figure 20. The quantities plotted are cross sections (cm²) per H nucleon: $\sigma = \kappa/N_{\rm H}$, where κ (cm⁻¹) is the opacity due to grains and $N_{\rm H}$ (cm⁻³) is the local density of H in any form. Rather than the total scattering cross section σ_s an effective scattering cross section $\sigma_{eff} = \sigma_s(1-g)$ is plotted; this discounts the radiation scattered near the forward direction; the asymmetry parameter g approaches unity at high and low energies, particularly for larger grains, so that σ_{eff} becomes much less than σ_a .

The optical depth τ is σ times the hydrogen column density (or κ integrated over the path). Absorption attenuates the incident radiation field as $\exp(-\tau_{abs})$. The effects of scattering are more difficult to model. In an open geometry, scattering attenuates approximately as $(1+0.5 d\tau_{s_e})^{-1}$. However, in a closed geometry, to within factors of order unity, the scattered light is not lost from the beam, and the scattering opacity can be ignored. In either case, τ_{eff} is generally fairly small through the ionized nebula at ionizing energies.

21.2 Photoelectric Emission

As discussed below, photoelectric emission from grains contributes directly to heating the gas and, through the grain potential U_g established, affects radiative and collisional heating of the grains and the grain drift velocity.

The photoionization rate of a grain, per unit projected area, is

$$\Gamma_g = \int_{\nu_o}^{\infty} Q_{abs} \frac{4\pi J}{h\nu} \hat{Y} d\nu, \qquad (143)$$

where \hat{Y} is the effective photoelectric yield per absorbed photon, Q_{abs} is the absorption efficiency factor, and $4\pi J/h\nu$ symbolizes the photon flux of direct, diffuse, and OTS radiation fields. For the OTS line component, the integral is of course just a sum over the line photons that are sufficiently energetic. The threshold for photoemission, to be determined self-consistently, is given by $h\nu_o = \max\{V_n + V_g, V_n\}$, where V_n is the photoelectric threshold for a neutral grain and $V_g = eU_g$.

 V_g will depend on grain size through Q_{abs} and \hat{Y} . In the present implementation, a typical V_g is defined for each species by using Q_{abs} averaged over the size distribution:

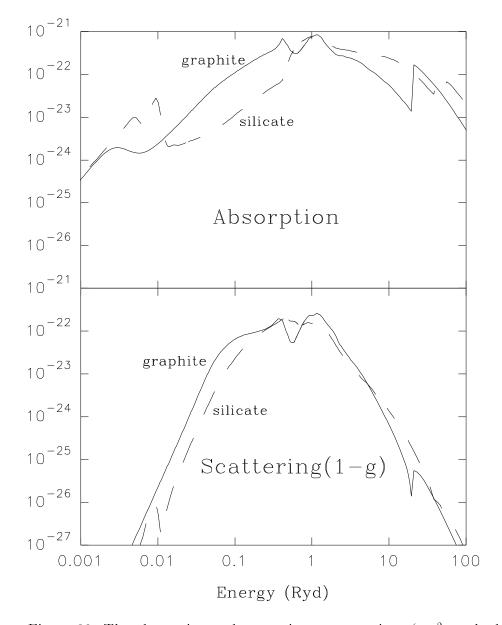


Figure 20: The absorption and scattering cross sections (cm² per hydrogen nucleon) for the two ISM grain populations, graphite and silicate, are shown. The effective scattering cross section is the scattering cross section multiplied by 1-g, where g is the asymmetry parameter. grainop

 $Q_{abs} = \sigma_a / \Sigma = \kappa_a / N_{\rm H} \Sigma$. The projected grain area per H, Σ , is similar for each species: $2.1 \times 10^{-22} \text{ cm}^2$ for graphite and $2.4 \times 10^{-22} \text{ cm}^2$ for silicates.

 \hat{Y} is constructed as follows. The basic laboratory data measure the yield (per absorbed photon) for a neutral surface, Y_n . For each incident photon energy $h\nu$, the photoelectrons emerging from the neutral surface have varying energies E, with a probability distribution $p_n(E)$. To account for electron escape from finite sized grains, yields measured for semi-infinite sheets in the laboratory have to be corrected by a factor f(E) (which introduces a size dependence). Such a correction would change the shape of the probability distribution as well as increase the integrated emission from a neutral surface (Draine 1978 gives an approximate expression for the overall increase). Then, formally

$$\hat{Y} = Y_n \int_{E_o}^{(h\nu - V_n)} f p_n dE,$$
(144)

where $E_0 = \max\{0, V_g\}$ introduces the fact that the lowest energy photoelectrons do not escape from positively charged grains.

The form adopted is

$$Y_n = \min\{ Y_0 (1 - V_n / h\nu), Y_1 \}$$
(145)

for $h\nu \geq V_n$, and $V_n = 8$ eV and $Y_0 = 0.5$ is assumed for both grain populations; according to Draine (1978) this combination gives about the right amount of photoelectric emission to heat neutral H I clouds in interstellar space ($h\nu \leq 13.6$ eV). For the higher energies a cap at $Y_1 = 0.2$ is introduced, which is suggested by experimental data. For p_n a simple form which is independent of E (Draine 1978) is adopted:

$$p_n = (h\nu - V_n)^{-1}.$$
 (146)

While only approximate, this induces the physically correct response (decrease) in \hat{Y} (and the photoelectric heating) when the grain is positively charged. Because the form of f(E) is highly uncertain f = 1 is assumed (this again avoids a size dependency). Extension of the flat cap in Y_n to high energies also addresses this issue to some degree. With these assumptions, \hat{Y} is known in analytic form:

$$\hat{Y} = Y_n \min\{1, 1 - V_g/(h\nu - V_n)\}.$$
(147)

21.3 Collisional Charging of a Grain

Per unit projected area of a grain, collisions with particles of space density N, mass m, and charge Z (Z = -1 for electrons) give an effective recombination rate

$$\alpha(gr) = -N\,\bar{v}\,SZ\,\eta,\tag{148}$$

where $\bar{v} = \sqrt{8kT/\pi m}$ is the mean particle speed. In this expression, and for other collisional rates involving N below, it is implicit that there is a sum of similar terms over all species in the gas. For electrons S is the sticking probability which we take to be 1 (Spitzer 1948; Watson 1972; Draine 1978). For positively charged nuclei, SZ is the charge transfer efficiency, taken to be Z here. The last factor η , the correction for Coulomb interactions between the grain and the recombining particles of charge Z, is given in terms of $\psi = ZV_q/kT_e$ by

$$\eta = \begin{cases} 1 - \psi & \text{if } \psi \le 0\\ \exp(-\psi) & \text{if } \psi > 0. \end{cases}$$
(149)

Terms for positively charged nuclei are included, but are usually small relative to the contribution from free electrons.

21.4 Grain Potential

The steady state grain potential is determined for each grain species independently by requiring charge balance: $\alpha_{gr} = \Gamma_{gr}$. Because of the many dependencies on V_g , this is carried out numerically.

21.5 Grain Drift Velocity

The grain drift velocity is determined by balancing the radiative acceleration due to the direct attenuated radiation field with the drag forces given by equations 1–6 of Draine and Salpeter (1979). The equations are solved numerically for the drift velocity, including interactions with electrons and all ions present in the gas.

21.6 Radiative Heating and Cooling of a Grain

Once the grain potential is known, the radiative rate of heating of the grain per unit projected area is

$$G_{grain}(rad) = \int_0^{\nu_o} Q_{abs} 4\pi J \, d\nu + \int_{\nu_o}^{\infty} Q_{abs} \frac{4\pi J}{h\nu} (h\nu - \widehat{EY}) \, d\nu.$$
(150)

The last term represents the portion of the photon energy that does not heat the grain, but rather passes to the escaping electrons:

$$\widehat{EY} = Y_n \int_{E_o}^{(h\nu - V_n)} E f p_n dE.$$
(151)

With the above approximations for f and p_n this is given analytically by

$$\widehat{EY} = 0.5 Y_n \min\{(h\nu - V_n), \left[(h\nu - V_n)^2 - V_g^2\right] / (h\nu - V_n)\}.$$
(152)

The cooling of a grain by radiative losses, per unit projected area, is given by

$$\Lambda_{grain}(rad) = \int_0^\infty Q_{abs} 4\pi B_\nu(T_g) \, d\nu \tag{153}$$

where $B_{\nu}(T_g)$ is the Planck function for the grain temperature.

21.7 Collisional Heating of a Grain

Collisions with electrons, ions, and neutral particles also heat the grains. Per unit projected area of the grain, this heating rate may be written as

$$G_{grain}(col) = N \,\bar{v} \,S \left(2kT_e\xi - ZV_g\eta + I\eta - 2kT_g\eta\right). \tag{154}$$

The first term corresponds to kinetic energy extracted from the gas. The factor ξ makes adjustment for Coulomb interactions and is given by

$$\xi = \begin{cases} 1 - \psi/2 & \text{if } \psi \le 0\\ (1 + \psi/2) \exp(-\psi) & \text{if } \psi > 0. \end{cases}$$
(155)

The second term in $G_{grain}(col)$ allows for the change of the particle's energy in the grain potential. In the third term, the product $I\eta$ is the average chemical energy released per impact; here it is assumed that when impinging ions recombine the ionization energy released is deposited as heat in the grain (there is then no corresponding term for heating the gas in Λ_g below). The last term describes the effect of thermal evaporation of neutralized ions and thermally accommodated neutral particles (there is no corresponding term for electrons).

In implementing the above processes, S for electrons is again the sticking probability. For positively charged nuclei, S is the energy transfer efficiency, taken here to be unity (this process should be evaluated consistently with that for charge transfer). For neutral particles of mass m striking a grain whose typical atom has mass M, the accommodation coefficient $S \simeq 2mM/(m+M)^2$ (Draine 1978).

21.8 Grain Temperature

The equilibrium grain temperature is determined by the balance between cooling (L) and heating (G) by radiative and collisional processes. For the radiative terms, Q_{abs} averaged over the size distribution is used to obtain a typical temperature for each species.

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As a test of the bandwidth of the code, and its behavior in a well-defined limit, tests where computed in which the grains were irradiated by black body radiation in strict thermodynamic equilibrium (i.e., the color and energy density temperatures were equal). Radiation temperatures between 10K and 10^9 K, the temperature limits to the code, were used. These tests showed that the deduced grain equilibrium temperature was within much better than 1 percent of the blackbody temperature.

21.9 Photoelectric Heating of the Gas

Heating of the gas by photoemission from grains can be an important process in ionized regions (Oliveira and Maciel 1986). For charged grains this heating rate (erg $cm^{-3} s^{-1}$) is given by

$$G_{gas} = \int_{\nu_o}^{\infty} \kappa_a \frac{4\pi J}{h\nu} \left(\widehat{EY} - V_g \hat{Y}\right) d\nu.$$
(156)

The first term describes the energy of the photoelectrons as they leave the surface, balancing the similar term in $G_{grain}(rad)$. The second term compensates for the grain potential, and can be seen to balance the related term in $G_g(col)$ when charge balance holds.

21.10 Collisional Cooling of the Gas

The gas is cooled as the gas particles hit the cooler grain surface. Per unit volume, this cooling rate may be written as

$$\Lambda_{gas} = N N_{\rm H} \sigma \, \bar{v} \, S \, (2kT_e \xi - 2kT_g \eta), \tag{157}$$

the individual terms consistently balancing the corresponding ones in $G_g(col)$.

22 OTHER PHYSICAL PROCESSES

22.1 Cosmic Ray Interactions

Synchrotron radio sources are usually modeled in terms of an interaction between a magnetic field and a relativistic gas with a typical energy per electron of a few hundred MeV (see Pacholczyk 1970; Longair 1981). The spectral index of the radio emission for radio-loud active galaxies is usually ~ -0.7, and this suggests that the electrons, which make the dominant contribution to synchrotron emission, have a density (per unit energy interval) given by $N(cr, E) \sim E^{-2.4}$ (Kellerman 1966). The total relativistic electron density is sensitive to the lower bound of the energy distribution, which is typically of order 10—100 MeV, corresponding to relativistic factor of $\gamma \sim 10$ –100 (Lee and Holman 1978).

The cosmic ray density used by CLOUDY is defined as

$$N(cr) = \int_{E_{min}}^{E_{max}} N(cr, E) dE$$
(158)

with the lower bound set to $E_{min} = 5$ MeV, corresponding to $\gamma \approx 10$. The density is only weakly sensitive to the upper limit $E_{max} \approx 10$ GeV because of the strong convergence of the electron density function, although uncertainties in the lower energy bound introduce a fundamental uncertainty. Cosmic ray protons should have much smaller affects than the electrons, so the total cosmic ray electron density N(cr) is the only parameter.

The code assumes that the gas is "optically thin" to the energetic electrons. Serious and fundamental uncertainties afflict detailed treatments of the penetration of energetic particles into gas, particularly if magnetic fields are present. In the simplest case penetration is impeded only by ionization and heating losses resulting from two-body collisions. In this case the ability to heat an entire cloud is determined by the range of a particle, or the column density of gas required to stop it (see Rossi 1952). Relativistic electrons have a range that is given to within 15% by (Berger and Seltzer 1965)

$$R_e = 10^{25} \left(\frac{E}{100 \ M eV}\right)^{0.8} \ cm^{-2} \tag{159}$$

for a gas composed of neutral hydrogen. The range of a 100 MeV electron in a fully ionized gas, in which bremsstrahlung and Coulomb losses are more important than ionization, would be some 10 times smaller.

The relativistic particles both heat and ionize the gas. The main concern is for the rate with which energy is transferred to the cold gas (Lea and Holman 1978; Ginzberg and Syrovatskii 1964). In the H^+ zone the main interaction will be with free electrons.

Kinetic energy is passed to the cold electrons at a rate

$$G_{cr} = 8.5 \times 10^{-19} N_e N(cr) \ ergs \ cm^{-3} \ s^{-1} \tag{160}$$

by direct Coulomb interactions (Jackson 1975; Spitzer 1962; Ginzburg and Syrovatskii 1964; Pacholczyk 1970). Here N_e is the thermal electron density, and we have integrated over the electron distribution given above.

In the H° zone the main interaction between thermal and relativistic gases is through ionization of the cold gas. For large neutral fractions very little of the energy of secondary electrons goes into actually heating the gas (Rossi 1952; Spitzer and Tomasko 1968); calculations show that secondary electrons have typical energies of ~40 eV, and that there is roughly one ionization per 15 eV deposited. Using the Bethe-Bloch approximation (Ginzburg and Syrovatskii 1964) the neutral heating rate is

$$G_{cr} = 3.7 \times 10^{-20} N(H^{\circ}) N(cr) \ ergs \ cm^{-3} \ s^{-1}$$
(161)

and the \mathbf{H}^{o} ionization rate is

$$\Gamma = 1.5 \times 10^{-8} N(cr) N(H^{\circ}) cm^{-3} s^{-1} \quad .$$
(162)

This ionization rate was scaled through Lotz's (1967) curves to include collisional ionization of heavy elements in the calculation of heavy element ionization equilibria.

If cosmic rays are not included, and the hydrogen ground state photoionization rate falls below the galactic background cosmic ray ionization rate, then a comment will be generated warning that the cosmic ray background should perhaps be included. According to Spitzer (1978), the background cosmic ray ionization rate is very uncertain, but of the order of 10^{-17} s⁻¹ for neutral hydrogen. According to the equations above, this rate corresponds to a cosmic ray density of ~ 10^{-9} cm⁻³, the value used as the "background" cosmic ray density for the COSMIC RAY command.

The discussion above, as well as the code, includes only two-body Coulomb interactions, and *does not* include collective effects, such as those discussed by Scott et al. (1980). Rephaeli (1987) notes that collective effects may not be important in most circumstances.

22.2 Line Radiation Pressure

Line radiation pressure was implemented in CLOUDY in collaboration with Moshe Elitzur. The following was written in collaboration with Moshe, and is adopted from Elitzur and Ferland (1986).

For radiation intensity I_{ν} , the standard expression for the radiation pressure per unit frequency, P_{ν} , is (e.g. Schwarzschild 1965)

$$P_{\nu} = \frac{1}{c} \int I_{\nu} \mu^2 d\Omega \quad , \tag{163}$$

where $\mu = \cos \theta$ and θ is the direction of propagation of the radiation. When the radiation field is isotropic, its pressure and energy density,

$$U_{\nu} = \frac{1}{c} \int I_{\nu} \Omega \quad , \tag{164}$$

are related by the familiar expression

$$P_{\nu} = \frac{1}{3}U_{\nu} \quad . \tag{165}$$

This relation holds for a rather wide range of circumstances. If the angular distribution of I_{ν} is expanded in a power series in μ , then only powers higher than the second will lead to violations of equation 165. However, the successive coefficients of this expansion are decreasing approximately like the optical depth (e.g. Schwarzschild 1965, p 40), so deviations from equation 165 will only be proportional to $1/\tau^2$. Hence, when the medium is optically thick at the frequency ν equation 165 is an excellent approximation for the radiation pressure.

The only radiative quantity we need to know in order to calculate the radiation pressure is the angle-averaged flux, J_{ν} , since

$$U_{\nu} = \frac{1}{c} 4\pi J_{\nu} \quad . \tag{166}$$

The integrated radiation pressure is then

$$P(\nu) = \frac{4\pi}{3c} \int J_{\nu} \, d\nu \quad . \tag{167}$$

Introducing the line-width, defined by

$$\Delta \nu = \frac{1}{\bar{J}} \int J_{\nu} \, d\nu \quad , \tag{168}$$

where

$$\bar{J} = \int J_{\nu} \Phi(\nu) \, d\nu \tag{169}$$

is the integrated mean intensity in the line and $\Phi(\nu)$ is the normalized line profile $[\int \Phi(\nu) d\nu = 1]$. The quantity \bar{J} is readily available in the escape probability approximation because it is related directly to the source function S by

$$\bar{J} = S(1 - P_l) \tag{170}$$

where P_l is the photon escape probability. The line source function S is simply $B_{\nu}(T_{exc})$, the Planck function of the line excitation temperature. The final expression for the pressure due to a line at frequency ν is therefore

$$P(\nu) = \frac{4\pi}{3c} B_{\nu}(T_{exc}) \,\Delta\nu \,(1 - P_e) \quad. \tag{171}$$

22.2 Line Radiation Pressure

The line width is a crucial parameter in the calculations since the line radiation pressure is directly proportional to it. For lines with a moderate optical depth (i.e., $\tau \leq 10^4$) the damping wings are optically thin, and the line emission profile is essentially identical to the absorption profile. In this case $\Phi(\nu)$ is simply described by the Doppler profile $\pi^{1/2} \exp(-x^2)$, where $x = (\nu - \nu_o)/\Delta\nu_d$ is the dimensionless frequency shift from line center and $\Delta\nu_d = (2kT/m)^{1/2}\nu_o/c$ is the Doppler width. The line width is then

$$\Delta \nu = \Delta \nu_D \times 2(\ln \tau)^{1/2} \tag{172}$$

for $\tau \gg 1$.

The situation when the line optical depth exceeds ~ 10^4 is much more complicated because scattering in the damping wings becomes significant, and the frequency dependence of the emission profile is not known before the entire radiative transfer problem is solved. In general, it is known that, for Ly α (generally the most important source of line radiation pressure) and large optical depths, the line width (in dimensionless units) is

$$x = k(a\tau)^{1/3} , (173)$$

(Adams 1972; Harrington 1973; Bonilha et al. 1979). In this expression a is the damping constant ($a \sim 4.7 \times 10^{-4}$ for Ly α), τ is the line center optical depth, and k is a number of order unity.

The frequency width required here is the value that will provide a rectangular profile with the same area as the proper integral of the source function. The results of Adams (1972) are adopted, and the resulting expression for the full line width in the case of large optical depths $(a\tau \gg 1)$ is

$$\Delta \nu = \Delta \nu_D \, 2.3 \, (a\tau)^{1/3} \tag{174}$$

An important point, evident from the plots provided by Adams for the source function as a function of frequency (his Fig 3), is that the width of the frequency distribution varies very little with position in the slab. This is also evident from the mean intensity plots of Harrington, as mentioned above, and is a result of the strong coupling between distant regions caused by scattering in the line wings. The expression provided in equation 174 for all locations in the slab, with τ being half the total slab thickness.

Background opacity is included in the determination of the level populations using the formalism outlined in the section on line radiative transfer. Its main effect is to lower the line excitation temperature by providing a second "escape" (actually destruction) route for trapped photons. This is assumed to be the only effect background opacity has on radiation pressure. Balmer continuous absorption typically has an optical depth of order unity, while the line optical depths are many orders of magnitude larger. Absorption in the Balmer continuum can only compete with line scattering in the extreme wings, at frequency shifts exceeding $\sim (a\tau)^{1/2}$, which are much larger than the line width predicted by equation 174.

Collisional de-excitation can also break the assumption of pure scattering because a photon will be lost to the thermal pool before the radiative process can take place. This will happen when the density is high enough that the rate for collisional de-excitation, C_{ul} , exceeds the probability for the effective rate for the transition, $P_l A_{ul}$, where P_l is the line escape probability and A_{ul} is the Einstein coefficient. Because at large optical depths P_l is essentially equal to τ^{-1} , the "effectively thin" assumption breaks down when

$$\tau \sim A_{ul}/C_{ul} \quad . \tag{175}$$

Once the line optical depth exceeds $\sim A/C$, a "thermalization limit" is encountered, and the assumption of a purely scattering nebula does not apply anymore. Therefore, in evaluating the optical depth for the line width expression (equation 174) the minimum of the actual line optical depth and the one prescribed by A/C is used. this is a conservative estimate of the effect of collisions on photon scattering. This is probably the most poorly understood part of the calculation of the line radiation pressure.

22.3 Radiative Acceleration

The radiative acceleration (cm s⁻²) due to the direct attenuated continuum flux F_{ν} , for density ρ , is given by

$$a_{rad} = \frac{1}{\rho c} \int F_{\nu} \hat{\kappa}_{\nu} \, d\nu + \frac{1}{\rho c} \sum_{l} F_{\nu}(l) \kappa_{l} \gamma_{l}.$$
(176)

Here $\hat{\kappa}$ is the effective continuous opacity; it includes the usual photoelectric, and free-free absorption in the gas, and Compton and Rayleigh scattering. In addition it includes $\kappa_a + (1-g)\kappa_s$ for the grain contributions if grains are present. The integral is over all energies considered by the code (from $\lambda \approx 1 \text{ cm to } h\nu \approx 100 \text{ MeV}$). The second term is a sum is over roughly a dozen strong ultraviolet and optical resonance lines; κ_l is the line opacity, B_l is the Einstein coefficient, and γ_l is the escape probability in the direction towards the source of ionizing radiation (Ferland and Rees 1988).

Really, something like 10^6 lines are needed for a realistic calculation of the radiative acceleration (Abbott 1982). The approximations used here will underestimate the actual radiative acceleration by as much as a factor of two, depending on the level of ionization of the gas and form of the incident continuum.

When the pressure is held constant (with the "CONSTANT PRESSURE" command) the pressure law is given by

$$P(r) = P_{gas}(r_o) + \int a_{rad} \ \rho \ dr = P_{gas}(r) + P_{line}(r)$$
(177)

where

$$P_{gas}(r_o) = N_{tot}kT \tag{178}$$

is the gas pressure at the illuminated face of the cloud, N_{tot} is the total particle density, and r is the radius in question. The gas pressure is stored as the variable PGAS and is evaluated in routine PTOT. The line radiation pressure is evaluated as described above, and its total is stored as the variable PRAD which is also evaluated in PTOT. Finally, the integrated radiative force on the gas is evaluated in routine RADINC and is stored as the variable PINTEG.

22.4 Wind Geometry

CLOUDY will do a simple wind geometry if the "WIND" command is specified. The effective acceleration is written as $a_{eff} = a_{rad} - g_{grav}$, where a_{rad} is computed as above, and g_{grav} is the inward gravitational acceleration due to the central object. The default is one solar mass. The velocity is computed assuming that the acceleration is constant across the zone. In this case the velocity v at the outer edge of a zone of thickness dr will be

$$v = \frac{v_o + \sqrt{v_o^2 + 4 \, a_{eff} \, dr}}{2} \tag{179}$$

where v_o is the velocity at the inner edge. The calculation will stop if the velocity ever falls below zero.

The density at the illuminated face of the cloud is entered with the "HDEN" command, and the density is varied across the model to conserve mass flux (i.e., the product $\rho(r)r^2 v(r)$ is kept constant). Because of this, a filling factor would not make physical sense, and should not be used. Note also that it is usually necessary to set an outer radius when a wind model is computed to stop the calculation from extending to infinity.

A simple Sobolev approximation is used for line transfer when a wind is computed. The effective optical depth is given by;

$$\tau_{lu}(R) = \alpha_{lu} \left(N_l - N_u \frac{g_l}{g_u} \right) R \frac{v_{thermal}}{v_{expansion}}$$
(180)

where R is the radius and $v_{thermal}$ and $v_{expansion}$ are the thermal and expansion velocities respectively.

Figure 21 shows a test case in which a wind is driven in the plane parallel electron scattering limit. As can be seen the numerical solution is in excellent agreement with the analytically predicted result.

The cooling (erg $cm^{-3} s^{-1}$) due to the hydrodynamic expansion of the gas is given by

$$\Lambda_{exp} = -kT \frac{dN}{dt} = N \left[\frac{a}{v} + \frac{2v}{R} \right]$$
(181)

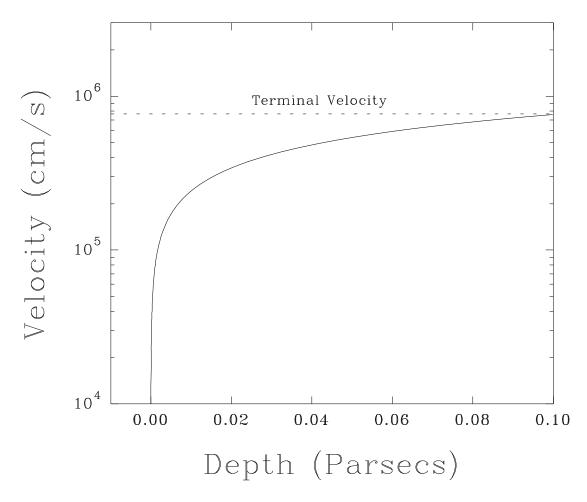


Figure 21: The wind velocity is computed using the input stream shown in one of the test cases in section 25. Parameters were chosen to have a readily computed final velocity. The velocity at the outer edge of the slab is within 1 percent of its expected value, wind

where N, a, v, and R are the total particle density, acceleration, wind velocity, and radius respectively.

22.5 Secondary Ionization

Secondary ionizations by supra-thermal electrons are treated following Shull and van Steenberg (1985). All sources of energetic electrons, including both Auger and primary electrons, are considered in the initial input of high-energy electrons into the gas. The resulting flux of non-thermal electrons is stored as the variable CSUPRA, which has units $\rm cm^{-2}~s^{-1}$. A typical energy of an electron in the non-thermal shower is ~ 20 eV; this energy is used to evaluate collisional ionization and excitation cross sections. Secondary ionization is included among the general ionization processes considered for all species.

22.6 Jeans Length and Mass

The Jeans length and mass are computed for each zone in the calculation. The smallest computed Jeans length and mass are saved, and a note is printed at the end of the calculation if the computed structure is Jeans unstable.

The expression for the Jeans length is

$$\lambda_J = \left(\frac{\pi kT}{\mu m_H G\rho}\right)^{1/2} = 6.257 \times 10^7 \left(\frac{T}{\mu\rho}\right)^{1/2} cm \tag{182}$$

where μ is the mean molecular weight of the gas (referred to as the variable WMOLE) and ρ is the density of the gas (gm, referred to as the variable DENSTY). Both are computed in routine PTOT.

The Jeans mass is then given by

$$M_J = \frac{4\pi}{3} \rho \left(\frac{\lambda_J}{2}\right)^3 gm \tag{183}$$

where the mass is that of a sphere with radius $\lambda_J/2$.

23 OTHER DETAILS

23.1 Geometry

This section defines the internal variables used to describe the geometry. The geometry is always spherical, but can be made effectively plane parallel by making the inner radius of the cloud much larger than its thickness.

Most variables having to do with the geometry are set and incremented in routine NEWRAD.

RINNER This is the separation between the center of symmetry (i.e., the center of the central object) and the inner edge of the cloud. It remains constant throughout the calculation. If an inner radius is not specified then it is given the default value of 10^{25} cm. This will usually result in a plane parallel geometry.

DRAD This is the thickness of the current zone. Note that the zone size changes continuously throughout the calculation. Upper or lower limits to DRAD can be set with the DRMAX and DRMIN commands, described above.

RADIUS This is the distance between the center of symmetry and the *outer* edge of the current zone. For the first zone, RADIUS has the value RINNER+DRAD/2.

DEPTH This is the distance between the inner edge of the cloud and the *outer* edge of the current zone. For the first zone, RADIUS has the value DRAD/2.

ROUTER This is the limit to the outer radius of the structure, as set before the calculation begins. The default value is effectively infinite, actually 10^{30} cm.

R1R0SQ This is the sphericity ratio

$$R1R0SQ = \left(\frac{distance \ to \ center \ of \ zone}{inner \ radius}\right)^2 = \left(\frac{RADIUS - DRAD/2}{RINNER}\right)^2$$
(184)

A problem can arise under certain extreme circumstances. The depth variable DEPTH must be increased for every zone, by adding the zone thickness DRAD. Both variables are double precision. If the radio DRAD/DEPTH falls below $\sim 10^{-14}$ then the depth cannot be updated on most machines. The problem is that the sum DEPTH+DRAD will be equal to DEPTH because of numerical underflow. If this occurs (i.e., the zone thickness DRAD falls below DEPTH/10¹⁴) the code will stop, with the comment than the zone thickness is too small relative to the depth. There is no obvious solution to this problem.

23.1 Geometry

- **PIRSQ** This is the log of the inner area $(4\pi r_{inner}^2)$.
- **DREFF** This is the effective radius, $dr_{eff} = dr \times f(r)$ where f(r) is the filling factor.
- **DVEFF** This is the effective volume relative to the inner radius.

24 COMPARISON CALCULATIONS

This section presents comparisons between the current predictions of the code, and results from other independent calculations. The "other" calculations are from the compendium resulting from the Meudon (1985) meeting on model nebulae edited by Daniel Pequignot.

The scatter among the calculations, as well as the changes that have occurred in the predictions made by CLOUDY, are in some sense an indication of the stability and reliability of these types of extreme non-LTE calculations. The largest discrepancies between current predictions made by CLOUDY and the other models (which were computed in 1985) are due to changes which have occurred in the atomic data base between 1985 and the present. In general, the strongest lines are in very good agreement (as they must because of energy conservation) while weak lines (which are very sensitive to changes in the computed temperature and ionization structure) scatter by nearly a factor of two.

24.1 Paris Planetary Nebula

This compares current predictions of the code with those of other participants at the Meudon meeting on photoionization calculations, for the case of ionization by a very hot black body. The input used to generate this model planetary nebula is shown in the sample input section. The model results are very sensitive to the detailed transfer of HeII Ly α ; this line is the dominant heat source across the model nebula. The parameters were chosen to be roughly similar to NGC 7027, a very well studied object.

Line		Harrington	Netzer	Pequignot	Mean
${ m H}eta$	erg/s	2.64E35	$2.51\mathrm{E}35$	2.67E35	$2.60\pm0.09\mathrm{E}35$
He I	5876	0.097	0.11	0.11	$0.106 {\pm} 0.008$
He II	4686	0.336	0.350	0.316	$0.334 {\pm} 0.017$
C II	2326	0.498	0.310	0.323	$0.377 {\pm} 0.105$
C III]	1909	1.67	1.73	1.70	$1.70 {\pm} 0.03$
C IV	1549	1.70	1.19	2.02	1.64 ± 0.42
[N I]	5200	0.020	0.010	0.017	$0.016 {\pm} 0.005$
[N II]	6584	1.12	1.10	1.03	$1.08 {\pm} 0.05$
N III]	1749	0.118	0.090	0.112	$0.107 {\pm} 0.015$
N IV]	1487	0.116	0.090	0.160	$0.122 {\pm} 0.035$
N V	1240	0.079	0.040	0.148	$0.089 {\pm} 0.55$
[O I]	6300	0.117	0.112	0.101	0.110 ± 0.008
[0 II]	3727	2.28	2.24	2.18	$2.23 {\pm} 0.05$
[O III]	5007	16.12	16.84	17.28	$16.74 {\pm} 0.58$
[O III]	4363	0.159	0.150	0.156	$0.155 {\pm} 0.005$
[O III]	$52 \mu { m m}$	1.44	1.42	1.43	1.43 ± 0.01
O IV]	1403	0.149	0.070	0.179	$0.132 {\pm} 0.56$
0 V]	1218	0.073	0.030	0.178	$0.094 {\pm} 0.076$
[Ne II]	$12.8 \mu { m m}$	0.023	0.030	0.032	$0.0285 {\pm} 0.004$
[Ne III]	$15.5 \mu { m m}$	2.56	2.44	2.54	$2.51 {\pm} 0.06$
[Ne III]	3869	2.05	1.92	1.98	$1.98 {\pm} 0.06$
Ne IV]	2423	0.62	0.43	0.62	$0.556 {\pm} 0.110$
[Ne V]	3426	0.48	0.44	0.69	$0.535 {\pm} 0.132$
[Ne V]	$24.2 \mu \mathrm{m}$	1.58	1.85	1.58	1.67 ± 0.16
Mg II	2798	1.46	1.00	1.97	$1.48 {\pm} 0.49$
Mg IV	$4.5 \mu { m m}$	0.074	-	0.099	$0.086 {\pm} 0.018$
Si II	$34.8 \mu { m m}$	-	0.12	0.15	$0.133 {\pm} 0.018$
Si II	2335	-	0.10	0.126	0.113 ± 0.018
Si III	1892	0.198	0.13	0.262	$0.197 {\pm} 0.067$
Si IV	1397	0.142	0.11	0.203	$0.152 {\pm} 0.047$
S II	6720	0.456	0.33	0.385	$0.390 {\pm} 0.063$
S II	4070	0.078	0.06	0.0642	$0.0674 {\pm} 0.009$
S III	$18.7 \mu { m m}$	0.493	0.52	0.446	$0.486 {\pm} 0.037$
S III	9532	1.36	1.70	1.37	$1.48 {\pm} 0.206$
S IV	$10.5 \mu { m m}$	2.21	1.66	1.88	$1.92 {\pm} 0.277$

Table 20: Paris Meeting Planetary Nebula

24.2 Paris HII Region

This compares current predictions of the code with those of other participants at the Meudon meeting on photoionization calculations for the case of a simple spherical HII region. The input used to generate this model HII region is shown in the sample input section.

Line		Mean	74.23	76.03	80.06
${ m H}eta$	erg/s	$2.60\pm0.09\mathrm{E}35$	$2.57\mathrm{E}35$	2.66 E35	2.52 E35
He I	5876	$0.106 {\pm} 0.008$	0.11	0.11	0.107
He II	4686	$0.334 {\pm} 0.017$	0.294	0.319	0.354
C II	2326	$0.377 {\pm} 0.105$	0.359	0.352	0.373
C III]	1909	$1.70 {\pm} 0.03$	1.572	1.48	1.72
C IV	1549	1.64 ± 0.42	2.237	2.76	2.48
[N I]	5200	$0.016 {\pm} 0.005$	0.009	0.009	0.009
[N II]	6584	$1.08{\pm}0.05$	1.06	1.05	1.08
N III]	1749	$0.107 {\pm} 0.015$	0.097	0.081	0.096
N IV]	1487	$0.122 {\pm} 0.035$	0.164	0.119	0.109
N V	1240	$0.089 {\pm} 0.055$	0.142	0.093	0.061
[O I]	6300	$0.110 {\pm} 0.008$	0.112	0.111	0.119
[0 II]	3727	$2.23 {\pm} 0.05$	2.24	2.19	2.35
[O III]	5007	$16.74 {\pm} 0.58$	15.94	15.81	15.30
[0 III]	4363	$0.155 {\pm} 0.005$	0.142	0.125	0.149
[O III]	$52 \mu { m m}$	$1.43 {\pm} 0.01$	1.40	1.35	1.37
[0 IV]	$26 \mu { m m}$	-	-	-	3.42
O IV]	1403	$0.132 {\pm} 0.056$	0.187	0.215	0.105
0 V]	1218	$0.094 {\pm} 0.076$	0.169	0.109	0.067
[Ne II]	$12.8 \mu { m m}$	$0.0285 {\pm} 0.004$	0.033	0.034	0.034
[Ne III]	$15.5\mu{ m m}$	$2.51 {\pm} 0.06$	2.77	2.70	2.67
[Ne III]	3869	$1.98 {\pm} 0.06$	2.41	2.26	2.43
Ne IV]	2423		0.62	0.514	0.513
[Ne V]		$0.535 {\pm} 0.132$	0.48	0.404	0.401
[Ne V]	$24.2 \mu \mathrm{m}$	1.67 ± 0.16	0.241	0.247	1.007
Mg II	2798	1.48 ± 0.49	0.830	1.82	1.96
Mg IV	$4.5 \mu { m m}$	$0.086 {\pm} 0.018$	0.116	0.130	0.135
Si II	$34.8 \mu { m m}$	$0.133 {\pm} 0.018$	0.156	0.162	0.162
Si II	2335	$0.113 {\pm} 0.018$	0.150	0.144	0.158
Si III	1892	$0.197 {\pm} 0.067$	0.322	0.417	0.419
Si IV	1397	$0.152 {\pm} 0.047$	0.168	0.240	0.222
S II	6720	$0.390 {\pm} 0.063$	0.382	0.679	0.662
S II	4070	$0.0674 {\pm} 0.009$	0.0647	0.121	0.118
S III	$18.7 \mu { m m}$	$0.486 {\pm} 0.037$	0.580	0.706	0.673
S III	9532	$1.48 {\pm} 0.19$	1.69	2.11	2.07
S IV	$10.5 \mu { m m}$	$1.92 {\pm} 0.28$	1.64	1.32	1.53

Table 21: Paris Planetary vs CLOUDY

Table 22: Paris Meeting HII Region

Line		Harrington	Rubin	Netzer	Pequignot	Mean
${ m H}eta$	erg/s	$2.04\mathrm{E}37$	$2.07\mathrm{E}37$	$2.09\mathrm{E}37$	2.03 E37	$2.06\pm0.03\mathrm{E37}$
$Ly\alpha$	1216	-	-	21.9	23.5	22.7 ± 1.1
He I	5876	0.116	-	0.120	0.113	0.116 ± 0.004
C II	2326	0.169	-	0.18	0.149	0.166 ± 0.016
C II	1335	0.080	-	0.080	0.079	$0.080 {\pm} 0.0006$
C III]	1909	0.059	-	0.04	0.0551	0.051 ± 0.0099
[N II]	6584	0.538	0.565	0.51	0.569	0.546 ± 0.027
[O I]	6300	0.0056	0.0095	0.007	0.0062	0.0072 ± 0.0017
[0 II]	7330	0.0283	0.0347	0.026	0.0266	0.0289 ± 0.0040
[O II]	3727	2.03	2.29	1.73	2.00	2.01 ± 0.23
[O III]	$52 \mu { m m}$	1.11	1.07	1.22	1.00	$1.10 {\pm} 0.092$
[O III]	5007	1.53	1.46	1.49	1.62	1.525 ± 0.069
O III	4363	0.0035	0.0033	0.003	0.0033	0.0033 ± 0.0002
O IV	$26 \mu { m m}$	0.0008	-	0.002	0.0019	0.0016 ± 0.0007
[Ne II]	$12.8 \mu\mathrm{m}$	0.182	0.226	0.18	0.24	0.207 ± 0.031
[Ne III]	$15.5 \mu { m m}$	0.465	0.451	0.42	0.415	0.438 ± 0.024
[Ne III]	3869	0.077	0.0716	0.069	0.069	0.072 ± 0.004
[S II]	6725	0.152	0.161	0.1	0.150	0.141 ± 0.028
[S II]	4070	0.0067	0.0076	0.006	0.0064	0.0067 ± 0.0007
[S III]	$18.7 \mu { m m}$	0.556	0.577	0.54	0.510	0.546 ± 0.028
[S III]	9532	0.87	0.91	0.99	0.99	0.940 ± 0.061
[S IV]	$10.5 \mu { m m}$	0.411	0.326	0.43	0.410	0.394 ± 0.046

Line		Mean	76.03	80.06
$\mathrm{H}\beta$	erg/s	$2.06\pm0.03\mathrm{E37}$	$2.06\mathrm{E}37$	2.04E37
$Ly\alpha$	1216	22.7 ± 1.1	23.3	23.4
He I	5876	0.116 ± 0.004	0.116	0.116
C II	2326	0.166 ± 0.016	0.237	0.166
C II	1335	$0.080 {\pm} 0.0006$	0.0926	0.107
C III]	1909	0.051 ± 0.0099	0.060	0.108
[N II]	6584	0.546 ± 0.027	0.578	0.602
[O I]	6300	0.0072 ± 0.0017	0.0080	0.0081
[0 II]	7330	0.0289 ± 0.0040	0.0348	0.0368
[0 II]	3727	2.01 ± 0.23	2.287	2.43
[O III]	$52 \mu { m m}$	$1.10 {\pm} 0.092$	1.15	1.09
[O III]	5007	$1.525 {\pm} 0.069$	1.829	1.62
[O III]	4363	0.0033 ± 0.0002	0.0044	0.0041
[0 IV]	$26\mu{ m m}$	0.0016 ± 0.0007	0.0009	0.0007
[Ne II]	$12.8 \mu { m m}$	0.207 ± 0.031	0.219	0.230
[Ne III]	$15.5\mu{ m m}$	0.438 ± 0.024	0.469	0.450
[Ne III]	3869	0.072 ± 0.004	0.0938	0.089
[S II]	6725	0.141 ± 0.028	0.267	0.291
[S II]	4070	0.0067 ± 0.0007	0.0124	0.0136
[S III]	$18.7 \mu { m m}$	0.546 ± 0.028	0.542	0.528
[S III]	9532	0.940 ± 0.061	1.04	1.04
[S IV]	$10.5 \mu { m m}$	0.394 ± 0.046	0.0852	0.108

Table 23: Paris HII Region vs CLOUDY

24.3 Paris NLR Model

This compares current predictions of the code with those of other participants at the Meudon meeting on photoionization calculations, for a model similar to the NLR of active nuclei.

Line		Netzer	Pequignot	Binette	Kraemer	Mean
$H\beta$	$erg/s/cm^2$	0.129	0.134	0.124	0.12	0.127 ± 0.006
${ m H}eta$	4861	1.00	1.00	1.00	1.00	1.00
$Ly\alpha$	1216	35.3	33.1	-	24.0	30.8 ± 6.0
He I	5876	0.095	0.098	0.092	0.090	0.094 ± 0.004
He II	4686	0.36	0.32	0.38	0.37	$0.358 {\pm} 0.026$
C II	2326	0.96	0.77	1.70	1.06	1.12 ± 0.40
C II	1335	0.14	0.14	0.20	0.08	0.14 ± 0.05
C III]	1909	4.59	4.99	6.50	4.91	5.25 ± 0.85
C IV	1509 1549	$\frac{4.03}{7.03}$	$\frac{4.33}{7.20}$	5.30	$\frac{4.91}{7.20}$	6.68 ± 0.93
[N I]	5200	0.31	0.33	0.82	0.37	0.08 ± 0.93 0.46 ± 0.24
[N II]	$5200 \\ 6548$	2.68	1.52	1.77	1.63	0.40 ± 0.24 1.90 ± 0.53
		0.40	$1.52 \\ 0.40$			
N III]	1749	0.40	0.40	0.43	0.48	0.428 ± 0.038
N IV]	1487	0.45	0.43	0.51	0.48	0.468 ± 0.035
N V	1240	0.32	0.30	0.32	0.28	0.305 ± 0.019
[O I]	$63.2~\mu{ m m}$	-	0.62	0.14	0.10	0.29 ± 0.29
[O I]	6300	1.32	0.90	1.62	1.04	1.22 ± 0.32
[O II]	7325	0.11	0.094	0.16	0.10	0.116 ± 0.03
[O II]	3727	3.4	2.62	4.41	2.73	3.29 ± 0.82
[O III]	$52 \mu { m m}$	2.5	2.54	2.31	2.65	$2.50{\pm}0.1$
[O III]	5007	27.36	27.36	23.28	27.76	26.44 ± 2.1
[O III]	4363	0.42	0.41	0.44	0.44	0.428 ± 0.01
O III]	1663	0.97	0.95	0.92	1.01	0.963 ± 0.03
[O IV]	$25.9 \mu m$	5.69	5.19	5.49		5.46 ± 0.2
O IV]	1403	0.53	0.44	0.51	0.66	0.534 ± 0.092
0 V]	1218	0.33	0.32	0.45	0.24	0.335 ± 0.080
O VI	$1210 \\ 1035$	$0.03 \\ 0.17$	0.32 0.17	$0.43 \\ 0.22$	0.24	0.165 ± 0.04
[Ne II]	$12.8 \mu m$	$0.11 \\ 0.28$	0.17	$0.22 \\ 0.48$	$0.10 \\ 0.13$	0.105 ± 0.04 0.268 ± 0.15
[Ne III]	$12.8\mu \mathrm{m}$ $15.5\mu \mathrm{m}$	2.8	2.62	1.83	1.25	2.13 ± 0.73
[Ne III]	15.5μ m 3869	$2.8 \\ 2.70$		$1.03 \\ 2.27$		
Ne IV]	2423	0.82	$\begin{array}{c} 2.59 \\ 0.79 \end{array}$	$\frac{2.27}{1.03}$	$\begin{array}{c} 1.67 \\ 1.12 \end{array}$	2.31 ± 0.4 0.94 ± 0.1
- 						
[Ne V]	$24.2\mu m$	3.54	2.64	3.54	-	3.24 ± 0.52
[Ne V]	3426	1.17	1.02	1.13	1.05	1.095 ± 0.06
Mg II	2798	1.58	1.43	1.51	1.10	1.40 ± 0.2
Si II	$34.8 \mu { m m}$	1.73	0.97	0.51	-	1.07 ± 0.6
Si II	2335	0.21	0.17	0.09	-	0.16 ± 0.0
Si III	1892	0.15	0.19	0.69	0.14	0.29 ± 0.2
Si IV	1397	0.21	0.14	0.02	0.13	$0.13 {\pm} 0.03$
S II	6720	1.00	0.62	1.29	0.37	$0.82 {\pm} 0.4$
S II	4070	0.07	0.04	0.078	0.03	0.055 ± 0.023
S III	$18.7 \mu { m m}$	0.75	0.49	0.68	0.65	0.64 ± 0.1
S III	9532	2.25	1.38	1.73	1.62	1.74 ± 0.3
S IV	$10.5 \mu m$	1.39	0.73	0.94	1.57	1.16 ± 0.3

Table 24: Paris Meeting NLR Model

25 SAMPLE INPUT

25.1 Limiting Cases

The following examples all have readily predictable answers, and demonstrate the behavior of the code in the appropriate limits.

```
title case A
c Seaton 1959 results; 4pi j (beta) = 5.56E-26
c for this model log totl H-beta = 4.745
c b(2)=3.73E-3 (3)=3.69E-2 (4)=0.0910 (5)=0.145 (6)=0.193
c n.b. very different results if not 1-mixed
no induced processes ; N.B. case A is a fiction; no induced transitions
hydrogen collisions off ; must turn off all collisions except 2s-2p
stop Lyman optical depth -6
constant temperature = 10,000K
print departure coef
stop zone 1
black body, T=50,000K
ionization parameter -2
hden = 15 ; must be high density to mix 2s, 2p
drmax 0
drmin 0
abundances -10
print short
```

Case A is a mathematical fiction; when the Lyman lines are optically thin continuum pumping must be important if the gas is ionized. Fluorescense is turned off with the "NO INDUCED PROCESSES" command. The density is set to a very high value $(10^{15} \text{ cm}^{-3})$ so that the 2s-2p states are well *l-mixed*, in keeping with standard casee A assumptions. As a result, collisional excitation would dominate the level populations, and hydrogen collisions must be turned off with the "hydrogen collisions off" command. The Lyman continuum optical depth is set to a small value to force the outward Ly α optical depth to a small value. The pair of DRMAX and DRMIN commands set the zone thickness to 1 cm. The abundances are set to a very small value so that the electron density is equal to the hydrogen density.

- departure coefficients for H, He levels
- neutral fractions
- $H\beta$ emissivity

```
title case B
c this is a test of the 10-level H atom
c this input will predict the Hb emissivity per
c unit vol; the answer should be 1.24E-25 (Seaton 1959)
c b(3) = 0.116; (4)=0.201; (5)=0.276; (6)=0.335
print departure coefficients
case b
constant temperature = 4
stop zone 1
black body, T=50,000K
ionization parameter -2
hden = 0
abundances -10
drmax O
drmin 0
print short
```

This test case compares the predictions of the ten level hydrogen atom with the Seaton (1959) results. The pair of DRMAX and DRMIN commands set the zone thickness to 1 cm. The "case b" command sets Lyman line optical depths to very large values.

Checks:

- departure coefficients for H, He levels
- neutral fractions
- $H\beta$ emissivity

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```
title hydrogen ionization in optically thin limit
c H cross sec=2.09E-18 cm<sup>2</sup>, rec coef(A)=4.18E-13
c answer is neutral fraction of 2.00E-4
laser 1.5 Ryd
hden 1
phi(h) = 10
iterate
print last iteration
stop lyman optical depth -6
constant temperature = 10,000K
stop zone 1
drmax 0
drmin 0
abundances -10
print short
```

This checks the calculation of the hydrogen photoionization equilibrium. The continuum is a "laser" peaked at 1.5 Ryd, where the hydrogen photoioinzation cross section is 2.09×10^{-18} cm⁻².

Checks:

• hydrogen neutral fraction is 2.00×10^{-4}

```
title Compton limit, test continuum partition
c test of thermal equil in compton limit; temp should EXACTLY equal 2E5K
c check continuum partition;
c energy range, photon densities, luminosities, follow
c 0.25-1. Q=26.6470 L=15.8190
                                   c 1-1.807 Q=26.8867 L=16.3766
c 1.807-4 Q=27.3042 L=17.0948
                                   c 4-20
                                              Q=27.2041 L=17.3179
c 20 --
           Q=22.9038 L=22.9038
                                   c total lumin 17.5597
c nufnu(912A) = 1.8029E+16
black body t=200,000K lte
grains -5 no heating, no cooling
hden = 6
stop zone 1
faint .1
print last short
metals -10
iterate
stop lyman continuum optical depth = -6
print departure coef
drmax 0
drmin 0
tolerance 0.0001 % decrease tolerance on heating cooling match
```

This tests the behaviour of the code in the Compton limit. The incident continuum is a blackbody in strict thermodynamic equilibrium. Strict thermodynamic equilibrium is expected for all constituents of the gas. The input stream also lists the expected photon fluxes for the incident continuum; this tests the normalization of the continuum, and its distribution. Grains are included to test confirm their behaviour in the LTE limit. The pair of DRMAX and DRMIN commands set the zone thickness to 1 cm.

- luminosity, photon flux, over various energy intervals, $4\pi J$ at 912Å.
- Electron temperature exactly 2×10^5 K.
- Grain temperature forced to 2×10^5 K by radiative processes.

This is mainly a test of the ability of the code to converge a model with a *very* strange electron density. The electrons are mainly contributed by heavy elements, and the gas is only slightly ionized.

- Electron density is correct.
- Hydrogen line spectrum strongly pumped by continuum.

```
title high electron density approach to lte
c test from Ferland and Rees 88, collisions drive H to LTE
c collisions should drive all departure coef to unity
constant temperature = 50,000
print departure coefficients
stop zone 1
stop lyman optical depth -6
black body t=50,000
ionization parameter -5
hden = 19
abundances -10
iterate
print last short
drmax 0
drmin 0
```

This model is a test of the behaviour of hydrogen and helium in the high density, collision dominated, limit. The temperature is preset, the hydrogen density is set to a very high value, and the ionization parameter is very low. The resulting model is collision dominated, so this case checks that the collision physics occurs in detailed balance. The predicted departure coefficients should all equal unity. The pair of DRMAX and DRMIN commands set the zone thickness to 1 cm.

Checks:

• Hydrogen departure coefficients *exactly* unity. (Density not high enough to bring helium departure coefficients to unity.)

```
title const temper black body limit from Ferland and Rees 1988
c tests whether departure coef are forced to unity by induced processes
constant temper 50,000
stop zone 1
grains -5 no heating no cooling
hden 10
stop lyman continuum optical depth -6
black body, t=50,000 lte
metals -10
print departure coef
faint -1
print short last
iterate
drmax 0
drmin 0
```

This example tests whether induced processes force level populations of hydrogen and helium to LTE when they are irradiated by a blackbody in strict thermodynamic equilibrium. The density is low enough value for radiation to dominate the rate equations coupling levels with each other and the continuum. The expectation is for all departure coefficients to equal unity. A small amount of grains are included to check that the grain thermal balance is handled properly in this radiation dominated limit. Checker

- Departure coefficients *exactly* unity.
- Grain temperature *exactly* 5×10^4 K.

```
title therm equil black body limit from Ferland and Rees 1988
c this tests whether thermal processes go to lte
stop zone 1
hden 10
stop lyman optical depth -6
black body, t=50,000 lte
abundances -10
print departure coef
print last short
iterate
drmax 0
drmin 0
```

This is the ultimate test of the bahaviour of the code in the strict thermodynamic equilibrium limit. The temperature is not held constant, so the resulting equilibrium temperature determines whether cooling processes are treated properly in the detailed balance limit. The equilibrium temperature should be exactly 5×10^4 K, and all departure coefficients should equal unity. A small amount of grains are included to check that the grain thermal balance is handled properly in this limit.

- Electron temperature *exactly* 5×10^4 K.
- Departure coefficients unity.

```
title check pure hydrogen sphere
c the answer is R(Stromgren) = 4.16e+17
hden 4
sphere static
radius 16
blackbody 50,000k
q(h) 49
stop eden 3.
constant temperature 7500
abundances -10
print short
```

This is a test of the conservation of photon number across a sperical model. The estimate of the Strömgren radius comes from arguments similar to those given in Osterbrock's book. The low temperature ensures that collisional ionization and excitation are unimportant. The "STOP EDEN" command is used to stop the code near the hydrogen ionization front.

- Strömgren radius exactly $4.16\times 10^{17}~{\rm cm}.$
- Compare predicted, case B, and Q(H), $H\beta$ luminosity.

```
title test against Van Blerkom and Hummer, Fig 4
 tests hydrogen grd state rec effic against vb+h exact results
С
  this is their case e) - "Zero contition"
С
  their answer for HO/Htot at the illuminated edge is approx 5.8E-4,
С
С
  and a Stromgren radius of roughly 7.8E16 cm
hden 4
blackbody 50,000k
phi(h) 12.30103
stop eden 3.5
constant temperature 4
abundances -10
print only zones
```

This is a test of the treatment of the diffuse fields, their transfer, and their effects on the ionization stucture of a nebula. The comparison is made against the exact calculation published by Van Blerkom and Hummer (1967). The geometry is open, that is, similar to that assumed in most BLR calculations.

- Neutral fraction at illuminated face 5.8×10^{-4} .
- Location of ionization front at 7.8×10^{16} cm.
- "TOTL 4861" and "ca b 4861" agree; both slightly lower than "Q(H) 4861".

```
title test hydrogen atom emissivity
black 5
ionization parameter -2
sphere static
                         ;want full outward flux
constant temperature 4
abundances -10
                         ;pure hydrogen
hden 7
                         ;suppress two-photon emission
stop eden 6
                         ;stop model at H ionization front
print short
hydrogen collisions off
                         ;make sure no collisional excitation
punch emitted continuum ;output the predicted continuum
```

This checks that the predicted hydrogen continuum is in good agreement with exact results in the optically thin nebular limit. It was used to generate Figure 9 in HAZY. Checks:

• Continuum relative to $H\beta$ should agree with Ferland (1980) filter averaged results.

```
title test of equations of motion in a wind
c test of wind code
c radiative acceleration (e- only) is 9.54E-7 cm s^-2
c terminal velocity (e- only) is 7.68 km s^-1
hden 4
table agn
luminosiy (total) 45
radius (parsecs) 1
stop thickness (parsecs) -1
no radiation pressure
wind 0.1
constant temperature 8
print only zones
```

This tests the management of the radiative acceleration of an electron scattering wind, and the resulting velocity. The parameters were chosen so that electron scattering is the dominant opacity source, so that the equations can be solved both numerically (in the example) and analytically (the expected solution given above). The actual acceleration is slightly below that due to Thomson scattering alone because the gas opacity at high energies is slightly below Thomson.

Checks:

• Terminal velocity should be ~ 7.68 cm s⁻¹.

298

```
title map of heating vs cooling
hden 0
table agn
ionization parameter -2.5
plot map
stop zone 1
print short
```

This is a test of the continuity of the code over a very large range of temperature. It was used to produce the thermal map shown in HAZY (Figure 3).

Checks:

• No breaks in heating-cooling curves where various approximations change.

25.2 Nebulae

The following examples establish "standard" models, useful to check whether (and how) the predictions of the code change with time.

```
title final F+P BLR model table 3
abundances osolar
stop column density 25.5
iterate 3 times
print last
ionization parameter -0.5
hden 9.5
table agn
plot continuum
stop zone 400
```

This calculation was presented by Ferland and Persson (1989). The differences between the present predictions and those given by FP are largely due to improved treatment of Balmer line escape and destruction. The cloud is quite thick, so that the default number of zones must be increased.

300

title "conventional" BLR model constant pressure ionization parameter -2 stop column density 23 table agn print last iteration iterate hden 9.5

This is an example of a "conventional" BLR calculation. Notice that the $Ly\alpha/H\beta$ ratio is much larger than observed.

```
title Kwan+Krolick Ap.J. 250, 478 BLR model
constant gas pressure
f(nu) -7.32148
abundances he-1 c-3.699 n-4 o-3.1549 ne-4 mg-4.5229
continue al-10 si-4.4229 s-10 ar-10 ca-10 fe-4.5229
stop column density 23
interpolate (0 -5) (.05 -5) (.1 0) (1 -0.5) (7.353 -2.233)
continue (735 -3.233) (800 -015) (8,000,000 -15)
print last iteration
normalise 1216 100
iterate
plot continuum -3
hden 9.60206
```

This is the "standard" BLR model presented by Kwan and Krolick (1981).

302

```
title (roughly) Ferland et al. DQ Her model
c model of ice cold ionized cloud arund old nova DQ Her
c roughly that of Ferland et al. 1984 Ap.J. 281, 194.
c tests behaviour of code at very low temperatures
stop temp = 100
c flat continuum, followed by nu<sup>-2</sup> power law
interpolate (0, 0) (0.3, 0) (8,000,000 -14.8)
luminosity 34
hden = 2.
filling factor 0.667
covering factor 0.667
radius 16.5682, thickness=16.14613
abundances 2 20 200 50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
grains
iterate
faint .05
print last
```

This is a test of the behaviour of the code in the extreme limit posed by the nebula surrounding DQ Her. A first cut at this model was published by Ferland et al. (1984).

```
title Ly alpha forest
c ionized by AGN power law plus cosmic background
background, z=2 ;this includes thermal and AGN background
double ; mimic two-sided photoionization
hden -2
stop neutral column density 15
metals -1.5 ;reduce all heavy elements by 1.5 dex
faint -1
iterate ; must iterate since optically thin
print last
```

This example demonstrates the behaviour of the code in the low density limit. The ionizing source is the cosmic background at a redshift of z = 2. The cloud is assumed to be optically thin to ionizing radiation, in keeping with the Gunn-Peterson test, so the "DOUBLE" command is included, and an iteration is performed.

```
title interstellar cloud irradiated by ism background
table ism
extinguish by a column of 22
cosmic rays, background
hden 0
abundances hii region ;this turns on Orion grains by default
grains ism ;this over rides above default, forcing ism grains
sphere ;set this since matter in all directions
stop temperature linear 10
stop thickness 0.1 linear parsecs
iterate
print last
faint .1
```

This is a test of the behaviour of the code in the extreme of photoionization by a relatively hard continuum, at low densities. The continuum is the galactic background, attenuated by a column density of 10^{22} cm⁻². This example checks whether the ionization balance, thermal balance, and electron density sum, are performed correctly in this limit.

```
title conditions similar to Orion nebula blister
sphere
table star kurucz 39,700K
phi(h) 13.0
turbulence 8 km/sec
hden 4
abundances hii region
constant pressure
iterate
print last iteration
```

This is a model similar in spirit to the blister geometry HII region model commputed by Baldwin et al. (1991). Orion grains are turned on with the abundances command. The constant pressure command does a hydrostatic equilibrium structure.

306

```
title liner model
c a constant pressure (gas+radiation) model of a liner cloud
c in the spirit of Ferland and Netzer 83
table agn
metals 0.3
constant pressure
iterate ;must iterate to get radiation pressure correctly
hden 6
stop column density 23
ionization parameter -3
print last
```

This is a model somewhat like the Liner parameters proposed by Ferland and Netzer (1983). A second iteration is performed to allow the calculation of the line radiation pressure.

```
title "New" Paris meeting Planetary nebula
c recompute "standard" PN model of the Pequignot Meudon Conferance
sphere
black body, T=150,000K radius = 10
hden = 3.4771213
radius = 17
abund -1 C-3.523 N-4. O-3.222 ne-3.824 mg-4.523 al=-7
continue si-4.523 s-4.824 ar-9 ca=-7 fe-7
plot continuum 0.1
```

This is one of the "standard" models computed at the Paris meeting on photoionization and shock calculations. Table 20 compares the predictions of the current version of CLOUDY with predictions of a few of the other codes.

```
title "New" Paris meeting HII region
c "standard" HII region model of the Pequignot Meudon Conferance
sphere
black body, T=40,000K radius = 12.113943
hden = 2
radius = 18.477121
abund -1 C-3.6576 N-4.39794 O-3.481146 ne-4.30103 mg-8 al=-8
continue si-8 s-5.04576 ar-8 ca=-8 fe-8
plot continuum .1
iterate ; must iterate since fine structure lines optically thick
print last
```

This is one of the "standard" models computed at the Paris meeting on photoionization and shock calculations. Table 22 compares the predictions of the current version of CLOUDY with predictions of a few of the other codes. It is necessary to iterate since some fine structure lines are optically thick.

```
title paris meeting NLR model
interpolate (0 -10) (0.073 -10) (0.074 1) (7352 -4)
continue (7400 -15) (7,353,000 -20)
stop lyman continuum optical depth 4
hden 3
abund -1 C-3.5229 N-4. O-3.22185 ne-3.82391 mg-4.5229 al=-8
continue si-4.5229 s-4.82391 ar-8 ca=-8 fe-7
ionization parameter -2
```

This is the NLR model presented in the Meudon meeting on model nebulae.

```
title test of optimization driver
optimize intensity -1 ;want H-bet flux of .1 erg cm^-2 s^-1
*
optimize column density ;read in sets of desired column densities
hydrogen 2 21.3
end of column dens
*
optimize lines ; read in sets of desired relative line intensities
0 3 5007 3.1415
end of lines
*
hden 3 vary ;vary the density, ionization parameter, and bb temp
black 5 vary
ionizat -2 vary
```

Vary three parameters to try to reproduce a desired H β intensity, ionized hydrogen column density, and 5007/H β intensity ratio.

26 **REFERENCES**

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27 GLOSSARY OF SYMBOLS

As far as possible, the notation used by HAZY follows standard texts (Osterbrock 1988; Mihalas 1978). This is a summary of some of the symbols used.

Symbol	Description	Units	Page
А	radiative rate	s^{-1}	
\mathbf{b}_n	departure coefficient	-	
С	collisional rate	s^{-1}	
D_{ul}	line destruction probability	-	
f(r)	filling factor	-	
\mathbf{g}_i	statistical weight	-	
G	energy gains, heating	${ m erg}~{ m cm}^3~{ m s}^{-1}$	
Ι	intensity	$\mathrm{erg} \mathrm{s}^{-1} \mathrm{sr}^{-1}$	
J	mean intensity	$erg s^{-1} sr^{-1}$	
N(cr)	cosmic ray density	cm^{-3}	
q	collisional rate coefficient	$\mathrm{cm}^3~\mathrm{s}^{-1}$	
$\dot{P}^*(x)$	LTE relative population	cm^3	
\mathbf{P}_{ul}	line escape probability	-	
P _c	continuum escape probability	-	
T_{u}	energy density temperature	Κ	
T_{color}	color temperature	Κ	
U_g	grain potential	volt	
${ m Q}^{'}_{abs}$	grain absorption efficiency	-	
Q(H)	hydrogen ionizing photons	s^{-1}	
v	velocity	${ m cm~s^{-1}}$	
V_g	grain potential	eV	
$\alpha(T)$	recombination coefficient	$\mathrm{cm}^3~\mathrm{s}^{-1}$	
α_{ν}	continuous absorption cross section	cm^{-2}	
α_{lu}	line absorption cross section	cm^{-2}	
β^{i}	recombination cooling coef	$\mathrm{cm}^3~\mathrm{s}^{-1}$	
η	photon occupation number	_	
$\dot{\gamma}$	one sided escape probability		
Γ	photoionization rate	s^{-1}	
κ	opacity	cm^{-1}	
Λ	energy loss, cooling	$erg \text{ cm}^3 \text{ s}^{-1}$	
ϕ	photon flux	cm^{-2} s ⁻¹	
σ^{φ}	scattering cross section	cm^{-2}	
Σ	projected grain area	cm^2	
τ	optical depth	-	
ν	frequency	Ηz	

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28 SAMPLE OUTPUT

Tests were computed with the Ohio Supercomputer CRAY Y-MP, a micro-VAX II, a SUN Sparcstation, and a Northgate 486, with essentially identical results. Tests were also computed on a Decstation 3100, and the results were similar but not identical. The following output is from models computed on the Cray.

CLOUDY 80.08

*		ł
* ti	itle final F+P BLR model table 3	1
* st	top column density 25.5	1
* it	terate 3 times	1
* pi	rint last	3
* io	onization parameter -0.5	1
* ho	den 9.5	1
* ta	able agn	1
* p]	lot continuum	1
* st	top zone 400	1
* с	blr.in	1
* с	cray	1
*	-	1

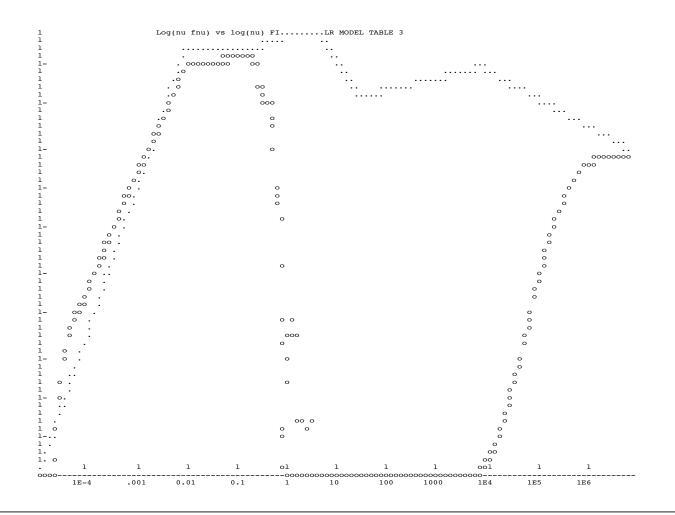
Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

546Cell Peak1.78E+00	Lo 1.00E-05=0.9101cm	Hi-Con:7.34E+06 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>lryd): 9.2980	Average nu:3.038E+00	P(X-ray): 8.4693	P(BalC): 8.8023	Q(Balmer C): 19.7651
Q(1.0-1.8): 19.1738	Q(1.8-4.0): 19.0661	Q(4.0-20): 18.5287	Q(20): 16.7913	Ion pht flx:3.001E+19
L(gam ray): 8.2078	Q(gam ray): 14.6227	L(Infred): 9.0163	Alf(ox): -1.4120	Total lumin: 9.5633
U(1.0):3.165E-01	U(4.0):3.628E-02	T(En-Den):2.004E+03	T(Comp):1.327E+07	nuJnu(912A):6.342E+08
Occ(FarIR):5.638E+01	Occ(H n=6):2.126E-02	Occ(1Ryd):2.924E-08	Occ(4R):1.499E-10	Occ (Nu-hi):2.089E-38
Tbr(FarIR):9.380E+01	Tbr(H n=6):9.439E+01	Tbr(1Ryd):4.619E-03	Tbr(4R):9.484E-05	Tbr (Nu-hi):2.306E-26

1 Te:2.208E+04 Hden:3.162E+09 Ne:3.806E+09 R:1.000E+25 R-R0:1.432E+08 dR:2.864E+08 NTR: 1 Htot:7.009E-05 T912: 5.368E-05###
2.25 4686 1.72 5876 0.00 1909 0.06 1549 38.66 6584 0.00 2326 0.00 3727 0.00 6300 0.00 2798 0.00 1035 39.16
Hvdrogen 9.416E-06 1.000E+00 H+0/Hden: 1.000E+00 1.474E-17 H- H2 7.808E-17 2.386E-14 H2+ HeH+ 2.470E-17 H col den 9.057E+17
H 2SP 3-6 6.402E-11 1.125E-11 8.395E-12 1.127E-11 1.588E-11 2.138E-11 Texc(La): 8.028E+03 T(contn): 2.004E+03 T(diffs): 8.404E+03
Helium 2.312E-08 1.768E-03 9.982E-01 He I 2S3 1.646E-09 Comp H, C 7.872E-08 1.310E-10 Fill Fact 1.000E+00 Gam 1/tot 9.095E-01
He singlet 2.147E-08 1.552E-13 1.984E-15 2.827E-15 4.203E-15 6.210E-15 He triplt 1.645E-09 9.014E-13 8.930E-15 2.479E-14 6.279E-15
HeII 1.768E-03 9.584E-10 4.051E-12 5.586E-12 8.030E-12 1.137E-11 9.559E-11 1.242E-09 1.614E-07 PRAD/GAS; 1.675E-02
Pressure NgasTgas; 1.610E+14 P(total): 2.261E-02 P(gas): 2.223E-02 P(Radtn): 3.724E-04 Rad accel 1.624E+00 Force Mul 3.918E+01
Carbon 0.000E+00 5.256E-07 9.219E-04 1.096E-01 7.964E-01 9.143E-02 1.636E-03 H2O+/Otot 0.000E+00 OH+/Ototl 0.000E+00
Nitrogen 0.000E+00 0.000E+00 1.458E-04 1.629E-02 1.961E-01 7.591E-01 2.825E-02 2.031E-04 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 0.000E+00 0.000E+00 1.150E-04 1.820E-02 1.858E-01 4.472E-01 3.471E-01 1.652E-03 0.000E+00 Hex(tot): 0.000E+00 A:-12.803
Neon 0.000E+00 0.000E+00 7.219E-05 1.204E-02 2.898E-01 6.226E-01 6.442E-02 9.901E-03 1.080E-03 0.000E+00 0.000E+00
Magnesium 0 0.000E+00 0.000E+00 1.845E-05 1.715E-03 2.367E-02 2.785E-01 5.064E-01 1.718E-01 1.677E-02 1.044E-03 4.213E-05 0.000E+00
Aluminium 0 0.000E+00 1.104E-07 2.641E-05 1.658E-03 1.867E-02 2.094E-01 5.099E-01 2.349E-01 2.428E-02 1.143E-03 4.154E-05 0.000E+00
Silicon 0 0.000E+00 0.000E+00 1.424E-05 1.038E-03 1.504E-02 1.625E-01 4.295E-01 3.213E-01 6.590E-02 4.456E-03 1.746E-04 0.000E+00
Sulphur 1 0.000E+00 2.300E-05 8.290E-04 7.498E-03 1.163E-01 4.269E-01 3.250E-01 1.083E-01 1.423E-02 8.465E-04 3.019E-05 7.951E-07
Argon 3 7.265E-04 1.620E-02 5.076E-02 2.499E-01 3.382E-01 2.932E-01 4.648E-02 4.368E-03 1.713E-04 4.042E-06 8.701E-08 1.511E-09
Calcium 0 0.000E+00 0.000E+00 2.241E-07 2.198E-05 4.989E-04 1.786E-02 1.640E-01 4.137E-01 3.018E-01 7.991E-02 2.107E-02 1.114E-03
Iron 1 0.000E+00 0.000E+00 0.000E+00 3.544E-05 4.726E-03 9.636E-02 5.009E-01 2.704E-01 1.050E-01 1.997E-02 2.408E-03 2.312E-04
######307 Te:4.954E+03 Hden:3.162E+09 Ne:7.727E+07 R:1.000E+25 R-R0:9.969E+15 dR:6.273E+13 NTR: 8 Htot:6.272E-09 T912: 1.813E+08###
7.26 4686 0.12 5876 0.22 1909 4.19 1549 10.83 6584 0.00 2326 0.07 3727 0.00 6300 0.09 2798 0.44 1035 1.63
Hydrogen 9.761E-01 2.385E-02 H+0/Hden: 1.000E+00 4.788E-11 H- H2 1.702E-07 2.993E-08 H2+ HeH+ 3.996E-09 H col den 3.162E+25
H 2SP 3-6 1.746E-07 5.238E-07 1.226E-08 3.143E-09 1.083E-09 5.073E-10 Texc(La); 6.138E+03 T(contn): 1.101E+03 T(diffs): 1.086E+03
Helium 9.974E-01 2.605E-03 0.000E+00 He I 2S3 8.584E-09 Comp H, C 1.853E-12 5.844E-14 Fill Fact 1.000E+00 Gam 1/tot 2.512E-02
He singlet 9.974E-01 3.757E-13 1.411E-15 4.922E-16 6.132E-16 8.212E-16 He triplt 8.310E-09 2.680E-10 5.488E-12 2.223E-14 1.152E-12
HeII 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 PRAD/GAS; 2.156E-03
Pressure NgasTgas; 1.893E+13 P(total): 2.960E-03 P(gas): 2.614E-03 P(Radtn): 3.467E-04 Rad accel 8.999E-05 Force Mul 1.171E+00
Carbon 5.329E-01 4.671E-01 3.909E-06 0.000E+00 0.000E+000E+
Nitrogen 9.825E-01 1.752E-02 2.146E-10 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/Otot1: 0.000E+00 02/Otot1: 0.000E+00 02/Otot1: 0.000E+00
Oxygen 9.792E-01 2.077E-02 3.439E-10 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.555

Neon 9.992E-01 8.319E-04 7.708E-08 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Magnesium 0 8.144E-03 9.918E-01 4.256E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Aluminium 0 7.461E-05 9.999E-01 7.036E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Silicon 0 1.876E-03 9.981E-01 1.734E-05 0.000E+00	
Sulphur 0 2.982E-04 9.996E-01 6.820E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Argon 0 9.989E-01 1.140E-03 2.484E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Calcium 0 3.856E-04 1.057E-01 8.939E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Iron 0 8.951E-02 9.104E-01 1.065E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00	
Calculation stopped because column dens reached.	
Geometry is plane-parallel.	
FeII-MgII photoionization of H N=2 reached 83.3 percent of the total rate out.	
Photoionization of He 2Tris reached 94.6 percent of the total rate out.	
!The largest continuum occupation number was 5.638E+01 at 1.054E-05 Ryd.	
The largest continuum brightness temperature was 2.683E+03K at 8.642E-03 Ryd.	
Hydrogen self ionization by alpha transitions reached 12.8% of the destruction rate for level 4.	
Some excited state HeI lines are thick.	
Some excited state HeII lines are thick.	
Some fine structines are optically thick, largest=7.12E+02	
Continuum occupation number reached 4.09E+02 for some fine structure transitions.	
Some fine structure lines were a heat source.	
Induced recombination was 11.4% of the total for H level 6	
Stimulated emission was 80.8% of the total for H transition 7 - 6	
Timeracule-photoerosion of Fe=8.17E+06yr	
Free-free heating was 1.6% of the total.	
C-Free-Free heating significant and frequency out of range of gaunt factor routine.	
H - absorption heating was 2.3% of the total.	
Balmer continuum optical depth is 9.96E+00	
Balmer continuum stimulated emission correction to optical depths reached 0.16	
Paschen cont optical depth= 1.06E+00	
Continuum optical depth at low nu (1.054E-05 Ryd) was 1.752E+05	
The optical depth to Rayleigh scattering at 1300A is 1.93E+02	
The optical depth to the H2+ molecular ion is 4.68E+00	
Optical depth to negative hydrogen ion is 9.69E-02	
The ratio of radiation to gas pressure reached 2.48E+00. Caused by Lyman alpha.	
C-Model thick to e-scat; tau= 1.90E+00	

C-Model thick to e-scat; tau= 1.90E+00 C-This is the last iteration and H(a) optical depth changed by 11.1% (was 5.18E+05). Try another iteration Line radiation pressure capped by thermalization length.



Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 3 of 3. Intensity (erg/s/cm^2)

Intensity (erg/s/cm ²)												
TOTL 4861	7.257 1	.0000 H	leat187	1 5.10	0 0.0070	N 2	4239	4.229	0.0009	PHOT 1895	4.915	0.0046
TOTL 1216			rst	0 6.73			5680	4.750	0.0031	Si 4 1397	7.252	0.9900
TotH 0			I-FB	0 7.42			2140	5.578	0.0210	Si 6 19	4.804	0.0035
BFH1 0	8.571 20	.6380 H	12+	0 7.13	6 0.7229	N 2	1084	3.659	0.0003	Si 7 2148	5.219	0.0092
BFHx 0	8.210 8	.9850 н	IEH+	0 4.52	6 0.0019	N 3	1750	7.156	0.7934	Si 7 25	4.525	0.0019
BFHe 0	8.227 9	.3361 H	leFF	0 7.07	7 0.6613	N 3	990	5.469	0.0163	Si 8 1446	4.085	0.0007
TotM 0	8.288 10	.7512 H	leFB	0 7.19	2 0.8616	N 4	1486	6.949	0.4927	Si 9 1985	4.110	0.0007
FF H 0	7.286 1	.0711 M	leFB	0 5.99	0 0.0542	N 4	765	5.066	0.0064	S 1R 1807	5.035	0.0060
ComH 0			leFF	0 6.18			1718	4.586	0.0021	S 2 6720	4.570	0.0021
н-н 0			OFF	0 8.38			1240	7.008	0.5641	S 2 4074	6.017	0.0576
pair 0			esc 51			N 7r		3.381	0.0001	S 210330	5.818	0.0364
CA B 4861			le I 50				6300	6.226	0.0932	S II 6731	4.412	0.0014
CA B 1216	9.977 524		le I 44'				6363	5.749	0.0311	S II 6716	4.054	0.0006
DU B 4861			OTL 58				5577	5.853	0.0395	S II 4070	5.937	0.0479
Q(H) 4861			a B 58'				7774	5.716	0.0288	S II 4078	5.246	0.0098
Q(H) 1216			OTL108				8446	5.801	0.0350	S II10323	5.434	0.0150
TOTL 6563			NWD108				1304	6.694	0.2736	S II10289	5.305	0.0112
TOTL 4861			OTL 38			6lev		3.686	0.0003	S II10373	4.776	0.0033
TOTL 4340			OTL 70			6lev		5.885	0.0425	S II10339	5.096	0.0069
TOTL 4102 TOTL18751			CHE	0 6.09			3727 7325	3.347	0.0001	S 3 9532 S 3 9069	3.875 3.459	0.0004
TOTL18751 TOTL12818			le I	2 6.1				4.705	0.0028			0.0002
TOTL12818 TOTL10938			evB Ie I 50				2471 7323	4.617	0.0023	S 3 6312 S 3 3722	4.095 3.866	0.0007
TOTL40512			evB 50				7332	4.342	0.0012	S 3 1198	4.689	0.0027
TOTL26252			еvв 30. Ie I 390				4651	5.440	0.0153	S 3 1729	5.192	0.002/
TOTL74578			evB 390				1663	7.413	1.4334	S 4 105	3.482	0.0002
2 NU 0			Ie I 36				1663	3.413	0.0001	S 4 1406	6.439	0.1524
TOTL 1216			evB 36			Rec	1663	5.810	0.0357	S 5 1198	5.519	0.0183
TOTL 1026			le I 344				5007	5.659	0.0253	S 5 786	3.908	0.0004
TOTL 973			evB 344				4959	5.182	0.0084	S 6 933	5.637	0.0240
TOTL 950			IeII 22				5007	4.824	0.0037	S 9 1715	3.970	0.0005
TOTL 938	5.572 0	.0207 E	ISC 3	4 6.38	8 0.1354	TOTL	4363	5.896	0.0436	Ar 3 7135	3.941	0.0005
LA X 1216	7.622 2	.3220 H	le2C 9	1 6.6	2 0.2604	0 3	2321	5.269	0.0103	Ar 3 7751	3.311	0.0001
Ind2 1216	4.782 0	.0034 т	TOTL 164	0 7.24	7 0.9787	O 3	834	5.935	0.0477	Ar 4 4740	3.485	0.0002
C13c 6563	3.934 0	.0005 T	COTL 46	6 6.33		O 3	3341	4.402	0.0014	Ar 4 7335	4.507	0.0018
C13h 6563	4.899 0	.0044 т	TOTL 12	6 6.69		O 4	1402	6.791	0.3423	Ca 2 3933	6.408	0.1419
C14h 4861			a B 164				1401	5.140	0.0076	Ca 2 8579	6.814	0.3609
CION 0			evB 164			O 4	789	5.971	0.0518	Ca 2 7306	6.212	0.0903
INWD 1216			Ca B 46			O 4		4.768	0.0032	Phot 7306	5.185	0.0085
INWD 6563	7.475 1	.6550 D	evB 46	6 6.15	3 0.0788	O 5	630	5.870	0.0410	Ca2K 3934	6.112	0.0717

FINAL F+P BLR MODEL TABLE 3								
Cooling: CION 0:0.224 H FF 0:0.187 H FB 0:0.166 TOTL 1909:0.062 C 4 1549:0.160 Heating: BFH1 0:0.306 BFHx 0:0.133 BFHe 0:0.139 TotM 0:0.160								
IONIZE PARMET: U(1-) -0.4996 U(4-): -1.4403 U(sp): -0.50 Q(ion): 10.707 L(ion): 6.205 Q(low): 20.82 P(low) 8.52 ENERGY BUDGET: Heat: 9.085 Coolg: 9.087 Error: 0.5% Compt H: 7.071 WorkF: 11.742 F-F H 7.286 PRADMX:2.48E+00 Column density H12:3.162E+25 H II:2.821E+24 HI:2.880E+25 H-: 2.487E+15 H2: 3.009E+18 H2+:6.693E+17 He H+:7.380E+16 OH: 0.000E+00 Heff:3.367E+25								
<nh>:3.162E+09 <tp>:5.78E+03 <t03>:1.31E+04 Ne:3.484E+09 ti(snd):1.62E+10 NeN+dl:1.59E+33 <t(c3)>:1.27E+04 <e(c3)>:3.47E+09 He/Ha:1.69E-01 = 1.72*true N/0ap:0.00E+00 = 0.00true T(03):1.00E+01 L THN:3.14E-03 <t(s2)>:5.48E+03 <e(s2)>:2.71E+08 T He+:1.06E+04 EHe+:2.43E+09 T(0+):5.40E+03 EO+:4.26E+08 iter/zn: 2.287 Te-low:4.30E+03 Te-light:2.21E+04 Hlu/zn:3.07E+00 <a>:0.00E+00 erdeFe2.5E+14 Tcompt1:01E-07 Tthr3.32E+02 <tden>: 5.51E+03 <den>:7.45E-15 <mol>:1.20E+00 Mean Jeans l(cm)4.79E+16 M(sun)2.16E+02 smallest: len(cm):4.54E+16 M(sun):1.84E+02 Alf(ox-tran): -244.3771</mol></den></tden></e(s2)></t(s2)></e(c3)></t(c3)></t03></tp></nh>								
Optical Depths: CONTN; COMP: 1.90E+00 H-: 9.69E-02 R(1300): 1.93E+02 H2+ 4.68E+00 HeTri:6.54E+00 Pfa:1.93E+00 Pa:2.05E+00 Ba:2.52E+00 Hb:2.22E+00 La:4.80E+03 1r:1.813E+08 1.8:5.83E+07 4.:9.077E+06 21R:1.043E+05 10830: 3.18E+04 3889: 1.39E+03 5876: 1.68E+03 7065: 9.24E+02								
1550: 1.24E+06 2800: 2.21E+09 774: 1.45E+02 1240: 1.52E+04 1035: 8.93E+04 1335: 1.21E+09 977: 9.62E+06 1397: 8.41E+05 789: 1.31E+05 1207: 1.04E+06 1085: 1.66E+07 1194: 3.15E+03 1909: 3.83E+00 1895: 2.78E+01 2326: 6.03E+02 1666: 3.54E+01 1750: 1.46E-01 1025: 3.03E+08 352: 1.03E+02 347: 1.00E-20 1860: 8.38E+04 630: 2.52E+05 834: 4.62E+08 835: 1.72E+06 1808: 1.92E+09 1256: 3.04E+07 -3: 9.79E+07 -48: 4.65E+02 3934: 2.25E+07 3969: 1.14E+07 8498: 3.39E+04 8542: 3.02E+05 8662: 1.72E+05 353: 1.48E+01 1364: 1.04E+09 1822: 9.94E+05 1600: 1.72E+00 1241: 1.36E+01 1656: 7.0E+00 1232: 9.94E+04 920: 6.22E+05 1402: 1.74E+00 1241: 1.74E+00 1241: <								
C157: 5.57E+01 N122: 3.95E+00 N205: 5.35E+00 N57: 7.48E-02 O146: 2.36E+02 O63: 7.12E+02 O88: 4.54E-01 O52: 7.62E-01 O26: 7.32E-02 NE13: 4.07E-01 NE36: 1.76E-01 NE16: 5.47E-01 MG4: 3.29E-03 MG14: 1.73E-03 MG6: 1.02E-03 S135: 6.49E+01 S19: 2.81E-02 S34: 1.33E-02 S11: 7.34E-02 AR7: 4.49E-02 AR9: 1.04E-02 AR2: 3.04E-03 AR13: 1.27E-04 AR8: 4.24E-04 CA3: 9.79E-03 CA12: 4.23E-05 CA4: 1.78E-04 Ne14: 8.67E-03 Ne24: 4.28E-03 Si3: 1.55E-03 Si4: 1.47E-02 Fe7: 3.32E-06 Fe61:-1.72E-01 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 3.35E-03 Si6.5: 1.01E-03 C610: 8.57E+00 C370: 5.96E+00								
Old hydro optical depths: 1 1.81E+08 2 9.43E+00 3 1.06E+00 4 5.67E-01 5 2.90E-01 6 1.51E-01 7 1.49E-01 Lines: 2-1 2.26E+12 3-2 5.18E+05 4-3 8.07E+04 5-4 7.50E+04 6-5 6.02E+04 7-6 4.90E+03 8-7 5.84E+03 New hydro optical depths: 1 1.81E+08 2 9.96E+00 3 1.06E+00 4 5.17E-01 5 2.60E-10 6 1.35E-01 7 1.38E-01 Lines: 2-1 2.30E+12 3-2 4.61E+05 4-3 8.05E+04 5-4 7.14E+04 6-5 5.77E+04 7-6 4.73E+03 8-7 5.92E+03								
Old He Is optical depths: 1 5.87E+07 2 4.67E+00 3 2.01E-07 4-1.02E-07 5-2.71E-07 6-4.64E-07 7-4.03E-06 Lines: 2-1 1.53E+11 3-2 3.49E+00 4-3 1.57E-01 5-4 4.59E-02 6-5-1.41E-02 7-6 1.86E-01 8-7 2.78E+00 New HE Is optical depths: 1 5.83E+07 2 4.11E+00 3 2.45E-07 4-1.09E-07 5-2.95E-07 6-5.07E-07 7-4.38E-06								
Lines: 2-1 1.57E+11 3-2 3.98E+00 4-3 1.87E-01 5-4 5.38E-02 6-5-1.27E-02 7-6 2.05E-01 8-7 3.07E+00								
Old He II optical depths: 1 9.11E+06 2 1.82E+08 3 2.43E-07 4-1.96E-08 5-4.47E-08 6-7.72E-08 7-7.59E-07 Lines: 2-1 2.51E+08 3-2 8.04E+01 4-3 3.49E-02 5-4 8.09E-04 6-5-3.67E-04 7-6 3.32E-03 8-7 4.93E-02 New HE II optical depths: 1 9.08E+06 2 1.81E+08 3-2 8.80E+07 4-1.94E-08 5-4.47E-08 6-7.74E-08 7-7.60E-07 Lines: 2-1 3.35E+08 3-2 8.83E+01 4-3 4.01E-02 5-4 8.73E-04 6-5-3.26E-04 7-6 3.34E-03 8-7 4.96E-02								
Hydrogen -0.041 -1.050 Log10 Mean Ionisation (over volume) Helium -0.003 -2.208 -3.637								
Carbon -0.375 -0.241 -2.509 -2.963 -3.807 -5.006 -6.944 Nitrogen -0.062 -0.894 -2.513 -2.987 -4.143 -3.876 -5.571 -7.850 Oxygen -0.036 -1.123 -2.428 -3.670 -4.067 -4.112 -4.486 -6.964 Neon -0.002 -2.985 -2.407 -4.533 -3.936 -4.046 -5.244 -6.055 -7.108 Magnesium -2.322 -0.016 -1.513 -4.478 -4.514 -4.050 -4.086 -4.729 -5.822 -7.050 -8.525 Aluminum -4.397 -0.002 -3.054 -2.483 -4.446 -4.067 -4.040 -4.573 -5.683 -7.043 -8.554								
Silicon -2.708 -0.003 -3.143 -2.732 -2.776 -3.998 -4.029 -4.395 -5.247 -6.503 -7.940 Sulphur -3.268 -0.002 -2.987 -2.575 -3.256 -4.126 -3.965 -4.341 -4.999 -6.012 -7.315 -8.867-13.643 Argon -0.003 -2.841 -3.945 -4.222 -4.222 -4.298 -4.498 -5.451 -6.596 -8.087-12.393-14.603-16.364 Calcium -3.642 -0.866 -0.064 -3.100 -4.783 -4.125 -4.142 -4.504 -5.184 -5.855 -7.206 Iron -1.166 -0.033 -3.045 -4.613 -4.388 -4.182 -3.993 -4.512 -5.829 -6.801 -7.862								

INWD 4861	7.234	0.9504	REC 1656	6.757	0.3164	TOTL 1218	7.204	0.8867	Ca2H 3969	6.103	0.0702
INWD18751	6.342	0.1218	C I 9850	5.080	0.0067	0 5 1218	7.204	0.8866	Ca2X 8498	6.315	0.1143
Strk 1216	5.075	0.0066	C 1 8727	6.338	0.1205	0 5 5112	4.020	0.0006	Ca2Y 8542	6.364	0.1282
Strk 6563	6.771	0.3271	C 2 2326	6.117	0.0725	0 6 1035	7.469	1.6308	Ca2Z 8662	6.330	0.1185
Strk 4861	6.494	0.1729	INWD 2326	6.112	0.0716	Ne 3 156	3.520	0.0002	CaF1 7291	5.958	0.0503
Strk18751	5.853	0.0395	Phot 2326	6.280	0.1057	Ne 3 3869	5.680	0.0265	CaF2 7324	5.859	0.0400
Strk40512	4.913	0.0045	C 2 1335	5.294	0.0109	Ne 3 3968	5.167	0.0081	Rec 3933	4.989	0.0054
Dest 1216	7.888	4.2801	REC 1335	6.776	0.3309	Ne 3 3343	4.834	0.0038	Ca 4 32	3.669	0.0003
Dest 6563	7.566	2.0399	C II 3134	3.590	0.0002	Ne 3 1815	4.973	0.0052	Fe 2 48	7.141	0.7656
Dest40516	4.222	0.0009	C 2 4267	5.087	0.0068	Ne 4 4720	3.486	0.0002	Fe 2 7	7.141	0.7668
Dest 4861	7.025	0.5871	TOTL 977	6.965	0.5112	Ne 4 1602	4.102	0.0007	Emis 3	6.261	0.1010
Dest18751	6.037	0.0603	C3 C 977	6.764	0.3218	Ne 5 3426	4.781	0.0033	Cool 3	7.154	0.7903
e-e+ 511	4.691	0.0027	C3 R 977	6.534	0.1894	Ne 5 3346	4.349	0.0012	TOT 0	7.507	1.7782
nFnu 4860	8.519	18.3131	TOTL 1909	7.879	4.1923	Ne 5 2976	3.956	0.0005	FEIR 0	4.941	0.0048
nFnu 1215	7.032	0.5958	INWD 1909	7.643	2.4355	Ne 5 1575	4.432	0.0015	Fe 3 0	4.577	0.0021
Inci 4861	8.459	15.9411	C 3 1907	4.335	0.0012	Ne 5 1134	5.754	0.0314	Fe 3 5270	3.897	0.0004
Inci 1216	8.740	30.4218	C 3 1909	7.879	4.1911	Ne 6 1007	5.465	0.0161	Fe 3 4658	4.141	0.0008
BA C 0	8.213	9.0540	C3 R 1909	6.119	0.0728	Ne 7 895	4.335	0.0012	Fe 3 1122	4.051	0.0006
PAC 0	8.227	9.3494	Phot 1909	5.994	0.0547	Ne 8 774	3.736	0.0003	Fe 6 0	4.069	0.0006
H FF 0	8.360	12.6948	C 3 2297	6.039	0.0606	Mg 1 4571	4.452	0.0016	Fe 6 5177	3.618	0.0002
ComC 0	3.838	0.0004	C 3 4187	4.184	0.0008	Emis 2798	6.899	0.4393	Fe 7 6087	4.101	0.0007
H FB 0	8.308	11.2629	C 3 4649	4.970	0.0052	Cool 2798	7.158	0.7979	Fe10 6374	5.202	0.0088
Hind 0	5.242	0.0097	C 4 1549	8.291	10.8298	Mg 5 2751	4.206	0.0009	Coll 6374	5.179	0.0084
Cool 1216	5.401	0.0139	INWD 1549	8.160	8.0027	Mg 6 1806	3.755	0.0003	Pump 6374	3.906	0.0004
Heat 1216	7.548	1.9581	DEST 1549	5.949	0.0493	Mg 7 2629	5.252	0.0099	Fell 7892	4.303	0.0011
Crst 960	3.638	0.0002	C4 r 1549	5.629	0.0236	Mg 8 3	3.464	0.0002	Coll 7892	4.256	0.0010
Hrst 960	3.420	0.0001	C 4 4659	3.979	0.0005	Al 3 1860	6.274	0.1040	Pump 7892	3.313	0.0001
Cool 6563	6.380	0.1327	C 6r 34	4.646	0.0025	Si 2 35	3.334	0.0001	Fell 2649	3.801	0.0004
Heat 6563	6.774	0.3292	N 1 5200	3.381	0.0001	Si 2 2335	5.758	0.0317	Fe12 2170	3.647	0.0002
Crst 4861	5.722	0.0292	N 2 6584	4.589	0.0021	Si 2 1808	4.583	0.0021	Totl 2	6.589	0.2150
Hrst 4861	5.163	0.0081	N 2 6548	4.112	0.0007	Si 3 1207	5.792	0.0343	AugC 2	6.589	0.2150
Cool18751	6.306	0.1122	N 2 5755	4.588	0.0021	Si 3 1895 361 Ar 2 7	6.963	0.5091			
Lines with nega	tive in	tensities;	205 T OI	0 255	Ne 2 128	361 Ar 2 7					

	1	2	3	4	5 6	5	7	8	9	10	11	12	13	14	15	16	17
Hydrogen	0 041	-1.050				To	~10 Mo:	an Ionis	ation	lover r	dina						
Helium		-2.208	-3 637			LOG	giu mea	in ionits	acion	(over ra	aurus)						
Carbon				-2.963 -	3.807 -5	5.006 -	-6.944										
Nitrogen	-0.062	-0.894	-2.513	-2.987 -	4.143 -3	8.876 -	-5.571	-7.850									
Oxygen	-0.036	-1.123	-2.428	-3.670 -	4.067 -4	.112 .	-4.486	-6.964									
Neon				-4.533 -													
Magnesium																	
Aluminum				-2.483 -													
Silicon Sulphur				-2.732 -								0 067	12 612				
Argon				-2.501 -										14 60	3-16 364		
Calcium				-3.100 -									-12.555	-14.00	5=10.504		
Iron				-2.403 -									-7.862				
0.5-1.0KE	EV:0.00E-	+00 1.0	-1.5:***	***** 1.	5-2.0:2.	89-61	8 2.0-2	2.5:2.37	-386 2	.5-3:1.6	56-254	3-5:5.4	3E-72 5-	-7.5:4	.61E+01	7.5-10:	1.60E-19
							Norr	nalised	contin	111m							
0.25 0.	114 0	.27 0.0	94 0.3	30 0.074	0.33 0	0.056		0.042	0.39		0.43 0	036	0.47 0.0	132	0.51 0.0	16 0.	56 0.002
0.62 0.		.67 0.0		74 0.000	0.81 0			0.000	0.97		0.98 0		0.99 0.0		1.00 0.0		50 01002
Inward co	ontinua	(nuFnu)	at head	d of Balm	ner, Lyma	in ser	ies; 5	5.59E+08	4.27	E+08							
Outwrd co	ntinua	(111 -	at bear	d of Balm	er Tuma	n cor	ioe ·	3 50E+07	0.00	F+00							
outwid co	meinuu	(nur nu)	ac neut	a or buin	ler, Dynic	in ser.	105, 1		0.00	1.00							
						Eme	rgent d	continuu	m - ph	ot/ryd/d	m2 (r :	in)					
	48E+19				0.00E+00		7.3 0.0			0.00E+0			4.85E-0		3.24E+05		
0.29 1.			.00E+00		0.00E+00		9.5 0.0			0.00E+0			2.02E+0		4.81E+05		
0.33 8.			.00E+00		0.00E+00		2.0 0.0			0.00E+0			1.15E+0		7.16E+05		
0.37 5.			.00E+00		0.00E+00 0.00E+00		4.8 0.0 7.9 0.0			1.53-157 5.25-136			1.75E+(1.97E+(1.06E+06 1.58E+06		
0.42 3.			.00E+00		0.00E+00		1.5 0.0			5.32-130			1.97E+0		1.58E+06 2.35E+06		
0.53 8.		1.57 2			0.00E+00		5.5 0.0			3.81-90			2.16E+0		3.49E+06		
0.60 1.		1.78 0			0.00E+00		0.0 0.0			5.31-73			3.49E+0		5.19E+06		
	63E+15				0.00E+00		5.0 0.0			5.50-65			8.41E+0				
0.76 2.	11E+09	2.25 2	.10E+09		0.00E+00		0.5 0.0	00E+00	173.9	7.94-38	37 4	46E+04	2.76E+0	02			
0.86 1.			.00E+00		0.00E+00		4.7 0.0			1.41-15		64E+04	1.04E+0	03			
0.97 0.			.00E+00		0.00E+00		9.3 0.0			1.02E-5			3.68E+0				
0.99 0.			.00E+00		0.00E+00		4.2 0.0			1.37E-3			1.05E+0				
0.99 0.	00E+00	3.63 0	.00E+00	15.4	0.00E+00	y 69	9.5 0.0	102+00	849.0	1.54E-1	LL 2.	.18E+05	2.22E+0	14			

CLOUDY 80.08

*******	*******	******91Aug03********	*****	******					
*				*					
	* title case A * c Seaton 1959 results; 4pi j(beta) 5.56E-26								
	*								
	nis model total H-beta=			*					
	3.73E-3 (3)=3.69E-2 (4)		.193	*					
	very different results			*					
	ced processes ;N.B. cas			*					
	n collisions off ; must	turn off all collisio	ns except 2s-2p	*					
	nan optical depth -6			*					
	temperature = 10,000K			*					
	eparture coefficients			*					
* stop zon				*					
	dy, T=50,000K			*					
	lon parameter -2			*					
	15; must be high to mix	2s, 2p		*					
* drmax 0				*					
* drmin 0				*					
* abundano				*					
* print sl				*					
* c casea	.in			*					
* c cray				*					
*				*					
******	**********	******	******	* * * * * * *					
	G	hemical composition							
He: 000 C:1.00E=10 N:1.00E=10 O			Si:1.00E=10 S:1.00E=10	0 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10					
	10002 10 1011002 10 1	g.1.002 10 111102 10							
333Cell Peak1.24E+00	Lo 1.00E-05=0.9105cm	Hi-Con:1.16E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV					
P(nu>1ryd): 12.9889	Average nu:1.491E+00	P(X-ray): 0.0000	P(BalC): 12.8421	Q(Balmer C): 23.7181					
Q(1.0-1.8): 23.3840	Q(1.8-4.0): 22.7615	Q(4.0-20): 20.3654	Q(20): 0.0000	Ion pht flx:3.001E+23					
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): 11.4994	Alf(ox): 0.0000	Total lumin: 13.2308					
U(1.0):1.001E-02	U(4.0):7.736E-06	T(En-Den):1.655E+04	T(Comp):4.787E+04	nuJnu(912A):1.157E+13					
Occ(FarIR):0.000E+00	Occ(H n=6):0.000E+00	Occ(1Ryd):0.000E+00	Occ(4R):0.000E+00	Occ (Nu-hi):0.000E+00					
Tbr(FarIR):0.000E+00	Tbr(H n=6):0.000E+00	Tbr(1Ryd):0.000E+00	Tbr(4R):0.000E+00	Tbr (Nu-hi):0.000E+00					
· · · · · · · · · · · · · · · · · · ·	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		, ,	,					
##### 1 Te:1.000E+04 Hden:1.000				Htot:2.455E+06 T912: 2.971E-06#					

////// 110	· · · · · · · · · · · · · · · · · · ·	,01,15 HG1515551,11 H			D of diction		100			
4.74 4686	0.00 5876 0.00 19	09 0.00 1549 0.00	6584 0.00	2326 0.00) 3727 0.0	00 6300 0.	00 2798 (0.00 1035	0.00	
Hydrogen	4.824E-04 9.995E-01	H+0/Hden: 1.000E+00	3.356E-11	Н- Н2	2.633E-13	6.132E-12	H2+ HeH+	1.216E-20	H col den	1.000E+15
Hydrogen	1.587E-04 1.000E+00	H+0/Hden: 1.000E+00	2.804E-01	н- н2	6.060E-02	H2+	1.474E+00	He H+	1.216E-20	
H 2SP 3-6	8.037E-08 2.409E-07	7.897E-07 1.598E-06	2.798E-06	4.433E-06	Texc(La);	1.363E+04	T(contn):	1.655E+04	T(diffs):	1.680E+03
H 2SP 3-6	3.749E-03 3.745E-03	3.667E-02 8.991E-02	1.438E-01	1.919E-01						
Helium	6.463E-03 9.918E-01	1.786E-03 He I 2S3	1.673E-05	Comp H, C	3.654E-01	7.633E-02	Fill Fact	1.000E+00	Gam 1/tot	9.964E-01
Helium	4.943E-08 5.004E-19	1.000E+00 He I 2S3	1.040E-01	Comp H, C	3.654E-01	7.633E-02	Fill Fact	1.000E+00	Gam 1/tot	9.964E-01
He singlet	6.427E-03 1.032E-06	3.532E-06 4.147E-06	4.760E-06	5.709E-06	He triplt	8.070E-06	6.754E-06	2.894E-07	7.535E-07	8.586E-07
He singlet	4.943E-08 4.849E-02	6.616E-01 9.414E-01	9.866E-01	9.965E-01	He triplt	1.040E-01	1.094E-01	1.076E-01	1.305E-01	9.635E-02
HeII	9.918E-01 1.835E-08	3 1.009E-07 2.310E-07	1.699E-07	1.381E-07	5.139E-07	2.371E-06	2.518E-04	PRAD/GAS;	1.048E-08	
HeII	5.004E-19 8.593E-07	1.360E-02 3.771E-01	7.350E-01	8.977E-01	9.945E-01	9.999E-01	1.000E+00	8.713E-07	PRAD/GAS;	1.048E-08
Pressure	NgasTgas; 2.000E+19	P(total): 2.761E+03	P(gas):	2.761E+03	P(Radtn):	2.892E-05	Rad accel	2.307E+05	Force Mul	1.015E+03
Carbon	8.757E-05 2.276E-01	7.701E-01 2.236E-03	0.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen	1.467E-04 2.981E-01	6.988E-01 2.893E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/Ototl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	1.712E-04 4.886E-01	5.105E-01 7.755E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.380
Neon	1.030E-03 6.812E-01	3.175E-01 1.866E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Magnesium 0	8.967E-04 2.409E-01	7.582E-01 1.640E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Aluminium 0	3.760E-04 4.799E-01	5.101E-01 9.568E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Silicon 0	7.157E-05 1.758E-01	8.101E-01 1.409E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

Sulphur	0 3.285E-05 1.707E-01	8.228E-01 6.464E-03	0.000E+00 0.	.000E+00 0.000E+	00 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00		
Argon	0 7.254E-05 3.459E-01	6.501E-01 3.966E-03	0.000E+00 0.	.000E+00 0.000E+	00 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00		
Calcium	0 1.318E-02 5.175E-01	4.687E-01 6.508E-04	0.000E+00 0.	.000E+00 0.000E+	00 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00		
Iron	0 3.546E-06 4.034E-02	6.679E-01 2.916E-01	2.118E-04 0.	.000E+00 0.000E+	00 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00		
Calculation stopped because optical depth reached											
Coomoty	Commetry is plane parallel										

Geometry is plane-parallel.
C-Density greater than 10**13 Photoinization of He 2Tris reached 4.1 percent of the total rate out.
W-A physical process has been disabled.
W-Heating - cooling mismatch = 1.19E+00 Whats wrong??? Frequency out of range of free-free gaunt factor routine. Continuum optical depth at low nu (1.053E-05 Ryd) was 5.952E+01

	* title case A *	
	* c Seaton 1959 results; 4pi j(beta) 5.56E-26 *	
	* c for this model total H-beta=4.745 *	
	* c b(2)=3.73E-3 (3)=3.69E-2 (4)=0.091 (5)=0.145 (6)=0.193 *	
	* c n.b. very different results if not 1-mixed *	
	* no induced processes ;N.B. case A is a fiction; no incuded transitions *	
	* hydrogen collisions off ; must turn off all collisions except 2s-2p *	
	* stop lyman optical depth -6 *	
	* constant temperature = 10,000K *	
	* print departure coefficients *	
	* stop zone 1 *	
	* black body, T=50,000K *	
	* ionization parameter -2 *	
	* hden = 15; must be high to mix 2s, 2p *	
	* drmax 0 *	
	* drmin 0 *	
	* abundances -10 *	
	* print short *	
	* c casea.in *	
	* c cray *	
	*********************************> LOG(U): -2.00 <***********************************	
	>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
	Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 1 of 1.	
	Intensity (erg/s/cm^2)	
	4.740 1.0000 Q(H) 1216 12.688******* TOTL74578 3.082 0.0220 Strk18751	2.
5	6.388 44.4709 TOTL 6563 5.022 1.9175 TOTL 1216 6.388 44.4709 nFnu 4860	5.
)	6.390 44.7176 TOTL 4861 4.740 1.0000 TOTL 1026 5.928 15.4447 nFnu 1215	з.

	(,)											
TOTL 4861	4.740	1.0000	Q(H) 1216	12.688*	******	TOTL74578	3.082	0.0220	Strk187	51	2.182	0.0028
TOTL 1216	6.388	44.4709	TOTL 6563	5.022	1.9175	TOTL 1216	6.388	44.4709	nFnu 48	60	5.355	4.1223
TotH 0	6.390	44.7176	TOTL 4861	4.740	1.0000	TOTL 1026	5.928	15.4447	nFnu 12	15	3.374	0.0431
BFH1 0	6.386	44.2523	TOTL 4340	4.510	0.5893	TOTL 973	5.620	7.5891	Inci 48	61	11.600*	******
BFHx 0	3.340	0.0398	TOTL 4102	4.319	0.3800	TOTL 950	5.382	4.3925	Inci 12	16	12.930*	* * * * * * * *
FF H 0	4.368	0.4254	TOTL18751	4.182	0.2769	TOTL 938	5.188	2.8099	BA C	0	5.717	9.4915
CA B 4861	5.093	2.2540	TOTL12818	3.979	0.1736	INWD 1216	6.078	21.8041	PA C	0	5.204	2.9140
CA B 1216	6.626	77.0445	TOTL10938	3.796	0.1140	Strk 1216	4.392	0.4489	H FF	0	5.243	3.1868
DU B 4861	5.093	2.2537	TOTL40512	3.568	0.0674	Strk 6563	3.022	0.0192	H FB	0	5.651	8.1480
Q(H) 4861	11.154*	*******	TOTL26252	3.412	0.0471	Strk 4861	2.740	0.0100	TOFF	0	5.243	3.1868

333Cell Peak1.24E+00 Lo 1.00E-05=0.9105cm Hi-Con:1.16E+01 Ryd E(hi):7.35E+06Ryd E(hi): 100.01 MeV
P(nu>1ryd): -2.0111 Average nu:1.491E+00 P(X-ray): 0.0000 P(BalC): -2.1579 Q(Balmer C): 8.7181
Q(1.0-1.8): 8.3840 Q(1.8-4.0): 7.7615 Q(4.0-20): 5.3654 Q(20): 0.0000 Ion pht flx:3.001E+08
L(gam ray): 0.0000 Q(gam ray): 0.0000 L(Infred): -3.5006 Alf(ox): 0.0000 Total lumin: -1.7692
U(1.0):1.001E-02 U(4.0):7.736E-06 T(En-Den):2.943E+00 T(Comp):4.787E+04 nuJnu(912A):1.157E-02
Occ(FarIR):3.607E-13 Occ(H n=6):1.295E-16 Occ(1Ryd):5.334E-19 Occ(4R):3.849E-23 Occ (Nu-hi):2.802E-33
Tbr(FarIR):5.999E-13 Tbr(H n=6):5.749E-13 Tbr(1Ryd):8.425E-14 Tbr(4R):2.435E-17 Tbr (Nu-hi):5.037E-27
1 Te:1.000E+04 Hden:1.000E+00 Ne:9.996E-01 R:1.000E+25 R-R0:5.000E-01 dR:1.000E+00 NTR: 1 Htot:1.980E-24 T912: 1.242E-20###
-24.91 4686 0.00 5876 0.00 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00
P(LINES): 1.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
Hydrogen 3.849E-04 9.996E-01 H+0/Hden: 1.000E+00 5.662E-16 H- H2 1.340E-18 2.766E-17 H2+ HeH+ 8.342E-21 H col den 1.000E+00
Hydrogen 1.293E+11 1.000E+00 H+0/Hden: 1.000E+00 5.927E+09 H- H2 4.842E+08 H2+ 1.044E+10 He H+ 8.342E-21
H 2SP 3-6 9.907E-15 2.016E-13 2.496E-21 3.577E-21 5.385E-21 7.823E-21 Texc(La); 5.265E+03 T(contn): 2.943E+00 T(diffs): 2.734E+02
H 2SP 3-6 4.620E+05 3.135E+06 1.159E-01 2.013E-01 2.767E-01 3.385E-01
Helium 6.713E-04 8.817E-01 1.176E-01 He I 2S3 2.233E-10 Comp H, C 3.654E-31 7.634E-32 Fill Fact 1.000E+00 Gam 1/tot 9.998E-01
Helium 5.806E+06 6.755E-06 1.000E+00 He I 2S3 3.236E+09 Comp H, C 3.654E-31 7.634E-32 Fill Fact 1.000E+00 Gam 1/tot 9.998E-01
He singlet 6.713E-04 2.091E-15 5.464E-22 7.203E-22 1.084E-21 1.574E-21 He triplt 2.233E-10 1.322E-20 3.125E-22 2.249E-21 6.212E-22
He singlet 5.806E+06 2.984E-03 1.151E-01 1.839E-01 2.526E-01 3.089E-01 He triplt 3.236E+09 2.408E-01 1.306E-01 4.379E-01 7.840E-02
HeII 8.817E-01 4.338E-16 1.165E-22 1.763E-22 2.792E-22 4.250E-22 3.689E-21 4.020E-20 8.035E-18 PRAD/GAS; 3.883E+04
HeII 6.755E-06 1.483E-09 2.382E-04 4.369E-03 1.834E-02 4.196E-02 1.084E-01 2.574E-01 4.846E-01 1.238E+00 PRAD/GAS; 3.883E+04
Pressure NgasTgas; 2.000E+04 P(total): 1.072E-07 P(gas): 2.761E-12 P(Radtn): 1.072E-07 Rad accel 1.877E-10 Force Mul 8.261E+02
Carbon 8.400E-06 3.524E-02 9.055E-01 5.918E-02 3.281E-05 0.000E+00 0.000E+00 H20+/Otot 0.000E+00 0H/Otot1 0.000E+00
Nitrogen 1.027E-05 2.968E-02 9.099E-01 6.038E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 1.204E-05 5.837E-02 9.118E-01 2.983E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.472
Neon 5.841E-05 6.776E-02 9.250E-01 7.226E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 0.000E+00 2.348E-02 9.761E-01 4.406E-04 0.000E+00
Aluminium 0 0.000E+00 8.098E-02 6.308E-01 2.882E-01 0.000E+00
Silicon 0 0.000E+00 1.758E-02 6.955E-01 2.831E-01 3.865E-03 0.000E+00 0.000E+000E+
Sulphur 0 0.000E+00 1.552E-02 8.364E-01 1.471E-01 9.894E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00

* * Chemical composition He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 A:1.0E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10

CLOUDY 80.08

* * * *

Cooling: H FF Heating: BFH1	CASE A 0:0.281 H FB 0:0.719 0:0.990				
IONIZE PARMET:				L(ion): 12.989 Q(low): 23.79	P(low) 12.86
ENERGY BUDGET:	Heat: 6.390 Coolg: 5.7	94 Error: 74.7%	Compt H: -0.437	WorkF: 6.979 F-F H 4.368	PRADMX:1.05E-08
Column density	H12:1.000E+15 H II:9.995E+	4 HI:4.824E+11	H-: 3.356E+04	H2: 2.633E+02 H2+:6.132E+03	He H+:1.216E-05
	OH: 0.000E+00 Heff:0.000E+	00			
<nh>:1.000E+15</nh>	<tp>:1.00E+04 <to3>:1.00E+</to3></tp>	04 Ne:9.995E+14	ti(snd):7.76E-07	NeN+dl:9.99E+29 <t(c3)>:1.00E+0</t(c3)>	4 <e(c3)>:1.00E+15</e(c3)>
He/Ha:2.97E-10	= 2.97*true N/Oap:0.00E+	00 = 0.00true	T(O3R):1.000E+01	L THIN:1.00E+30 <t(s2)>:1.00E+0</t(s2)>	4 <e(s2)>:1.00E+15</e(s2)>
T He+:1.00E+04	EHe+:1.00E+15 T(O+):1.00E+	04 EO+:1.00E+15	iter/zn: 1.000	Te-low:1.00E+04 Te-high:1.00E+0	4 Hlu/zn:1.00E+00
<a>:0.00E+00	erdeFe0.0E+00 Tcompt1.65E-	15 Tthr6.65E-03	<tden>: 1.00E+04</tden>	<dens>:1.66E-09 <mol>:5.00E-01</mol></dens>	
Mean Jeans	l(cm)2.17E+14 M(sun)4.47E+	00 smallest:	len(cm):2.17E+14	M(sun):4.47E+00 Alf(ox-tran):	0.0000

Argon0 4.726E-06 3.715E-02 8.487E-01 1.139E-01 3.008E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+000.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00Calcium0 0.000E+00 4.066E-04 8.936E-02 8.677E-01 4.243E-02 5.715E-05 0.000E+00 0.00E+00 0

*********************************** CLOUDY 80.08 <*******
* title case B
* c this is a test of the 10-level H atom
* c this input will predict the Hb emissivity per
* c unit vol; the answer should be 1.24E-25 (Seaton 1959)
* c b(3) = 0.116; (4)=0.201; (5)=0.276; (6)=0.335
* print departure coefficients
* case b
* constant temperature = 4</pre> constant temperature = 4 * constant temperature = 4
* stop zone 1
* black body, T=50,000K
* ionization parameter -2
* hden = 0
* abundances -10
* drmax 0 drmin 0 print short Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 1 of 1. Intensity (erg/s/cm^2)

TOTL 4861-24.910 1.0000 TOTL 1216-23.641 18.5924	TOTL 6563-24.478	2.7068	TOTL74578-26.671 2 NU 0-23.876	0.0174	nFnu 1215-26.626 Inci 4861 -3.400**	0.0193
Toth 0-23.703 16.1011	TOTL 4861-24.910	0.5066	TOTL 1216-23.641	18.5924	Inci 1216 -2.070**	
BFH1 0-23.703 16.1009	TOTL 4102-25.434	0.2995	INWD 1216-23.942	9.2962	BA C 0-24.283	4.2391
CA B 4861-24.907 1.0067	TOTL18751-25.468	0.2769	Dest 1216-24.219	4.9083	PA C 0-24.796	1.3014
CA B 1216-23.374 34.4095	TOTL12818-25.736	0.1492	e sc 1216-27.558	0.0022	H FF 0-24.757	1.4233
DU B 4861-24.907 1.0067	TOTL10938-25.957	0.0898	e sc18751-25.468	0.2771	H FB 0-24.465	2.7860
Q(H) 4861 -3.846*******		0.0579	e sc40512-26.147	0.0580	Cool 1216-26.856	0.0113
Q(H) 1216 -2.312*******	TOTL26252-26.341	0.0371	nFnu 4860-24.385	3.3524	Toff 0-24.757	1.4233

Cooling: H FF Heating: BFH1	CA 0:0.337 H FB 0:1.000	SE B 0:0.660					
IONIZE PARMET:				Q(ion): 8.477		Q(low): 8.79	P(low) -2.14
ENERGY BUDGET:	Heat: -23.703	Coolg: -24.285	Error: 73.8%	Compt H: -30.437	WorkF: -20.000	F-F H-29.743	PRADMX:3.88E+04
Column density	H12:1.000E+00	H II:9.996E-01	HI:3.849E-04	H-: 5.662E-16	H2: 1.340E-18	H2+:2.766E-17	He H+:8.342E-21
	OH: 0.000E+00	Heff:0.000E+00					
<nh>:1.000E+00</nh>	<tp>:1.00E+04</tp>	<to3>:1.00E+04</to3>	Ne:9.996E-01	ti(snd):7.76E-07	NeN+dl:9.99E-01	<t(c3)>:1.00E+04</t(c3)>	<e(c3)>:1.00E+00</e(c3)>
He/Ha:9.32E-11	= 0.93*true	N/Oap:3.26E-01	= 0.33true	T(03R):9.854E+03	L THIN:1.00E+30	<t(s2)>:1.00E+04</t(s2)>	<e(s2)>:1.00E+00</e(s2)>
T He+:1.00E+04	EHe+:1.00E+00	T(O+):1.00E+04	EO+:1.00E+00	iter/zn: 1.000	Te-low:1.00E+04	Te-high:1.00E+04	Hlu/zn:1.00E+00
<a>:0.00E+00	erdeFe0.0E+00	Tcompt1.65E+15	Tthr7.98E+12	<tden>: 1.00E+04</tden>	<dens>:1.66E-24</dens>	<mol>:5.00E-01</mol>	
Mean Jeans	l(cm)6.87E+21	M(sun)1.41E+08	smallest:	len(cm):6.87E+21	M(sun):1.41E+08	Alf(ox-tran):	0.0000

CLOUDY 80.08

**************************************	L J J J J J J
*	*****
title Compton limit, test continuum partition	*
* c test of thermal equil in compton limit; temp should EXACTLY equal 2E5K	*
* c check continuum partition;	*
* c energy range, photon densities, luminosities, follow	*
* c 0.25-1. Q=26.6470 L=15.8190 c 1-1.807 Q=26.8867 L=16.3766	*
* c $1.807-4$ 0=27.3042 L=17.0948 c $4-20$ 0=27.2041 L=17.3179	*
* c 20 $Q=22.9038$ L=22.9038 c total lumin 17.5597	*
* c nufnu(912A) = 1.8029E+16	*
* black body t=200,000K lte	*
* grains -5 no heating no cooling	*
* hden = 6	*
* stop zone 1	*
* faint .1	*
* print last short	*
* metals -10	*
* iterate	*
* stop lyman continuum optical depth = -6	*
* print departure coef	*
* drmax 0	*
* drmin 0	*
* tolerance .0001 % decrease tolerance on heat-cool match	*
* c compton.in	*
* c cray	*
*	*
***************	*****
Chemical composition	
He:.098 C:3.63E-14 N:1.12E-14 O:8.51E-14 Ne:1.23E-14 Mg:3.80E-15 Al:3.0E-16 Si:3.55E-15 S:1.62E-15 A	A:3.6E-16 Ca:2.3E-16 Fe:4.68E-15
378Cell Peak4.95E+00 Lo 1.00E-05=0.9105cm Hi-Con:4.43E+01 Ryd E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 17.5517 Average nu:3.727E+00 P(X-ray): 13.4506 P(BalC): 15.8197	Q(Balmer C): 26.6477
Q(1.0-1.8): 26.8874 Q(1.8-4.0): 27.3043 Q(4.0-20): 27.2042 Q(20): 22.7730	Ion pht flx:4.387E+27
L(gam ray): 0.0000 Q(gam ray): 0.0000 L(Infred): 14.1236 Alf(ox): 0.0000	Total lumin: 17.5599
U(1.0):1.463E+11 U(4.0):5.338E+10 T(En-Den):2.000E+05 T(Comp):1.999E+05	nuJnu(912A):1.805E+16
Occ(FarIR):1.202E+05 Occ(H n=6):4.463E+01 Occ(1Ryd):8.331E-01 Occ(4R):4.426E-02	Occ (Nu-hi):1.074E-15
Tbr(FarIR):1.999E+05 Tbr(H n=6):1.982E+05 Tbr(1Ryd):1.316E+05 Tbr(4R):2.800E+04	Tbr (Nu-hi):7.396E-09
Grain(Pal):4.423E-28 Grain(Bal):1.783E-27 Grain Mg2:4.381E-27 Grain R:1.527E-26	Grain(HeII):5.214E-27
##### 1 Te:1.999E+05 Hden:1.000E+06 Ne:1.196E+06 R:1.000E+25 R-R0:5.000E-01 dR:1.000E+00 NTR: 1 H	

1 Te:1.999E+05 Hden:1.000E+06 Ne:1.196E+06 R:1.000E+25 R-R0:5.000E-01 dR:1.000E+00 NTR: 1 Htot:3.892E-05 T912: 2.527E-20###
-14.48 4686 2.00 5876 0.00 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00
P(LINES): 0.000

Carbon 0.000E+00 0.000E+00 0.000E+00 0.000E+00 7.713E-13 3.361E-05 1.000E+00 H2O+/Otot 0.000E+00 OH+/Ototl 0.000E+00	
Nitrogen 0.000E+00 0.000E+00 0.000E+00 0.000E+00 7.343E-18 4.031E-04 9.996E-01 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+0	00
Oxygen 0.000E+00 0.000E+00 0.000E+00 0.000E+00 3.655E-26 1.661E-13 1.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-13.42	26
Neon 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 1.940E-21 5.618E-11 1.000E+00 0.000E+00 0.000E+00	
Magnesium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 3.016E-15 1.372E-07 1.000E+00 0.000E+0	00
Aluminium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 1.374E-11 8.677E-06 1.000E+0	00
Silicon 1 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 1.940E-08 1.522E-04 9.998E-0	01
Sulphur 1 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 2.322E-06 8.677E-03 9.913E-0	01
Argon 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 4.825E-09 6.202E-04 9.994E-0	01
Calcium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 9.378E-21 1.682E-10 1.000E+00 0.000E+0	00
Iron 5 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 5.080E-08 3.008E-04 9.997E-0	01
Calculation stopped because NZONE reached.	
Geometry is plane-parallel.	
Photoionization of He 2TriS reached 100.0 percent of the total rate out.	
The largest continuum occupation number was 1.202E+05 at 1.053E-05 Ryd.	
The continuum occupation number fell below 1 at 1.033E+03 Angstroms.	
!The largest continuum brightness temperature was 1.999E+05K at 1.053E-05 Ryd.	
The continuum brightness temperature fell below 10,000K at 5.745E+00 Ryd.	
W-A physical process has been disabled.	
Continuum occupation number reached 8.37E+03 for some fine structure transitions.	
Induced recombination was 94.8% of the total for H level 7	
Stimulated emission was 99.4% of the total for H transition 7 - 6	
Population of H n=2 reached $3.30E+00$ relative to the ground state.	
Compton heating was100.0% of the total.	
W-Maximum tempertaure of grain Gra-ISM was 2.00E+05, above sublimation temperature?	
W-Maximum tempertaure of grain Sil-ISM was 2.00E+05, above sublimation temperature?	
Frequency out of range of free-free gaunt factor routine.	
The ratio of radiation to gas pressure reached 5.11E+03. Caused by line number 7	

faint .1
print last short
metals -10
iterate stop lyman continuum optical depth = -6 print departure coef drmax 0 drmin 0 tolerance .0001 % decrease tolerance on heat-cool match c compton.in Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2)
 Emergent line intensities

 TOTL 6563-14.123
 2.2854
 TOTL 4340-14.770
 0.5145

 C 4 1549-35.000
 0.0000
 N 2 6584-35.000
 0.0000

 O 1 6363-35.000
 0.0000
 TOTL 3727-35.000
 0.0000

 TOTL 4363-35.000
 0.0000
 Emis 2798-35.000
 0.0000
 TOTL18751-15.039 TOTL 4861-14.482 1.0000 0.2772 N 2 6548-35.000 O 3 5007-35.000 S 2 6720-35.000 TOTL 1909-35.000 O 1 6300-35.000 0.0000 0.0000 0.0000 o s 3 4959-35.000 3 9532-35.000 0.0000 0.0000 Intrinsic line intensities TOTL 6563-14.122 TOTL 4861-14.481 TOTL 4340-14.769 TOTL 4102-15.006 TOTL18751-15.038 0-12.364 130.6723 0-13.072 25.6150 0-12.373 128.0286 0-12.644 68.6153 0-11.823 454.6321 TOTL 4861-14.481 1.0000 TOTL 1216-12.680 63.2397 TotH 0-4.410******** BFH1 0-12.200 190.6821 e sc 6563-14.724 0.5714 e sc 4861-14.480 1.0015 2.2844 Hind e sc 4861-14.480 1.0015 nFnu 4860 -6.388******** nFnu 1215 -4.043******** Inci 4861 14.226******** Heff Heff 0.5146
 BFH1
 0-12.200
 190.6821

 BFHx
 0-12.605
 75.0747

 BFHe
 0-12.199
 191.3468

 FF H
 0-14.818
 460.1147

 ComH
 0-4.410********
 10.1147

 CA B
 4861-14.199
 1.9118

 CA B
 1216-12.539
 87.4564

 DU B
 4861-14.373
 1.2809

 Q(H)
 1261
 15.319********

 Q(H)
 1216
 16.853********
 0.2769 TOFF Inci 1261 14.226******** Inci 1216 15.930******** BA C 0-13.259 16.6518 PA C 0-13.910 3.7232 Grai 0-2.907******* Grai 1216-14.479 1.0029 H FF 0-11.967 326.6035 ToFF 0-11.823 454.6321 HeII 228-11.901 380.0344 He2C 911-12.975 32.0131 TOTL 1640-13.215 18.4318 TOTL 4686-14.179 2.0005 TOTL 1216-13.622 7.2220 TOTL128/51-15.038 0.2769 TOTL12818-15.300 0.1516 TOTL 1216-12.680 63.2397 TOTL 973-13.600 7.5891 TOTL 950-13.897 3.8357 TOTL 938-14.138 2.2030 INWD 1216-12.974 32.1294
 TOTL
 1216-13.622
 7.2220

 Ca B
 1640-13.025
 28.5197

 Ca B
 4686-14.144
 2.1686

 DevB
 4686-14.488
 0.9824
 0-11.907 320.0035 0 -4.410********* 0-12.148 215.1410 Dest 1216-14.479 1.0029 e sc 1216-12.680 63.2397 ComC H FB

Cooling: ComC 0:1.000 Heating: ComH 0:1.000	COMPTON LIMIT, TEST CONTINUUM P	ARTITION			
IONIZE PARMET: U(1-) 11.1654	U(4-): 10.7274 U(sp): 11.17		L(ion): 17.552	Q(low): 26.68	P(low) 15.83
ENERGY BUDGET: Heat: -4.410	Coolg: -4.410 Error: 0.0%	Compt H: -4.410	WorkF: -11.272	F-F H-11.818	PRADMX:5.11E+03
Column density H12:1.000E+06	H II:1.000E+06 HI:5.500E-10	H-: 0.000E+00	H2: 0.000E+00	H2+:0.000E+00	He H+:0.000E+00
OH: 0.000E+00	Heff:0.000E+00				
<nh>:1.000E+06 <tp>:2.00E+05</tp></nh>	<to3>:0.00E+00 Ne:0.000E+00</to3>	ti(snd):1.91E-07	NeN+dl:1.20E+12	<t(c3)>:0.00E+00</t(c3)>	<e(c3)>:0.00E+00</e(c3)>
He/Ha:1.56E-01 = 1.59*true	N/Oap:0.00E+00 = 0.00true	T(O3R):0.000E+00	L THIN:1.00E+30	<t(s2)>:0.00E+00</t(s2)>	<e(s2)>:0.00E+00</e(s2)>
T He+:2.00E+05 EHe+:1.20E+06	T(O+):0.00E+00 EO+:0.00E+00	iter/zn: 1.000	Te-low:2.00E+05	Te-high:2.00E+05	Hlu/zn:1.00E+00
<a>:0.00E+00 erdeFe0.0E+00	Tcompt2.58E-10 Tthr2.44E+00	<tden>: 2.00E+05</tden>	<dens>:2.31E-18</dens>	<mol>:6.07E-01</mol>	
Mean Jeans l(cm)2.36E+19	M(sun)8.02E+06 smallest:	len(cm):2.36E+19	M(sun):8.02E+06	Alf(ox-tran):	0.0000
L(dust):-2.907E+00			. ,	. ,	
Gra-ISM Sil-ISM	Gra-Ori Sil-Ori Sil-0.01	Sil-0.1 Silica	tPN		
<tdust>: 2.001E+05 2.001E+05</tdust>	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+	00		
<vel d="">: 3.579E+12 4.204E+12</vel>	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+	00		
<pot d="">: 4.377E+02 4.273E+02</pot>	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+	00		

CLOUDY 80.08

title test that energy is conserved	
hden 1.0	
constant pressure	
iterate	
print last iteration	
black body, temp=5.5	
luminostity total -4	
stop temperature 3 linear	
radius 25	
c conserv.in	
c cray	

Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 A1:3.0E-06 S1:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05
398Cell Peak7.74E+00 Lo 1.00E-05=0.9105cm Hi-Con:6.88E+01 Ryd E(hi):7.35E+06Ryd E(hi): 100.01 MeV
P(nu> rvd): -4.0022 Average nu:5.628E+00 P(X-ray): -6.0827 P(BalC): -6.2859 O(Balmer C): 4.5377
Q(1.0-1.8): 4.8343 $Q(1.8-4.0)$: 5.3839 $Q(4.0-20)$: 5.6985 $Q(20)$: 3.2209 Ion pht fix:8.115E+05
L(gam ray): 0.0000 0(gam ray): 0.0000 L(Infred): -8.0210 Alf(ox): 0.0000 Total lumin: -3.9999
U(1.0):2.707E-06 U(4.0):1.672E-06 T(En-Den):8.149E-01 T(Comp):3.028E+05 nuJnu(912A):1.478E-06
Occ(FarIR):8.382E-18 Occ(H n=6):3.124E-21 Occ(1Ryd):6.821E-23 Occ(4R):6.913E-24 Occ (Nu-hi):7.530E-38
Tbr(FarIR):1.394E-17 Tbr(H n=6):1.387E-17 Tbr(1Ryd):1.077E-17 Tbr(4R):4.373E-18 Tbr (Nu-hi):8.093E-31
Pressure not converged; zone 18 Te: 1.19E+03 Hden: 3.04E+01 current Pres: 5.58E-12 Corr Pres 1.32E-11
Pressure not converged; zone 19 Te: 7.17E+02 Hden: 5.45E+01 current Pres: 5.99E-12 Corr Pres 1.32E-11
Pressure not converged; zone 20 Te: 5.17E+02 Hden: 9.76E+01 current Pres: 7.50E-12 Corr Pres 1.32E-11 Pressure not converged; zone 21 Te: 3.85E+02 Hden: 1.75E+02 current Pres: 9.92E-12 Corr Pres 1.32E-11
Pressure not converged; Zone 21 re: 3.85±42 Haen: 1.75±42 current Pres: 9.92E=12 Corr Pres 1.32E=11 ###### 1 Te:6.567E+03 Haen:1.000E+10 Ne:2.730E+10 R:1.00E+125 R-R0:1.013E+15 AR:2.02E+15 NR: 6 Htot:8.049E-23 T912: 9.904E-02###
1 Teto.50/E+U3 Hdenil.000E+U1 Net2./30E+U0 Kil.000E+25 K-RUII.013E+15 GK12.026E+15 NTK: 6 Http://dxiau.org/12.9.904E-02### -8.54 4686 0.04 5876 0.21 1909 0.00 1549 0.00 6584 2.04 5007 0.00 3727 1.80 6300 2.04 2798 1.38 1035 0.00
Hydrogen 7.762E-01 2.238E-01 H+0/Hden: 1.000E+00 3.050E-08 H- H2 9.256E-06 3.167E-08 H2+ HeH+ 9.917E-08 H col den 2.026E+16
H 25P 3-6 4.868E-14 3.056E-16 1.432E-20 1.865E-20 2.682E-20 3.803E-20 Texc(La); 3.108E+03 T(contn): 8.139E-01 T(diffs): 2.911E+02
Helium 5.211E-01 4.625E-01 1.636E-02 He I 2S3 2.907E-09 Comp H, C 3.550E-32 7.700E-34 Fill Fact 1.000E+00 Gam 1/tot 9.643E-01
He singlet 5.211E-01 3.959E-15 1.060E-21 1.413E-21 2.150E-21 3.151E-21 He triplt 2.907E-09 2.408E-20 5.241E-22 3.999E-21 1.265E-21
HeII 4.625E-01 2.126E-16 5.735E-23 8.778E-23 1.406E-22 2.161E-22 1.901E-21 2.025E-20 4.039E-18 PRAD/GAS: 2.648E-06
Pressure NgasTgas; 9.496E+04 P(total): 1.311E-11 P(gas): 1.311E-11 P(Radtn): 3.472E-17 Rad accel 2.337E-10 Force Mul 9.091E+05
Carbon 5.723E-01 4.173E-01 1.039E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 H2O+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 6.244E-01 3.755E-01 1.214E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 7.974E-01 2.025E-01 9.431E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.334
Neon 2.008E-01 5.223E-01 2.769E-01 1.477E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 1.284E-02 8.026E-01 1.845E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 4.568E-01 4.711E-01 6.435E-02 7.710E-03 4.288E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Silicon 0 3.451E-01 6.542E-01 5.756E-04 7.085E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Sulphur 0 7.537E-02 8.860E-01 3.868E-02 0.000E+00
Argon 0 2.921E-01 4.366E-01 2.714E-01 0.000E+00
Calcium 0 9.143E-01 8.505E-02 6.875E-04 0.000E+00
Iron 0 2.022E-02 9.735E-01 6.251E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Pressure not converged; zone 17 Te: 1.09E+03 Hden: 3.15E+01 current Pres: 5.32E-12 Corr Pres 1.31E-11
Pressure not converged; zone 18 Te: 6.93E+02 Hden: 5.64E+01 current Pres: 5.83E-12 Corr Pres 1.31E-11
Pressure not converged; zone 19 Te: 4.95E+02 Hden: 1.01E+02 current Pres: 7.41E-12 Corr Pres 1.31E-11
Pressure not converged; zone 20 Te: 3.71E+02 Hden: 1.81E+02 current Pres: 9.89E-12 Corr Pres 1.31E-11
#####184 Te:2.888E+00 Hden:4.029E+04 Ne:1.296E-01 R:1.000E+25 R-R0:3.948E+17 dR:6.933E+14 NTR: 9 Htot:3.001E-24 T912: 5.099E+03###
-6.21 4686 0.02 5876 1.16 1909 0.00 1549 0.00 6584 0.53 5007 0.00 3727 0.38 6300 0.81 2798 0.31 1035 0.00

Hydrogen											H col den	
H 2SP 3-6											T(diffs):	
Helium											Gam 1/tot	
He singlet												6.219E-25
HeII	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	PRAD/GAS;	7.403E-06	
Pressure											Force Mul	
Molecules											OH/Ototl:	1.874E-05
Carbon						0.000E+00						
Nitrogen	1.000E+00	3.278E-05	3.632E-12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/Ototl:	6.890E-08	02+/0tot:	2.047E-11
Oxygen											0.000E+00	A:-10.170
Neon	9.999E-01	8.127E-05	1.859E-12	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Magnesium (9.990E-01	9.640E-04	6.227E-09	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Aluminium (9.901E-01	9.875E-03	4.525E-09	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Silicon (9.822E-01	1.783E-02	8.967E-11	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Sulphur (9.700E-01	2.996E-02	1.606E-08	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
	9.996E-01											
Calcium (9.997E-01	2.557E-04	2.104E-09	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Iron (9.979E-01	2.081E-03	2.751E-13	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
	on stopped		owest Te r	eached.								
	is plane-p											
	ve of cooli						•					
	e struc lin											
	computed d					+00						
W-Temperatu												
	cooling equ											
C-Cloud thi										-01Mo)		
	as+line rad						constant p	pressure me	odel.			
	ire out of											
	<i>v</i> out of ra				routine.							
	ve level p			•								
C-3 body re												
	radiation						ackground v	with FIREB	ALL command	1.		
	radiation											
	on rate fel						ould this l	be include	1?			
	amount of t				tion reach	ed 66.7%						
	on molecula											
	low and ma											
	low and ma										0E+03	
Temp too	low and ma	trix not u	sed for He	ion in so	me zones.	Low-densit	y Case B a	ssumed. 1	68 THE2LO=	1.500E+03		

* title test that energy is conserved * hden 1.0 * constant pressure constant pressure
iterate
print last iteration
black body, temp=5.5
luminostity total -4
stop temperature 3 linear
ordine 25

Emission Line Spectrum. Constant Pressure Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2)

			, , , , , , , , , , , , , , , , , , ,			
TOTL 4861 -6.205 1.0000	Cool 1216 -8.177	0.0107	C 1 370 -5.750	2.8571	Si 2 2335 -8.318	0.0077
TOTL 1216 -4.777 26.8389	H2 1 2 -6.098	1.2802	C 2 158 -5.456	5.6109	Si 2 1808 -9.984	0.0002
TotH 0 -4.321 76.6107	H-FB 0 -7.547	0.0456	C 2 2326 -7.997	0.0161	PHOT 1895 -9.087	0.0013
BFH1 0 -4.631 37.5097	H2+ 0 -7.962	0.0175	INWD 2326 -8.298	0.0081	S 1R 1807 -6.982	0.1674
BFHe 0 -4.636 37.1006		0.0428	Phot 2326 -8.753	0.0028	S 2 6720 -5.760	2.7906
TotM 0 -5.905 1.9993	Heff 0 -7.375	0.0678	REC 1335 -8.685	0.0033	S 2 4074 -7.535	0.0468
н-н 0-9.509 0.0005	HeFB 0 -7.088	0.1311	Phot 1909 -8.768	0.0027	S 210330 -7.708	0.0314
CA B 4861 -6.227 0.9506	MeFB 0 -8.601	0.0040	N 1 5200 -7.009	0.1573	S II 6731 -6.152	1.1311
CA B 1216 -4.652 35.8045	MeFF 0 -9.079	0.0013	REC 5200 -9.171	0.0011	S II 6716 -5.985	1.6595
DU B 4861 -6.228 0.9504	Toff 0 -6.708	0.3144	N 2 6584 -6.478	0.5340	S II 4070 -7.659	0.0352
Q(H) 4861 -6.414 0.6186	esc 584 -7.759	0.0279	N 2 6548 -6.955	0.1780	S II 4078 -8.141	0.0116
Q(H) 1216 -4.880 21.1511		0.0078	N 2 5755 -9.037	0.0015	S II10323 -8.162	0.0111
TOTL 6563 -5.533 4.7029	He I 504 -6.653	0.3566	N 2 122 -6.954	0.1784	S II10289 -8.291	0.0082
TOTL 4861 -6.205 1.0000	He I 4471 -6.944	0.1826	N 2 203 -6.825	0.2402	S II10373 -8.611	0.0039
TOTL 4340 -6.565 0.4366	TOTL 5876 -6.142	1.1561	N 2 2140 -9.501	0.0005	S II10339 -8.291	0.0082
TOTL 4102 -6.816 0.2451	Ca B 5876 -6.143	1.1541	0 1 6300 -6.298	0.8072	S 3 18 -7.330	0.0751
TOTL18751 -6.763 0.2769	TOTL10830 -6.263	0.8768	0 1 6363 -6.776	0.2691	S 3 34 -6.990	0.1641
TOTL12818 -7.096 0.1286	INWD10830 -6.549	0.4535	O 1 5577 -9.009	0.0016	S 3 9532 -7.385	0.0662
TOTL10938 -7.339 0.0735	TOTL 3889 -6.875	0.2138	0 1 630 -5.152	11.3034	S 3 9069 -7.801	0.0254
TOTL40512 -7.507 0.0499	TOTL 7065 -7.681	0.0335	O 1 1470 -6.489	0.5200	S 3 6312 -9.767	0.0003
TOTL26252 -7.723 0.0303	CCHE 0 -9.720	0.0003	0 1 7774 -9.232	0.0009	S 3 3722 -9.996	0.0002
TOTL74578 -8.053 0.0142	He I 2 -7.205	0.1002	6lev 8446 -9.929	0.0002	Ar 2 7 -7.354	0.0710
2 NU 0 -5.205 10.0131	DevB 2 -7.401	0.0637	6lev 1304 -9.183	0.0011	Ar 3 7135 -7.705	0.0317
TOTL 1216 -4.777 26.8389	He I 5016 -7.345	0.0726	6lev 11-10.091	0.0001	Ar 3 7751 -8.334	0.0074
TOTL 1026-10.167 0.0001	DevB 5016 -7.436	0.0589	TOTL 3727 -6.625	0.3808	Ar 3 22 -8.450	0.0057
TOTL 973-10.130 0.0001	He I 3965 -7.678	0.0337	TOTL 7325 -9.004	0.0016	Ar 3 9 -7.305	0.0795
TOTL 950-10.072 0.0001	DevB 3965 -7.860	0.0222	IONZ 3727 -7.778	0.0268	Ca 2 3933 -7.381	0.0668
TOTL 938-10.015 0.0002	He I 3614 -7.962	0.0175	IONZ 7325 -8.377	0.0067	Ca 2 8579 -8.126	0.0120
LA X 1216 -4.873 21.5142	DevB 3614 -8.070	0.0137	O II 3729 -6.877	0.2130	Ca 2 7306 -6.208	0.9950
INWD 1216 -4.777 26.7921	He I 3448 -8.180	0.0106	O II 3726 -7.056	0.1411	Ca2K 3934 -7.590	0.0413
INWD 6563 -5.834 2.3515	DevB 3448 -8.348	0.0072	O II 2471 -9.106	0.0013	Ca2H 3969 -7.799	0.0255
INWD 4861 -6.506 0.5000	HeII 228 -6.733	0.2967	O II 7323 -9.262	0.0009	Ca2X 8498 -9.257	0.0009
INWD18751 -7.064 0.1384		0.0631	O II 7332 -9.352	0.0007	Ca2Y 8542 -8.299	0.0081
Dest 1216 -5.436 5.8841	He2C 911 -8.492	0.0052	Phot 1663-10.018	0.0002	Ca2Z 8662 -8.719	0.0031
e sc 6563 -9.761 0.0003		0.1843	O 3 5007 -9.833	0.0002	CaF1 7291 -6.433	0.5923
e sc 4861 -9.361 0.0007		0.0201	O 3 880 -9.308	0.0008	CaF2 7324 -6.600	0.4027
e sc18751 -6.763 0.2771		0.0726	O 3 520 -9.563	0.0004	Fe 2 48 -9.616	0.0004
e sc40512 -7.506 0.0500		0.2437	Ne 2 128 -6.090	1.3049	Fe 2 7 -6.283	0.8373
nFnu 4860 -5.948 1.8087		0.2231	Ne 3 156 -6.009	1.5719	Emis 3 -6.712	0.3115
nFnu 1215 -9.809 0.0002		0.0458	Ne 3 361 -7.083	0.1325	Cool 3 -6.712	0.3115
Inci 4861 -7.919 0.0193	DevB 4686 -7.578	0.0424	Ne 3 3869 -7.428	0.0600	TOT 0 -6.145	1.1492

IONIZE PARMET: U(1-) -5.5676 U(4-): -5.7769 U(sp): -9.17 Q(ion): 2.765 L(ion): -6.577 Q(low): 4.34 P(low) -6.62
ENERGY BUDGET: Heat: -4.321 Coolg: -4.320 Error: 0.4% Compt H: -14.041 WorkF: -4.154 F-F H-11.380 PRADMX:1.98E-03
Column density H12:6.725E+20 H II:6.016E+17 HI:3.950E+20 H-: 1.509E+11 H2: 1.382E+20 H2+:9.618E+11 He H+:6.427E+11
OH: 0.000E+00 Heff:0.000E+00
<pre><nh>:1.702E+03 <tp>:4.84E+03 <t03>:5.72E+03 Ne:2.364E+00 ti(snd):2.86E+12 NeN+dl:1.29E+18 <t(c3)>:5.52E+03 <e(c3)>:2.27E+00</e(c3)></t(c3)></t03></tp></nh></pre>
He/Ha:8.56E-01 = 8.73*true N/Oap:1.41E-01 = 1.07true T(O3R):5.980E+03 L THIN:1.00E+30 <t(s2)>:1.28E+02 <e(s2)>:8.72E-01</e(s2)></t(s2)>
T He+:4.88E+03 EHe+:2.12E+00 T(O+):5.41E+03 EO+:2.22E+00 iter/zn: 4.897 Te-low:2.89E+00 Te-high:6.57E+03 Hlu/zn:7.03E+00
<a>:0.00E+00 erdeFe0.0E+00 Tcompt6.80E+17 Tthr2.62E+11 <tden>: 4.48E+01 <dens>:4.00E-21 <mol>:1.60E+00</mol></dens></tden>
Mean Jeans l(cm)1.01E+18 M(sun)2.57E+01 smallest: len(cm):2.56E+17 M(sun):4.20E-01 Alf(ox-tran): 0.0000
Optical Depths: CONTN; COMP: 5.14E-07 H-: 5.88E-06 R(1300): 2.65E-03 H2+ 6.73E-06 HeTri:9.80E-06
Pfa:5.14E-07 Pa:5.16E-07 Ba:6.00E-06 Hb:5.13E-06 La:6.13E-01 1r:5.099E+03 1.8:1.48E+03 4.:2.175E+02 21R:2.381E+00
10830: 4.70E-02 3889: 2.00E-03 5876: 3.19E-13 7065: 1.76E-13
1550: 1.00E-20 2800: 2.95E+04 774: 1.00E-20 1240: 1.00E-20 1035: 1.00E-20 1335: 2.52E+03 977: 3.04E+00 1397: 6.52E-03
789: 1.00E-20 1207: 6.15E-02 1085: 1.08E+01 1194: 5.07E-02 1909: 1.21E-06 1895: 1.65E-06 2326: 1.26E-03 1666: 5.71E-08
1750: 3.14E-10 1025: 2.38E+05 352: 1.00E-20 347: 1.00E-20 1860: 6.00E+00 630: 1.00E-20 834: 9.79E+01 835: 2.78E-03
1808: 1.72E+05 1256: 5.24E+03 -3: 1.38E+03 -48: 1.73E-11 3934: 1.61E+01 3969: 8.13E+00 8498: 6.92E-09 8542: 6.16E-08
8662: 3.51E-08 353: 1.00E-20 1304: 8.15E+05 1122: 2.71E-02 990: 1.38E-03 1402: 1.00E-20 1214: 1.00E-20 1486: 1.00E-20
2335: 4.10E-01 1406: 1.00E-20 1656: 1.27E+06 9830: 2.11E-04 8727: 4.39E-11 6300: 2.16E-03 5577: 1.64E-13 7291: 4.19E-05
7324: 2.90E-05 1039: 1.16E+05 -8446: 7.55E-13 -4368: 2.86E-15 -132: 2.87E-17 -113: 4.51E-17 -29: 1.07E-20 -46: 1.07E-16
-245: 1.00E-20 765: 1.00E-20 -1198: 1.00E-20 786: 1.00E-20
C157: 6.86E-03 N122: 1.06E-05 N205: 2.09E-03 N57: 2.42E-08 O146: 1.06E-05 O63: 4.22E+00 O88: 5.30E-07 O52: 1.33E-09
026: 1.00E-20 NE13: 1.37E-03 NE36:-5.07E-09 NE16: 2.17E-04 MG4: 1.00E-20 MG14: 1.00E-20 MG6: 1.00E-20 SI35: 2.65E-02
S19: 1.41E-08 S34: 4.26E-05 S11: 1.00E-20 AR7: 2.35E-05 AR9: 4.41E-06 AR22:-3.84E-11 AR13: 1.00E-20 AR8: 1.00E-20
CA3: 1.00E-20 CA12: 1.00E-20 CA4: 1.00E-20 Ne14: 1.00E-20 Ne24: 1.00E-20 Si3: 1.00E-20 Si4: 1.00E-20 Fe7: 1.00E-20
Fe61: 1.00E-20 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 1.00E-20 Si6.5: 1.00E-20 C610: 2.30E-01 C370: 2.11E+01
Old hydro optical depths: 1 5.04E+03 2 2.82E-06 3 5.59E-06 4 1.58E-06 5 5.54E-16 6 1.36E-15 7 8.23E-15
Lines: 2-1 9.81E+08 3-2 6.67E-07 4-3 4.61E-13 5-4 2.97E-13 6-5 2.70E-13 7-6 3.99E-13 8-7 4.14E-13
New hydro optical depths: 1 5.10E+03 2 2.98E-06 3 5.89E-06 4 1.67E-06 5 5.41E-16 6 1.33E-15 7 8.02E-15
Lines: 2-1 9.89E+08 3-2 6.27E-07 4-3 4.38E-13 5-4 2.83E-13 6-5 2.57E-13 7-6 3.83E-13 8-7 4.24E-13
Old He Is optical depths: 1 1.46E+03 2 1.89E-06 3 2.20E-20 4 1.80E-20 5 1.89E-20 6 2.23E-20 7-2.04E-19
Lines: 2-1 1.12E+08 3-2 2.17E-08 4-3 7.97E-14 5-4 5.75E-14 6-5 5.62E-14 7-6 8.52E-14 8-7 3.95E-14
New HE Is optical depths: 1 1.48E+03 2 1.99E-06 3 2.16E-20 4 1.75E-20 5 1.79E-20 6 2.06E-20 7-2.16E-19
Lines: 2-1 1.14E+08 3-2 2.11E-08 4-3 7.66E-14 5-4 5.56E-14 6-5 5.45E-14 7-6 8.31E-14 8-7 4.17E-14
Old He II optical depths: 1 2,15E+02 2 5,04E+03 3 9,65E-21 4 9,15E-21 5 8,34E-21 6 7,11E-21 7-2,14E-20
Lines: 2-1 9.07E+03 3-2 1.92E-11 4-3 2.84E-18 5-4-1.37E-18 6-5-1.60E-17 7-6 4.46E-17 8-7 6.36E-16
New HE II optical depths: 1 2.17E+02 2 5.10E+03 3 9.64E-21 4 9.10E-21 5 8.25E-21 6 6.96E-21 7-2.30E-20
Lines: 2-1 9.40E+03 3-2 1.97E-11 4-3 2.90E-18 5-4-1.49E-18 6-5-1.68E-17 7-6 4.65E-17 8-7 6.64E-16
Hydrogen -0.001 -2.818 Log10 Mean Ionisation (over volume)
Helium -0.001 -2.644 -4.210
Carbon -0.002 -2.340 -4.541
Nitrogen -0.001 -2.883 -6.682
Oxygen 0.000 - 3.149 - 6.731
Neon -0.004 -2.174 -2.798 -7.837
Magnesium -0.022 -1.317 -2.834
Aluminum -0.049 -0.972 -3.144 -3.818 -6.167
Silicon -0.095 -0.706 -5.873 -6.370
Sulphur -0.168 -0.493 -3.636
Argon -0.003 -2.266 -3.049
Calcium -0.007 -1.808 -4.543 Iron -0.024 -1.272 -4.967
1101 -0.024 -1.272 -4.507

TEST THAT ENERGY IS CONSERVED Cooling: C I 9850:0.060 C 1 610:0.096 C 2 158:0.073 O 1 630:0.147 Si 2 35:0.333 FEIR 0:0.062 Heating: BFH1 0:0.490 BFHe 0:0.484

Inci 1	216 -6.176	1.0700	C 1	1656	-9.331	0.0007	Ne 3	3968	-7.941	0.0184	FEIR	0 -5.528	4.7624
BA C	0 -5.795	2.5725	REC	1656	-7.283	0.0837	Mg 1	4571	-9.893	0.0002	Fe 3	0 -9.287	0.0008
PA C	0 -6.266	0.8700	СЛ	9850	-5.539	4.6431	Emis	2798	-6.714	0.3103	Fe 3 5	270 -9.967	0.0002
H FF	0 -6.816	0.2454	C 1	8727	-6.986	0.1658	Cool	2798	-6.714	0.3103	Fe 3 4	658 -9.723	0.0003
H FB	0 -6.546	0.4564	C 1	L 610	-5.337	7.3813	Si 2	35	-4.797	25.6395			

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
Hydrogen	-0.001	-2.818					Loq10 Mea	n Ionis	ation	(over 1	adius)						
Helium	-0.001	-2.644	-4.210				-										
Carbon	-0.002	-2.340	-4.541														
Nitrogen	-0.001	-2.883	-6.682														
Oxygen	0.000	-3.149	-6.731														
Neon	-0.004	-2.174	-2.798	-7.837													
Magnesium	-0.022	-1.317	-2.834														
Aluminum	-0.049	-0.972	-3.144	-3.818	-6.167												
Silicon	-0.095	-0.706	-5.873	-6.370													
Sulphur	-0.168	-0.493	-3.636														
Argon	-0.003	-2.266	-3.049														
Calcium	-0.007	-1.808	-4.543														
Iron	-0.024	-1.272	-4.967														
0 5 1 075			1 5 0	00 0 000 1	5 2 0	0 005		F 0 00	-	5 2 0	0.07	2 5 0 0	0.00.0	7 5 0	005.00	7 5 10	0 00 0 00

0.5-1.0KEV:7.08E-01 1.0-1.5:0.00E+00 1.5-2.0:0.00E+00 2.0-2.5:0.00E+00 2.5-3:0.00E+00 3-5:0.00E+00 5-7.5:0.00E+00 7.5-10:0.00E+00

				Normalised	continuum				
0.25******	0.2773.254	0.3045.456	0.3332.698	0.3628.435	0.3923.702	0.4320.881	0.4718.581	0.5116.424	0.5614.095
0.62 7.225	0.67 6.008	0.74 1.980	0.81 0.637	0.88 0.029	0.97 0.045	0.98 0.049	0.99 0.050	1.00 0.051	

Inward continua (nuFnu) at head of Balmer, Lyman series; 3.38E-06 2.52E-06

Outwrd continua (nuFnu) at head of Balmer, Lyman series; 3.38E-06 0.00E+00

			Emergent continuu	m - phot/ryd/cm2	(r in)	
0.26 2.37E+06	0.67 3.08E+05	1.0 0.00E+00	2.5 1.32-283	5.3 1.24E-44	1.36E+01 4.63E+00	3.54E+01 6.91E-01
0.29 1.26E+06	0.76 3.07E+04	1.1 0.00E+00	2.9 2.75-210	5.9 1.84E-31	1.54E+01 2.45E+01	3.99E+01 8.07E-02
0.33 8.77E+05	0.86 1.61E+03	1.2 0.00E+00	3.2 6.03-156	6.7 1.17E-21	1.73E+01 5.87E+01	4.50E+01 9.80E-03
0.37 7.93E+05	0.97 3.16E+03	1.4 0.00E+00	3.6 3.23-115	7.5 1.79E-14	1.95E+01 7.62E+01	5.05E+01 9.08E-04
0.42 7.26E+05	0.99 3.52E+03	1.6 7.56E-03	3.9 3.59E-97	8.5 2.57E-09	2.20E+01 4.95E+01	5.47E+01 1.35E-04
0.47 6.92E+05	0.99 3.65E+03	1.8 0.00E+00	4.0 1.02E-88	9.5 1.32E-05	2.48E+01 2.87E+01	5.92E+01 1.73E-05
0.53 6.51E+05	1.00 0.00E+00	2.0 5.36E-02	4.2 1.01E-79	10.8 5.35E-03	2.79E+01 1.15E+01	6.41E+01 1.77E-06
0.60 3.38E+05	1.01 0.00E+00	2.3 1.46E-03	4.7 3.63E-60	12.1 3.24E-01	3.15E+01 3.21E+00	

CLOUDY 80.08

**************************************	*******
*	
* title (roughly) Ferland et al. DQ Her model	
* c model of ice cold ionized cloud arund old nova DQ H	er
* c roughly that of Ferland et al. 1984 Ap.J. 281, 194.	
* c tests behaviour of code at very low temperatures	
* stop temp = 100	
* c flat continuum, followed by nu^-2 power law	
* interpolate (0, 0) (0.3, 0) (8,000,000 -14.8)	
* luminosity total 34	
* hden = 2.	
* filling factor 0.667	
* covering factor 0.667	
* radius 16.5682, thickness=16.14613	
* abundances 2 20 200 50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
* grains	
* iterate	
* faint .05	
* print last	
* c dgher.in	
* c cray	
*	
*****	*********************

Chemical composition He:.196 C:7.26E-03 N:2.24E-02 O:4.26E-02 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

	Peak2.45E-01	Lo 1.00E-05=0.9120				hi): 100.01 MeV	
	/d): 33.1814	Average nu:2.007E+				Balmer C): 44.6874	
	.8): 43.3814	Q(1.8-4.0): 42.92				n pht flx:2.019E+09	
	ay): 29.3554	Q(gam ray): 35.86				tal lumin: 34.0001	
L/Lsola:		Abs bol mg: 3.67		.9271 Bol cor: -1		Fnu(Bbet): 33.4932	
U(1.0):6.734E-04	U(4.0):4.249E-	-05 T(En-Den):7.11	6E+00 T(Comp):6.50	3E+04 nuJ	Jnu(912A):8.762E-02	
Occ(Far	ER):3.833E-02	Occ(H n=6):2.005E-	12 Occ(1Ryd):4.03	8E-18 Occ(4R):3.95	7E-21 Occ	c (Nu-hi):2.710E-52	
Tbr(Far	ER):6.364E-02	Tbr(H n=6):8.901E-	-09 Tbr(1Ryd):6.37	8E-13 Tbr(4R):2.50	3E-15 Tbr	r (Nu-hi):2.990E-40	
Grain(Pa	al):4.422E-23	Grain(Bal):1.782E-	-22 Grain Mg2:4.38	0E-22 Grain R:1.52	7E-21 Gra	ain(HeII):5.214E-22	
		0E+02 Ne:1.176E+02 R					103E=02###
		09 0.00 1549 0.00					
		H+0/Hden: 1.000E+00					
		5.348E-18 4.615E-18					
		2.953E-02 He I 2S3					
		4.185E-18 3.612E-18					2.798E-18
		9.874E-21 8.521E-21					
		Pot(Volt)-9.775E-03					
		Pot(Volt)-8.168E-03					
		P(total): 1.100E-11					5.661E+04
		3.521E-01 2.313E-03					
		1.917E-01 4.992E-03					
		2.367E-01 2.577E-03					A:-11.422
		3.615E-01 1.021E-02					
Magnesium 0 4.532	2-02 5.982E-01	3.506E-01 5.795E-03	1.782E-05 2.888E-0	8 1.515E-11 0.000E+0	0 0.000E+00 0).000E+00 0.000E+00	0.000E+00
		1.961E-01 1.657E-02					
Silicon 0 6.683	2-03 8.912E-01	9.495E-02 7.044E-03	1.258E-04 1.992E-0	7 9.818E-11 3.020E-1	4 6.926E-18 0).000E+00 0.000E+00	0.000E+00
		3.447E-01 1.693E-03					
Argon 1 5.523	2-01 4.367E-01	6.663E-03 6.628E-05	0 1.975E-06 1.144E-0	8 1.687E-10 4.912E-1	3 5.009E-17 4	4.201E-21 3.241E-25	2.068E-29

Calcium 0 2.056E-01 6.614E-01 1.293E-01 3.588E-03 1.512E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
11uTe:6.478E+02 Hden:1.000E+02 Ne:1.111E+02 R:5.029E+16 R-R0:1.329E+16 dR:6.173E+14 NTR: 1 Htot:3.569E-19 T912: 5.236E-01###
-4.02 4686 0.01 5876 0.81 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 1.17 6300 0.00 2798 0.00 1035 0.00
Hydrogen 1.118E-01 8.882E-01 H+0/Hden: 1.000E+00 8.096E-10 H- H2 6.618E-09 1.277E-09 H2+ HeH+ 1.300E-08 H col den 9.070E+17
H 2SP 3-6 7.313E-12 4.353E-16 3.019E-18 2.871E-18 3.600E-18 4.735E-18 Texc(La); 3.439E+03 T(contn): 6.036E+00 T(diffs): 2.460E+00
Helium 2.512E-01 7.310E-01 1.776E-02 He I 2S3 1.352E-06 Comp H, C 9.578E-28 9.687E-30 Fill Fact 6.670E-01 Gam 1/tot 1.000E+00
He singlet 2.512E-01 1.435E-12 2.201E-18 2.094E-18 2.625E-18 3.453E-18 He triplt 1.352E-06 2.816E-17 1.498E-19 1.731E-18 1.187E-18
HeII 7.310E-01 3.839E-14 3.342E-21 3.179E-21 3.985E-21 5.242E-21 0.000E+00 0.000E+00 0.000E+00 PRAD/GAS; 1.877E-03
Gra-ISM Dust temp 3.414E+01 Pot(Volt)-8.148E-02 Nelectron-1.697E+01 drft cm/s 6.941E+04 Heating: 1.282E-22 Frac(tot) 3.593E-04
Sil-ISM Dust temp 3.039E+01 Pot(Volt)-7.873E-02 Nelectron-1.640E+01 drft cm/s 3.960E+04 Heating: 1.630E-22 Frac(tot) 4.568E-04
Pressure NgasTgas; 1.514E+05 P(total): 2.095E-11 P(gas): 2.091E-11 P(Radtn): 4.024E-14 Rad accel 9.219E-08 Force Mul 5.954E+04
Carbon 1.635E-02 7.055E-01 2.775E-01 6.447E-04 2.355E-05 0.000E+00 0.000E+00 H20+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 3.171E-02 8.982E-01 6.920E-02 9.355E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/0totl: 0.000E+00 02/0totl: 0.000E+00
Neon 6.714E-02 6.257E-01 3.042E-01 2.994E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 6.043E-02 6.257E-01 3.119E-01 1.915E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 1.003E-02 8.057E-01 1.672E-01 1.696E-02 9.250E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Silicon 0 9.619E-03 9.604E-01 2.617E-02 3.752E-03 1.986E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Sulphur 0 8.168E-03 7.060E-01 2.853E-01 5.589E-04 2.526E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Argon 0 6.556E-03 5.271E-01 4.638E-01 2.496E-03 2.633E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calcium 0 2.455E-01 6.462E-01 1.063E-01 1.989E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Iron 0 2.672E-03 7.625E-01 2.102E-01 2.358E-02 9.818E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calculation stopped because outer radius reached.
Geometry is a thick shell.
Temperature out of range of free-free gaunt factor routine.

Temperature out of range of free-free gaunt factor routine. Frequency out of range of free-free gaunt factor routine. OI negative level populations 2 times. The ratio of radiation to gas pressure reached 2.94E+00. Caused by Lyman alpha. Temp too low and matrix not used for H in some zones. Low-density Case B assumed. 11 THLO= 1.000E+03 Temp too low and matrix not used for He singlets in some zones. Low-density Case B assumed. 11 THEILO= 1.000E+03 Temp too low and matrix not used for He ion in some zones. Low-density Case B assumed. 11 THE2LO= 1.500E+03

********************************* CLOUDY 80.08 <******
* title (roughly) Ferland et al. DQ Her model
* c model of ice cold ionized cloud arund old nova DQ Her
* c roughly that of Ferland et al. 1984 Ap.J. 281, 194.
* c tests behaviour of code at very low temperatures
* stop temp = 100
* c flat continuum, followed by nu^-2 power law
* interpolate (0, 0) (0.3, 0) (8,000,000 -14.8)
* luminosity total 34
* bden = 2.</pre> hden = 2. filling factor 0.667 Covering factor 0.667 radius 16.5682, thickness=16.14613 abundances 2 20 200 50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 abundances grains iterate faint .05 print last c dqher.in n Line Spectrum. Constant Density Model. Open geometry. Iteration 2 of 2. Luminosity (erg/s) emitted by shell with a covering factor of 66.7%. Emission Line Spectrum. INWD 1216 31.503 19.5182 INWD 6563 30.542 2.1380 INWD 4861 29.911 0.5000 TOTL 4861 30.212 TOTL 1216 31.825 TOTH 0 31.836 BFH1 0 31.496 TOTT 10830 30.021 0.6438 N 2 122 31.107 N 2 203 30.409 N 2 5680 29.016 1.0000 7.8525 40.9534 42.0279 INWD10830 29.715 TOTL 3889 29.474 0.3178 1.5728 0.0636
 TOTL 3889 29.474

 He I 2 29.117

 DevB 2 29.060

 He I 5016 28.985

 DevB 5016 28.985

 Bell 228 30.066

 HEII 228 30.066

 HEZC 911 29.067

 TOTL 1640 29.945

 DevB 1640 29.945

 DevB 1640 29.945

 Ca B 4686 29.429
 N 2 5680 29.016 N 3 57 30.935 O 1 630 28.923 O 1 7774 29.200 61ev 1304 28.954 TOTL 3727 30.279 IONZ 3727 30.279 INWD 4861 29.911 0.5000 INWD18751 29.354 0.1384 Dest 1216 29.683 0.2958 e sc18751 29.315 0.1266 nFnu 4860 30.369 1.4345 Inci 4861 33.4931909.1455 Inci 1216 33.3021229.7086 BFH1 0 31.496 19.1959 0.0803 5.2814 0.0704 0.0592 0.0566 BFHe 0 31.206 9.8626 0.0513
 TotM
 0
 31.324

 CA B
 4861
 30.298

 CA B
 1216
 31.795

 DU B
 4861
 30.298
 12.9272 1.2179 38.2751 0.0971 0.7131 1.1666 1.2172 0.2363 1.1666 Q(H) 4861 31.042 6.7457 Q(H) 1216 32.575 230.6365 TOTL 6563 30.844 4.2759 TOTL 4861 30.212 1.0000 BA C 0 30.630 PA C 0 30.179 Grai 0 30.126 Grai 1216 29.681 2.6136 0.9252 0.8188 0.0716 0.0809 0.5398 0.5287
 IONZ
 7325
 29.643

 O
 3
 880
 31.298

 O
 3
 520
 31.308

 O
 4
 26
 29.797
 0.2696 12.1676 12.4655 0.3844 4.2759 0.2941 Ne 3 156 29.089 Si 2 35 29.981 S 3 34 29.269 FEIR 0 29.297 Ca B 4686 29.429 DevB 4686 29.414 TOTL 4340 29.832 TOTL 4102 29.560 0.4167 H FB 0 29.394 esc 584 30.060 0.1518 0.1646 0.0752 0.5862
 esc
 584
 30.060

 He2p
 910
 29.329

 He I
 504
 30.649

 He I
 4471
 29.365
 DevB 4686 29.414 REC 1656 29.007 C 2 158 30.103 REC 1335 28.977 Phot 1909 29.292 REC 5200 29.372 0.1592 0.0623 0.7769 0.0582 TOTL18751 29.655 TOTL12818 29.302 0.2769 0.1308 2.7316 0.1138 TOTL10938 29.036 0.0667 0.1420 2 NU 0 31.225 10.2808 TOTL 5876 30.121 TOTL 1216 31.825 40.9534 Ca B 5876 30.074 Lines with negative intensities; 205 T OI 0 0.8091 0.1202 0.7270 0.1445

(ROUGHLY) FERLAND ET AL. DQ HER MODEL Cooling: N 2 122:0.188 N 3 57:0.126 O 3 880:0.291 O 3 520:0.298 Heating: BFH1 0:0.457 BFHe 0:0.235 TotM 0:0.308 U(1-) -3.1718 U(4-): -4.3717 U(sp): -3.44 Q(ion): 43.390 L(ion): 33.056 Q(low): 45.91 Heat: 31.836 Coolg: 31.833 Error: 0.6% Compt H: 23.280 WorkF: 32.292 F-F H 22.471 H12:9.0702F17 H II:8.242E+17 HI:8.281E+16 H-: 4.231E+08 H2: 3.109E+09 H2+:3.373E+08 OH: 0.000E+00 Heff:2.757E+19 TONTZE PARMET: P(low) 33.93 PRADMX:2.94E+00 ENERGY BUDGET : He H+:9.686E+09 Column density <TO3>:4.51E+02 Ne:1.147E+02 NeN+dl:9.41E+19 <T(C3)>:4.69E+02 <E(C3)>:1.14E+02 <NH>:1.000E+02 ti(snd):5.28E+10 <Tp>:4.75E+02 He/Ha:5.98E-01 T He+:4.74E+02 <a>:0.00E+00
 Strue
 N/Oap:0.00E+00
 0.00true
 T(OAR):0.00E+00

 EHe+:1.14E+02
 T(O+):4.79E+02
 EO+:1.14E+02
 iter/zn:
 3.500

 erdeFe1.1E+28
 Tcompt2.68E+10
 Thtr2.67E+07
 <Tden>: 4.76E+02
 1(cm)5.69E+19

 L THIN:1.00F+30 <T(S2)>:4.78E+02 <E(S2)>:1.14E+02

 Te-low:3.33E+02 Te-high:6.48E+02 Hlu/zn:3.50E+00

 <dens>:4.77E-22 <Mol>:1.19E+00

 M(sun):1.40E+04 Alf(ox-tran): -1.9936
 Mean Jeans L(dust): 3.013E+01 Sil-ISM Gra-Ori Sil-Ori Sil-0.01 Sil-0.1 Gra-ISM SilicatPN Gra-ISM SII-ISM Gra-Ur1 SII-Ur1 S Optical Depths: CONTN; COMP: 6.89E-07 Pfa:1.27E-05 10830: 2.41E+00 1550: 4.83E+00 4.:4.967E-01 21R:9.670E-03 977: 2.92E+03 1397: 3.57E-01
 1.02E-20
 1035:
 1.00E-20
 1335:
 2.7/E+03
 977:
 2.92E+03

 1.32E-01
 1909:
 1.16E-03
 1895:
 2.90E-04
 2326:
 1.39E-03

 1.00E-20
 1860:
 2.40E+00
 630:
 3.84E-02
 834:
 2.16E+04

 1.00E-20
 3934:
 1.25E+01
 3969:
 6.31E+00
 8498:
 1.41E-19

 3.60E+00
 990:
 7.80E+02
 1402:
 7.40E-05
 1214:
 2.07E-07

 7.87E-09
 8727:
 1.00E-20
 6300:
 1.72E-06
 5577:
 1.00E-20
 789: 5.55E+00 1666: 1.16E-02 1750: 1.77E-04 835: 5.65E+02 -3: 6.40E+00 1304: 6.51E+02 1656: 4.72E+01 -48: 1122: 9830: 1808: 1.78E+02 1256: 2.05E+00 8542 1.04E-18 353: 1.00E-20 1406: 1.56E-06 8662: 6.76E-19 2335: 4.25E-04 1486: 8.30E-05 7291: 8.38E-07
 1039: 9.24E+01
 8446: 6.70E-12
 4368:

 765: 5.05E+01
 -1198: 1.32E-07
 786:

 N122: 1.57E-02
 N205: 1.94E-02
 N57:

 NE13: 2.21E-04
 NE36:-3.44E-08
 NE16:
 7324: 5.80E-07 -245: 2.59E-16 2.56E-14 -132: 5.86E-14 -113: 9.23E-14 -29: 1.00E-20 -46: 2.19E-13

 7324: 5.80E-07
 1039: 9.24E+01
 -8446: 6.70E+12
 -436: 2.58E-14
 -132: 5.86E-14
 -113: 9.23E-14
 -29: 1.00E-20
 -46: 2.19E-13

 -245: 2.59E-16
 765: 5.05E+01
 -1198: 1.32E-07
 786: 3.92E-04
 -013: 5.86E-14
 -113: 9.23E-14
 -29: 1.00E-20
 -46: 2.19E-13

 C157: 2.29E-03
 N122: 1.57E-02
 N205: 1.94E-02
 N57: 1.06E-02
 0146: -1.90E-05
 063: 1.98E-02
 088: 4.98E-02
 052: 1.20E-04

 C050: 2.40E-04
 NE13: 2.21E-04
 N861: 4.33E-07
 MG14: 1.95E-15
 MG63: 3.99E-10
 S135: 1.181E-04

 S19: 4.14E-06
 S34: 1.01E-04
 S11: 1.25E-07
 AR7: 7.88E-06
 AR9: 9.58E-06
 AR22:-2.43E-11
 AR13: 3.65E-09
 AR8: 1.91E-13

 CA3: 2.668E-08
 CA12: 3.41E-20
 CA4: 2.62E-11
 Ne14: 1.43BE-11
 Ne24: 3.91E-09
 S13: 1.00E-20
 S14: 1.00E-20
 Fe7: 1.00E-20

 Fe61: 1.00E-20
 Fe23: 1.00E-20
 Fe13: 1.00E-20
 S16: 5: 1.00E-20
 C610: 1.77E-05
 C370: 7.36E-04

 Old hydro optical depths: 1 4.63E-01 2 2.84E-04 3 1.16E-04 4 5.54E-05 Lines: 2-1 2.08E+04 3-2 1.87E-05 4-3 1.47E-11 5-4 1.48E-11 5 2.73E-05 6-5 1.71E-11 6 1.48E-05 7 5.02E-06 7-6 3.05E-11 8-7 1.00E-20 New hydro optical depths: 1 5.24E-01 2 3.09E-04 Lines: 2-1 2.25E+04 3-2 1.85E-05 3 1.26E-04 4 6.01E-05 4-3 1.44E-11 5-4 1.46E-11 5 2.96E-05 6-5 1.70E-11 6 1.61E-05 7 5.45E-06 7-6 3.04E-11 8-7 1.00E-20

 Old He Is optical depths:
 1 4.34E-01
 2 4.07E-04
 3 2.84E-18
 4 3.43E-18
 5 5.29E-18
 6 8.48E-18
 7 1.00E-20

 Lines:
 2-1 6.82E+03
 3-2 1.75E-06
 4-3 4.74E-12
 5-4 4.77E-12
 6-5 5.51E-12
 7-6 9.83E-12
 8-7 1.00E-20

 New HE Is optical depths:
 1 4.80E-01
 2 4.42E-04
 3 2.90E-18
 4 3.52E-18
 5 5.45E-18
 6 8.75E-18
 7 1.00E-20

 Lines:
 2-1 7.19E+03
 3-2 1.74E-06
 4-3 4.64E-12
 5-4 4.71E-12
 6-5 5.47E-12
 7-6 9.82E-12
 8-7 1.00E-20

 Old He II optical depths: 1 4.56E-01 2 4.63E-01 Lines: 2-1 1.75E+04 3-2 1.31E-08 New HE II optical depths: 1 4.97E-01 2 5.24E-01 Lines: 2-1 1.83E+04 3-2 1.30E-08 3 1.53E-20 4 1.64E-20 4-3 2.26E-15 5-4 2.27E-15 3 1.54E-20 4 1.66E-20 5 1.99E-20 6 2.58E-20 7 1.00E-20 6-5 2.61E-15 7-6 4.65E-15 8-7 1.00E-20 5 2.01E-20 6 2.63E-20 7 1.00E-20 6-5 2.59E-15 7-6 4.63E-15 8-7 1.00E-20 4-3 2.21E-15 5-4 2.23E-15 Hydrogen -1.031 -0.042 Helium -0.628 -0.129 -1.672 Log10 Mean Ionisation (over volume) Hellum -0.028 -0.129 -1.072 Carbon -1.852 -0.169 -0.512 -2.920 -4.593 Nitrogen -1.603 -0.066 -0.943 -2.654 Oxygen -0.912 -0.138 -0.827 -3.028 -6.065 Neon -1.231 -0.213 -0.490 -2.269 -5.921 Magnesium -1.345 -0.205 -0.483 -2.493 -5.870 -8.660-11.941 Aluminum -2.073 -0.100 -0.743 -1.788 -4.077 -8.054-11.423-14.981

Silicon -2.188 -0.028 -1.292 -2.307 -4.284 -7.822-11.129-14.641-18.281 Sulphur Argon Calcium Iron 13 14 15 16 17 Hydrogen -1.040 -0.042 Log10 Mean Ionisation (Helium -0.633 -0.128 -1.661 Carbon -1.661 -0.171 -0.507 -2.891 -4.588 Nitrogen -1.617 -0.069 -0.920 -2.618 Oxygen -0.925 -0.140 -0.806 -2.981 -5.932 Neon -1.239 -0.214 -0.486 -2.242 -5.787 Magnesium -1.351 -0.206 -0.481 -2.468 -5.736 -8.527-11.807 Aluminum -2.078 -0.101 -0.739 -1.789 -4.082 -7.920-11.289-14.847 Silicon -2.197 -0.030 -1.262 -2.293 -4.243 -7.688-10.995-14.507-18.147 Culabur -2.091 -0.166 -0.505 -2.099 -4.360 -7.029 -8.897-12.281-16.127-Log10 Mean Ionisation (over radius) -2.491 -0.166 -0.505 -2.999 -4.366 -7.029 -8.897-12.281-16.127-19.855-23.855 -2.269 -0.263 -0.352 -2.376 -4.386 -6.692 -8.929-10.760-13.296-17.288-21.364-25.477-29.672 -0.701 -0.169 -0.917 -2.562 -5.808 -2.721 -0.205 -0.513 -1.193 -2.549 -4.642 -7.911-10.623-13.683 Sulphur Argon Calcium Iron 0.5-1.0KEV:1.09E+06 1.0-1.5:2.19E+05 1.5-2.0:7.17E+04 2.0-2.5:3.41E+04 2.5-3:2.04E+04 3-5:2.65E+04 5-7.5:8.59E+03 7.5-10:3.19E+03 Normalised continuum 0.25 1.038 0.27 0.997 0.30 0.997 0.33 0.998 0.36 0.999 0.39 0.999 0.43 1.000 0.47 1.002 0.51 1.003 0.56 1.005 0.62 1.006 0.67 1.006 0.74 0.998 0.81 0.995 0.88 0.994 0.97 0.994 0.98 0.994 0.99 0.994 1.00 0.994 Inward continua (nuFnu) at head of Balmer, Lyman series: 1.24E-03 2.84E-06 Outwrd continua (nuFnu) at head of Balmer, Lyman series; 1.04E-03 0.00E+00 Emergent continuum - phot/ryd/cm2 (r in) mergent continu 17.3 7.74E+05 19.5 5.43E+05 22.0 3.78E+05 24.8 2.65E+05 27.9 1.86E+05 31.5 1.29E+05 m - phot/ryd/cm2 75.3 9.54E+03 81.6 7.52E+03 88.3 5.92E+03 95.7 4.67E+03 103.7 3.68E+03 112.3 2.90E+03 0.26 1.71E+11 1.00 2.24E+09 0.29 1.51E+11 1.01 2.21E+09 0.33 1.12E+11 1.02 2.18E+09 0.37 7.81E+10 1.10 1.89E+09 3.9 5.06E+07 4.0 3.42E+07 4.2 3.59E+07 4.7 2.81E+07 1.26E+03 2.09E+00 1.87E+03 6.37E-01 2.78E+03 1.94E-01 4.14E+03 5.94E-02 3.24E+05 1.28E-07 4.81E+05 3.90E-08 7.15E+05 1.19E-08 1.06E+06 3.64E-09 4.7 2.81E+07 5.3 2.12E+07 5.9 1.73E+07 6.7 1.25E+07 7.5 8.92E+06 8.5 6.35E+06 9.5 4.51E+06 10.8 3.18E+06 12.1 2.24E+06 13.6 1.57E+06 15.4 1.10E+06 0.42 5.46E+10 0.47 3.82E+10 1.24 1.48E+09 1.40 1.17E+09 6.15E+03 1.81E-02 9.15E+03 5.54E-03 1.58E+06 1.11E-09 2.35E+06 3.39E-10 112.3 2.90E+03 121.6 2.28E+03 131.7 1.80E+03 142.7 1.41E+03 173.8 7.85E+02 258.3 2.40E+02 383.9 7.32E+01 570.6 2.24E+01 9.15E+03 5.54E=03 1.36E+04 1.69E=03 2.02E+04 5.16E=04 3.00E+04 1.58E=04 0.53 2.68E+10 0.60 1.87E+10 1.57 9.37E+08 1.78 5.97E+08 35.5 9.03E+04 40.0 6.21E+04 3.49E+06 3.19E=10 5.19E+06 3.17E=11 0.67 1.31E+10 2.00 3.32E+08 45.0 4.38E+04 50.5 3.12E+04 54.7 2.47E+04 59.2 1.95E+04 64.2 1.53E+04 0.76 9.04E+09 2.25 2.27E+08 2.54 1.71E+08 4.46E+04 4.81E-05 6.63E+04 1.47E-05 0.86 6.31E+09 0.97 4.40E+09 0.99 4.13E+09 2.86 1.06E+08 3.22 7.95E+07 9.86E+04 1.47E-05 9.86E+04 4.49E-06 1.47E+05 1.37E-06 2.18E+05 4.19E-07

69.5 1.21E+04

848.1 6.83E+00

0.99 4.03E+09

3.63 6.03E+07

CLOUDY 80.08

**************************************	*****
*	*
* title Martin Gaskell's funny model	*
* c used to test that electron density convergence is ok	*
* c hydrogen line spectrum strongly pumped by continuum	*
* black 4000	*
Is T(star) = 4.00E+03 correct???	
* lumin 27.2	*
* constant temper 5500	*
* faint -3	*
* radius 15	*
* hden 5.13	*
* abundances 1000 1000 1000 1000 1000 1000 1000 10	*
* continue 1000 1000 1000 1000 1000 1000	*
Is a helium abundance of 9.800E+01 reasonable?	
Is an abundance of 3.630E-01 for element 2 reasonable?	
Is an abundance of 1.120E-01 for element 3 reasonable?	
Is an abundance of 8.510E-01 for element 4 reasonable?	
Is an abundance of 1.230E-01 for element 5 reasonable?	
* stop zone 1	*
* print short	*
* drmax 0	*
* drmin 0	*
* c eden.in	*
* c cray	*
*	*
*****	*******
Chemical composition	

He:**** C:3.63E-01 N:1.12E-01 O:8.51E-01 Ne:1.23E-01 Mg:3.80E-02 Al:3.0E-03 Si:3.55E-02 S:1.62E-02 A:3.6E-03 Ca:2.3E-03 Fe:4.68E-02

263Cell Peak9.90E-02	Lo 1.00E-05=0.9105cm	Hi-Con:1.80E+00 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 27.2025	Average nu:1.027E+00	P(X-ray): 0.0000	P(BalC): 38.3567	Q(Balmer C): 49.5708
Q(1.0-1.8): 37.8529	Q(1.8-4.0): 0.0000	Q(4.0-20): 0.0000	Q(20): 0.0000	Ion pht flx:5.671E+06
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): 40.3304	Alf(ox): 0.0000	Total lumin: 40.3350
L/Lsolar: 6.7522	Abs bol mg: -12.1605	Abs V mag: -11.3684	Bol cor: -0.7921	nuFnu(Bbet): 39.7854
U(1.0):1.402E-09	U(4.0):0.000E+00	T(En-Den):1.660E+03	T(Comp):3.835E+03	nuJnu(912A):4.627E-03
Occ(FarIR):7.124E+01	Occ(H n=6):1.460E-02	Occ(1Ryd):2.105E-19	Occ(4R):0.000E+00	Occ (Nu-hi):1.270E-32
Tbr(FarIR):1.185E+02	Tbr(H n=6):6.481E+01	Tbr(1Ryd):3.325E-14	Tbr(4R):0.000E+00	Tbr (Nu-hi):3.542E-27

##### 1 Te:5.500E+03 Hden:1.349E+05 Ne:4.0	652E+04 R:1.000E+15 R-R0:5.000)E-01 dR:1.000E+00 NTR: 1 Htot	2:9.513E-16 T912: 1.092E-12###
-15.90 4686 0.00 5876 0.00 1909 0.00 154	49 0.00 6584 6.84 5007 0.00) 3727 1.10 6300****** 2798***	*** 1035 0.00
Hydrogen 9.985E-01 1.497E-03 H+0/Hden:	1.000E+00 6.383E-15 H- H2	1.326E-11 6.545E-11 H2+ HeH+	1.284E-09 H col den 1.349E+05
H 2SP 3-6 1.006E-10 1.685E-11 8.938E-14	1.809E-14 1.040E-14 8.650E-15	Texc(La); 3.650E+03 T(contn):	1.660E+03 T(diffs): 3.049E+01
Helium 1.000E+00 0.000E+00 0.000E+00 H	He I 2S3 0.000E+00 Comp H, C	1.371E-16 1.967E-16 Fill Fact	1.000E+00 Gam 1/tot 8.289E-01
He singlet 0.000E+00 0.000E+00 0.000E+00 (0.000E+00 0.000E+00 0.000E+00	He triplt 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00
HeII 0.000E+00 0.000E+00 0.000E+00 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	PRAD/GAS; 4.434E-07
Pressure NgasTgas; 7.489E+10 P(total):	1.034E-05 P(gas): 1.034E-05	P(Radtn): 4.584E-12 Rad accel	1.890E-05 Force Mul 1.002E+00
Carbon 4.473E-01 5.527E-01 0.000E+00 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 H2O+/Otot 0.000E+00	OH+/Ototl 0.000E+00
Nitrogen 9.985E-01 1.454E-03 0.000E+00 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 02/Ototl:	0.000E+00 O2+/Otot: 0.000E+00
Oxygen 9.987E-01 1.306E-03 0.000E+00 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	Hex(tot): 0.000E+00 A:-12.258
Neon 1.000E+00 8.137E-13 0.000E+00 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00
Magnesium 0 7.100E-04 9.993E-01 6.772E-07 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00
Aluminium 0 1.115E-06 1.000E+00 7.487E-12 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00
Silicon 0 1.471E-04 9.999E-01 1.862E-06 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00
Sulphur 0 1.445E-02 9.856E-01 4.763E-16 (0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00

Argon 0 1.000E+00 2.885E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calcium 0 7.089E-05 9.992E-01 7.586E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calculation stopped because NZONE reached.
Geometry is plane-parallel.
IThe largest continuum occupation number was 7.124E+01 at 1.053E-05 Ryd.
W-Heating - cooling mismatch = 2.00E+00 Whats wrong???
Continuum occupation number reached 4.95E+00 for some fine structure transitions.
Induced recombination was 1.7% of the total for H level 7
Stimulated emission was 8.1% of the total for H level 7
Stimulated enisy of radiation field was greater than the Compton temperature. Is this physical?
Frequency out of range of free-free gaunt factor routine.
H- absorption heating was 3.7% of the total.
C-The Lyman continuum is thin, and I assumed that it was thick. Try another iteration.

	********	*********	*******	**> CLOUD	Y 80.08	3 <	<***	******	*******	****	****	**	
	* title Mart	in Gaskell's	funny m	odel								*	
* c used to test that electron density convergence is ok											*		
* c hydrogen line spectrum strongly pumped by continuum											*		
* black 4000											*		
	* lumin 27.2											*	
	* constant t	emper 5500										*	
	* faint -3	-										*	
* radius 15											*		
* hden 5.13												*	
* abundances 1000 1000 1000 1000 1000 1000 1000 10											*		
	* stop zone	1										*	
	* print shor	t										*	
	* drmax 0											*	
	* drmin 0											*	
	* c eden.in											*	
	* c cray											*	
	*******	*********	*******	<pre>*> LOG(U)</pre>	: -8.85	5 <*	* * * * *	******	**********	****	****	**	
	>>>>>> W	arnings exis	t, this	calculati	on is s	susp	pect.						
	>>>>>> A	nother itera	tion is	suggested									
Er	nission Line	Spectrum. Luminosity								ion	1 0	f 1.	
.198	1.0000	TOTL 938		0.2299				13.755		-		6731	
	*******	INWD 1216				_		13.269		-		6716	
.078	7.5730	Dest 1216						12.283				4070	
.489	0.0195	e sc18751	12.268	0.0012				12.988			II	4078	1
.746	0.0035	nFnu 4860	16.152	8.9969	0	1 6	6300	18.6903	3099.8769	S	II1	0323	1
.999	6.3244	Inci 4861	39.786**	******	0	1 6	6363	18.2131	033.2923	S	II1	0289	1

TOTL 4861	15.198 1.0000	TOTL 938	14.560 0.2299	N 2 5755 13.755 0.0360	S II 6731 18.073 748.6573
TOTL 1216	19.766*******	INWD 1216	19.766*******	N 2 122 13.269 0.0118	S II 6716 17.723 334.8413
TotH 0	16.078 7.5730	Dest 1216	15.467 1.8545	N 2 203 12.283 0.0012	S II 4070 17.989 617.1406
BFH1 0	13.489 0.0195	e sc18751	12.268 0.0012	N 2 2140 12.988 0.0062	S II 4078 17.499 199.6309
BFHx 0	12.746 0.0035	nFnu 4860	16.152 8.9969	O 1 6300 18.6903099.8769	S II10323 17.486 193.7774
TotM 0	15.999 6.3244	Inci 4861	39.786*******	0 1 6363 18.2131033.2923	S II10289 17.357 143.9799
FF H 0	12.505 0.0020	Inci 1216	32.551*******	0 1 5577 15.930 5.3953	S II10373 17.028 67.6201
ComH 0	15.236 1.0917	BAC 0	13.948 0.0562	0 1 630 18.033 683.1214	S II10339 17.348 141.3086
н-н 0	14.318 0.1318	PAC 0	13.457 0.0181	0 1 1470 16.489 19.5166	Ar 2 7 13.301 0.0127
CA B 4861	13.395 0.0157	HFF 0	13.178 0.0095	0 1 7774 13.715 0.0329	Ca 2 3933 18.037 689.5098
CA B 1216	14.909 0.5132	ComC 0	15.393 1.5658	T OI 0 13.761 0.0366	Ca 2 8579 16.465 18.4953
DU B 4861		HFB 0	13.583 0.0242	6lev 1304 13.761 0.0365	Ca 2 7306 19.0577231.0594
Q(H) 4861	25.530*******	Cool 1216	13.317 0.0131	TOTL 3727 15.239 1.0993	Ca2K 3934 17.852 450.4940
Q(H) 1216	27.063*******	H-FB 0	14.449 0.1783	TOTL 7325 14.424 0.1681	Ca2H 3969 17.577 239.0158
TOTL 6563	16.481 19.1627	MeFB 0	15.779 3.8043	O II 3729 14.614 0.2602	Ca2X 8498 15.285 1.2202
TOTL 4861	15.198 1.0000	MeFF 0	15.544 2.2182	O II 3726 15.122 0.8390	Ca2Y 8542 16.243 11.0833
TOTL 4340	14.485 0.1935	Toff 0	15.546 2.2277	O II 2471 14.322 0.1329	Ca2Z 8662 15.990 6.1918
TOTL 4102	14.014 0.0655	REC 1656	16.621 26.4660	O II 7323 14.166 0.0927	CaF1 7291 18.8324298.5488
TOTL18751	14.641 0.2769	C I 9850	18.7223340.5012	O II 7332 14.075 0.0753	CaF2 7324 18.6662932.5105
TOTL12818	13.954 0.0570	C 1 8727	17.998 630.3314	Mg 1 4571 13.759 0.0364	Fe 2 48 13.801 0.0401
TOTL10938	13.491 0.0196	C 1 610	13.415 0.0165	Emis 2798 18.2271067.7718	Fe 2 7 18.6442792.1011
TOTL40512	13.543 0.0221	C 1 370	14.313 0.1303	Cool 2798 18.2271067.7718	Emis 3 18.123 841.0212
TOTL26252	13.107 0.0081	C 2 158	16.101 8.0019	Si 2 35 17.756 361.0007	Cool 3 18.123 841.0212
TOTL74578	12.777 0.0038	C 2 2326	16.985 61.1770	Si 2 2335 16.508 20.3813	TOT 0 18.7593633.1624
2 NU 0	13.536 0.0217	C 2 1335	13.879 0.0479	Si 2 1808 14.769 0.3724	FEIR 0 18.6062555.5387
TOTL 1216	19.766*******	N 1 5200	17.117 82.8697	S 1R 1807 14.987 0.6143	Fe 3 0 13.324 0.0134
TOTL 1026	16.938 54.9398	REC 5200	12.415 0.0016	S 2 6720 18.2331083.4986	Fe 3 5270 12.644 0.0028
TOTL 973	15.711 3.2593	N 2 6584	16.033 6.8367	S 2 4074 18.110 816.7716	Fe 3 4658 12.888 0.0049
TOTL 950	15.020 0.6632	N 2 6548	15.556 2.2789	S 210330 17.936 546.6860	

M Cooling: C I 9850:0.123 O Heating: TotM 0:0.835 Com		TOT 0:0.134	FEIR 0:0.094		
IONIZE PARMET: U(1-) -8.8531	U(4-):-37.0000 U(sp): -8.85	Q(ion): 37.853	L(ion): 27.203	Q(low): 52.16	P(low) 40.33
ENERGY BUDGET: Heat: 16.078	Coolg: 19.631 Error:*****	Compt H: 15.236	WorkF: 17.632	F-F H 12.505	PRADMX:4.43E-07
Column density H12:1.349E+05	H II:2.019E+02 HI:1.347E+05	H-: 8.611E-10	H2: 1.789E-06	H2+:8.829E-06 1	He H+:1.732E-04
OH: 0.000E+00	Heff:0.000E+00				
<nh>:1.349E+05 <tp>:5.50E+03</tp></nh>	<to3>:0.00E+00 Ne:0.000E+00</to3>	ti(snd):3.02E-06	NeN+dl:9.39E+06	<t(c3)>:0.00E+00 ·</t(c3)>	<e(c3)>:0.00E+00</e(c3)>
He/Ha:0.00E+00 = 0.00*true	N/Oap:0.00E+00 = 0.00true	T(O3R):0.000E+00	L THIN:1.00E+30	<t(s2)>:5.50E+03 ·</t(s2)>	<e(s2)>:4.65E+04</e(s2)>
T He+:0.00E+00 EHe+:0.00E+00	T(O+):5.50E+03 EO+:4.65E+04	iter/zn: 1.000	Te-low:5.50E+03	Te-high:5.50E+03	Hlu/zn:1.00E+00
<a>:0.00E+00 erdeFe0.0E+00	Tcompt2.81E-02 Tthr4.50E+06	<tden>: 5.50E+03</tden>	<dens>:9.42E-17</dens>	<mol>:4.16E+00</mol>	
Mean Jeans l(cm)2.34E+17	M(sun)3.19E+02 smallest:	len(cm):2.34E+17	M(sun):3.19E+02	Alf(ox-tran):	0.0000

******	*******	******	*******	91Aug03**	******	*****	******	******
*				2				*
* title	test hydrogen	atom co	ntinuous	emissivit	У			*
* black	5				-			*
* ioniza	tion paramete	r -2						*
* sphere	static	; w	ant full	outward f	lux			*
* consta	nt temperatur	e 4						*
* abunda	nces -10	; P	oure hydro	ogen				*
* hden 7		;s	suppress t	wo-photon	emissio	on		*
* stop e	den 6	;s	stop model	L at H ion	ization	front		*
<pre>* print</pre>	short							*
* punch	emitted conti	nuum ;o	utput the	e predicte	d contir	nuum		*
* hydrog	en collisions	off						*
* c hemi	s.in							*
* c cray								*
*								*
******	**********	******	********	********	*******	*****	******	*************

Chemical composition He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 Al:1.0E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10

356Cell Peak2.46E+00	Lo 1.00E-05=0.9105cm	Hi-Con:2.30E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 5.1532	Average nu:2.177E+00	P(X-ray): -5.0583	P(BalC): 4.2200	Q(Balmer C): 15.0617
Q(1.0-1.8): 15.1279	Q(1.8-4.0): 15.1711	Q(4.0-20): 14.2441	Q(20): 4.2804	Ion pht flx:3.001E+15
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): 2.6360	Alf(ox): 0.0000	Total lumin: 5.2023
U(1.0):1.001E-02	U(4.0):5.851E-04	T(En-Den):1.628E+02	T(Comp):9.574E+04	nuJnu(912A):3.960E+04
Occ(FarIR):4.222E-07	Occ(H n=6):1.550E-10	Occ(1Ryd):1.827E-12	Occ(4R):1.261E-14	Occ (Nu-hi):2.090E-27
Tbr(FarIR):7.022E-07	Tbr(H n=6):6.882E-07	Tbr(1Ryd):2.886E-07	Tbr(4R):7.980E-09	Tbr (Nu-hi):7.463E-21

Pressure	NgasTgas;	1.105E+11	P(total):	1.546E-05	P(gas):	1.525E-05	P(Radtn):	2.075E-07	Rad accel	3.319E-05	Force Mul	1.480E+03
Carbon	2.426E-04	9.884E-01	1.136E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen	5.915E-02	9.407E-01	1.162E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/Ototl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9.287E-01	7.130E-02	1.247E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.588
Neon	1.092E-01	4.307E-01	4.601E-01	1.916E-05	0.000E+00							
Magnesium 0	1.962E-03	5.675E-01	4.305E-01	2.115E-05	0.000E+00							
Aluminium 0	2.434E-04	7.453E-01	1.805E-01	7.293E-02	1.086E-03	0.000E+00						
Silicon 0	1.048E-04	9.986E-01	1.196E-03	8.100E-05	0.000E+00							
Sulphur 0	3.091E-05	9.758E-01	2.422E-02	0.000E+00								
Argon 0	4.986E-01	4.487E-01	5.266E-02	0.000E+00								
Calcium 0	7.153E-04	1.975E-02	9.790E-01	5.201E-04	0.000E+00							
Iron 0	1.254E-02	9.795E-01	7.980E-03	0.000E+00								
Calculati	on stopped	because lo	owest EDEN	reached.								
Geometry	is plane-pa	arallel.										

Geometry is plane-parallel. Photoionization of He 2Tris reached 86.1 percent of the total rate out. W-A physical process has been disabled. W-Heating - cooling mismatch = 1.76E+00 Whats wrong???? Continuum occupation number reached 9.81E-01 for some fine structure transitions. C-I must iterate when SPHERE STATIC is set. Frequency out of range of free-free gaunt factor routine. The ratio of radiation to gas pressure reached 2.81E+01. Caused by Lyman alpha. C-This is the last iteration and H(a) optical depth changed by 91.3% (was 2.32E+01). Try another iteration

* title test hydrogen atom	continuous competitity	
* black 5		
 ionization parameter -2 		
* sphere static	;want full outward flux	
* constant temperature 4		
* abundances -10	;pure hydrogen	
* hden 7	;suppress two-photon emission	
* stop eden 6	stop model at H ionization front;	
* print short		
* punch emitted continuum	;output the predicted continuum	
* hydrogen collisions off		
* c hemis.in		
* c cray		
*******	******> LOG(U): -2.00 <***********************************	**
>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	this calculation is suspect.	
>>>>>>>> Another iterati		

Emission Line Spectrum. Constant Density Model. Closed geometry. Iteration 1 of 1. Intensity (erg/s/cm^2)

TOTL 4861	3.124	1.0000	Q(H) 1216	4.688	36.5957	TOTL74578	1.418	0.0197	BA C	0	3.798	4.7204
TOTL 1216	4.706	38.1728	TOTL 6563	3.621	3.1404	2 NU 0	2.193	0.1172	PA C	0	3.286	1.4492
TotH 0	4.895	58.9393	TOTL 4861	3.124	1.0000	TOTL 1216	4.706	38.1728	H FF	0	3.324	1.5849
BFH1 0	4.895	58.9290	TOTL 4340	2.851	0.5332	LA X 1216	1.341	0.0165	H FB	0	3.457	2.1525
BFHx 0	1.013	0.0077	TOTL 4102	2.633	0.3227	INWD 1216	4.706	38.1724	H-FB	0	0.580	0.0029
н-н 0	0.490	0.0023	TOTL18751	2.663	0.3454	Dest 1216	1.197	0.0118	H2+	0	0.227	0.0013
CA B 4861	3.174	1.1210	TOTL12818	2.361	0.1725	nFnu 4860	3.440	2.0707	TOFF	0	3.324	1.5849
CA B 1216	4.708	38.3170	TOTL10938	2.132	0.1018	nFnu 1215	1.456	0.0214				
DU B 4861	3.174	1.1210	TOTL40512	1.950	0.0670	Inci 4861	2.738	0.4107				
Q(H) 4861	3.154	1.0704	TOTL26252	1.748	0.0420	Inci 1216	4.328	15.9710				

Cooling: H FF Heating: BFH1	0:0.424 H F 0:1.000		M CONTINUOUS E	MISSIVITY			
IONIZE PARMET: ENERGY BUDGET:		U(4-): -3.2328		Q(ion): 11.624 Compt H: -2.239			P(low) 4.23 PRADMX:2.81E+01
Column density	Heat: 4.895 H12:1.411E+21						He H+:2.392E+04
corumn density	OH: 0.000E+00	Heff:0.000E+00	HI:1.601E+20	H=: 3.455E+12	H2: 3.303E+13	H2+:1.301E+12	He H+:2.392E+04
<nh>:1.000E+07</nh>	<tp>:1.00E+04</tp>	<to3>:1.00E+04</to3>	Ne:9.852E+06	ti(snd):1.13E+08	NeN+dl:1.20E+28	<t(c3)>:1.00E+04</t(c3)>	<e(c3)>:9.58E+06</e(c3)>
He/Ha:5.18E-11	= 0.52*true	N/Oap:0.00E+00	= 0.00true	T(O3R):1.000E+01	L THIN:1.00E+30	<t(s2)>:1.00E+04</t(s2)>	<e(s2)>:4.49E+06</e(s2)>
T He+:1.00E+04	EHe+:7.28E+06	T(O+):1.00E+04	EO+:7.13E+06	iter/zn: 1.000	Te-low:1.00E+04	Te-high:1.00E+04	Hlu/zn:1.41E+00
<a>:0.00E+00	erdeFe0.0E+00	Tcompt3.52E+01	Tthr1.00E+06	<tden>: 1.00E+04</tden>	<dens>:1.66E-17</dens>	<mol>:5.41E-01</mol>	
Mean Jeans	l(cm)1.61E+18	M(sun)1.84E+04	smallest:	len(cm):1.61E+18	M(sun):1.84E+04	Alf(ox-tran):	0.0000

	***********************************91Auq03************************************	* *
	k	*
	* title high electron density approach to lte	*
,	* c test from Ferland and Rees 88, collisions drive H to LTE	*
,	* c collisions should drive all departure coef to unity	*
	* constant temperature = 50,000	*
,	* print departure coefficients	*
,	* stop zone 1	*
	* stop lyman optical depth -6	*
	* black body t=50,000	*
,	* ionization parameter -5	*
	* hden = 19	*
,	* abundances -10	*
	* iterate	*
1	* print last short	*
,	* drmax 0	*
1	* drmin 0	*
,	* c highn.in	*
1	* c cray	*
	k la	*
	***************************************	**

Is this value of the H-density reasonable?

He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 Al:1.0E-10 S:1.00E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10

Chemical composition

333Cell Peak1.24E+00 Lo	o 1.00E-05=0.9105cm Hi-Co	on:1.16E+01 Ryd E(h	i):7.35E+06Ryd E	(hi): 100.01 MeV	
P(nu>1ryd): 13.9889 Ave	verage nu:1.491E+00 P(X-	-ray): 0.0000 P(B	BalC): 13.8421 Q	Balmer C): 24.7181	
Q(1.0-1.8): 24.3840 Q(1	(1.8-4.0): 23.7615 Q(4.0	0-20): 21.3654 Q(2	0.0000 I	on pht flx:3.001E+24	
L(gam ray): 0.0000 Q(d	(gam ray): 0.0000 L(Inf	Ered): 12.4994 Alf	(ox): 0.0000 T	otal lumin: 14.2308	
U(1.0):1.001E-05 U(4	(4.0):7.736E-09 T(En-	-Den):2.943E+04 T(C	comp):4.812E+04 n	Jnu(912A):1.157E+14	
Occ(FarIR):3.607E+03 Occ	cc(H n=6):1.295E+00 Occ(1			c (Nu-hi):2.802E-17	
			(4R):2.435E-01 T	or (Nu-hi):5.037E-11	
##### 1 Te:5.000E+04 Hden:1.000E+19					#
	0.00 1549 0.00 6584 0.00				
	0/Hden: 1.000E+00 4.712E-06			4.439E-18 H col den 1.000E+1	.9
	0/Hden: 1.000E+00 9.996E-01			He H+ 4.439E-18	
			4.994E+04 T(contn):	2.793E+04 T(diffs): 2.864E+0	4
	000E+00 1.000E+00 1.000E+00				
				1.000E+00 Gam 1/tot 2.897E-0	
				1.000E+00 Gam 1/tot 2.897E-0	
				3.884E-04 1.090E-03 1.792E-0	
He singlet 1.042E+00 1.010E+00 1.00					/1
	029E-04 9.902E-05 1.164E-04				
				1.000E+00 PRAD/GAS; 4.051E-0	
				5.583E+07 Force Mul 2.572E+0	4
	221E-01 2.028E-04 0.000E+00				
				0.000E+00 O2+/Otot: 0.000E+0	
				Hex(tot): 0.000E+00 A:-12.98	3
	519E-01 0.000E+00 0.000E+00				
Magnesium 0 3.143E-06 9.884E-03 9.90	901E-01 0.000E+00 0.000E+00	0 0.000E+00 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+0	0
Aluminium 0 3.837E-05 9.218E-02 7.16	162E-01 1.916E-01 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+0	0
Silicon 0 1.036E-04 2.126E-01 7.53	539E-01 3.339E-02 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+0	10
Sulphur 0 2.037E-05 1.079E-01 8.82	826E-01 9.429E-03 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+0	10

Argon 0 4.921E-05 9.993E-02 8.989E-01 1.113E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calculation 0 4.675E-05 4.540E-02 8.963E-01 5.826E-02 1.851E-05 0.000E+00 0.00E+00 0.000E+00 0.00E+00 0.00E+0

TotH	0 13.242	729.6163	TOTL10938	9.304	0.0841	Strk 1216	12.359	95.5367	H FF 0	13.5811590.9079
BFH1	0 12.612	170.9720	TOTL40512	9.104	0.0531	Strk 6563	10.761	2.4088	HFB 0	13.6451843.3791
BFHx	0 12.711	214.8266	TOTL26252	8.894	0.0328	Strk 4861	10.355	0.9468	Hind 0	12.120 55.1043
FF H	0 12.913	342.2061	TOTL74578	8.560	0.0152	Strk18751	9.797	0.2621	Cool 1216	13.161 605.3822
н- н	0 10.586	1.6108	TOTL 1216	12.375	99.0903	Strk40512	9.103	0.0530	Crst 960	11.437 11.4252
CA B 486	1 12.362	96.1266	TOTL 1026	10.530	1.4145	Dest 1216	10.485	1.2753	Cool 6563	12.789 257.1106
CA B 121	6 13.963	3840.0487	TOTL 973	11.325	8.8350	Dest 6563	9.926	0.3528	Crst 4861	12.286 80.7343
DU B 486	1 12.358	95.3853	TOTL 950	11.103	5.2945	Dest40516	9.163	0.0608	Cool18751	13.032 449.8266
Q(H) 486	1 12.154	59.5680	TOTL 938	10.976	3.9570	Dest 4861	9.947	0.3702	Crst 0	12.017 43.5010
Q(H) 121	6 13.688	2036.6283	C13c 6563	11.990	40.8341	Dest18751	9.491	0.1294	H-FB 0	11.311 8.5443
TOTL 656	3 10.764	2.4294	C14c 4861	10.832	2.8403	nFnu 4860	13.259	758.2635	H2+ 0	10.909 3.3890
TOTL 486	1 10.379	1.0000	CION 0	13.7772	2498.6938	nFnu 1215	13.367	972.2584	Toff 0	13.5811590.9079
TOTL 434	0 10.113	0.5426	INWD 1216	12.057	47.6666	Inci 4861	12.600	166.5390	Mion 0	7.735 0.0023
TOTL 410	2 9.936	0.3606	INWD 6563	10.446	1.1670	Inci 1216	13.9303	3557.6206		
Lines with ne	gative i	ntensities;	255 Ne 2 1	28 361	Ar 2 7	389 Ca 4 32	2			

Cooling: CION Heating: BFH1	0:0.324 H FF 0:0.206	ENSITY APPROACH I FB 0:0.239 FF H 0:0.469		Cool18751:0.058	
IONIZE PARMET:	U(1-) -4.9996 U(4-): -8.111	5 U(sp): -5.00	Q(ion): 24.337	L(ion): 13.870 Q(low): 24.68	P(low) 13.81
ENERGY BUDGET:	Heat: 13.242 Coolg: 14.26	Error:957.9%	Compt H: 4.545	WorkF: 16.239 F-F H 12.913	PRADMX:4.05E-08
Column density	H12:1.000E+19 H II:9.553E+1	B HI:4.472E+17	H-: 4.712E+13	H2: 2.359E+12 H2+:7.176E+10	He H+:4.439E+01
-	OH: 0.000E+00 Heff:0.000E+0)			
<nh>:1.000E+19</nh>	<tp>:5.00E+04 <to3>:5.00E+04</to3></tp>	Ne:9.553E+18	ti(snd):3.51E-07	NeN+dl:9.13E+37 <t(c3)>:5.00E+0</t(c3)>	4 <e(c3)>:9.55E+18</e(c3)>
He/Ha:1.34E-08	= 134.41*true N/Oap:0.00E+0) = 0.00true	T(O3R):1.000E+01	L THIN:1.00E+30 <t(s2)>:5.00E+0</t(s2)>	4 <e(s2)>:9.55E+18</e(s2)>
T He+:5.00E+04	EHe+:9.55E+18 T(O+):5.00E+0	EO+:9.55E+18	iter/zn: 1.000	Te-low:5.00E+04 Te-high:5.00E+0	4 Hlu/zn:1.00E+00
<a>:0.00E+00	erdeFe0.0E+00 Tcompt1.72E-2) Tthr5.99E-07	<tden>: 5.00E+04</tden>	<dens>:1.66E-05 <mol>:5.11E-01</mol></dens>	
Mean Jeans	l(cm)4.80E+12 M(sun)4.84E-0	smallest:	len(cm):4.80E+12	M(sun):4.84E-01 Alf(ox-tran):	0.0000

*	
*	title test of H ionization is optically thin limit
*	c H cross section is 2.09E-18 cm^2, rec coef is 4.18E-14
*	c answer is neutral fraction 2.00E-4
*	laser 1.5 Ryd
*	phi(h) 10
*	hden 1
*	constant temperature = 4
*	iterate
*	stop zone 1
*	abundances -10
*	drmax 0
*	drmin 0
*	print last
	print short
*	c hion.in
*	c cray
*	

Chemical composition He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 Al:1.0E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10

263Cell Peak1.53E+00 Lo 1.00E-05=0.9112cm Hi-Con:1.81E+00 Ryd E(hi):7.35E+06Ryd E(hi): 100.01 MeV P(nu>1ryd): -0.4860 Average nu:1.499E+00 P(X-ray): 0.0000 P(BalC): -30.0000 Q(Balmer C): -24.2981 Q(1.0-1.8): 10.0000 Q(1.8-4.0): 0.0000 Q(4.0-20): 0.0000 Q(20): 0.0000 Ion pht flx1.000E+10 L(gam ray): 0.0000 Q(1.0): 0.0000 Q(1.0): 0.0000 T(chred): -36.3400 Alf(ox): 0.0000 Total lumin: -0.4860 U(1.0):3.336E-02 U(4.0): 0.000E+00 T(En-Den):6.160E+00 T(Comp):5.918E+04 nuJnu(912A):1.462E-35 Occ(FarIR):6.090E-42 Occ(H n=6):8.5379E-49 Occ(IRyd):6.746E-52 Occ(Au:4.206E-53 Occ (Nu-hi):2.136E-52 Tbr(FarIR):1.012E-41 Tbr(H n=6):3.791E-45 Tbr(IRyd):1.066E-46 Tbr(4R):2.661E-47 Tbr (Nu-hi):5.996E-47
1 Te:1.000E+04 Hden:1.000E+01 Ne:9.998E+00 R:1.000E+25 R-R0:5.000E-01 dR:1.000E+00 NTR: 1 Htot:4.502E-22 T912: 2.246E-20###
-23.24 4686 0.00 5876 0.00 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00
Hydrogen 1.980E-04 9.998E-01 H+0/Hden: 1.000E+00 1.744E-12 H- H2 5.832E-14 2.441E-12 H2+ HeH+ 1.418E-22 H col den 1.000E+01
H 2SP 3-6 5.869E-14 2.684E-21 8.734E-21 1.672E-20 2.880E-20 4.538E-20 Texc(La); 2.962E+03 T(contn): 6.160E+00 T(diffs): 3.936E+02
Helium 1.000E+00 0.000E+00 0.000E+00 He I 2S3 0.000E+00 Comp H, C 8.672E-29 1.465E-29 Fill Fact 1.000E+00 Gam 1/tot 9.999E-01
He singlet 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 He triplt 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
HeII 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 PRAD/GAS; 1.395E-06
Pressure NgasTgas; 2.000E+05 P(total): 2.761E-11 P(gas): 2.761E-11 P(Radtn): 3.852E-17 Rad accel 2.733E-09 Force Mul 6.265E+02
Carbon 1.431E-04 9.999E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 H2O+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 9.720E-05 9.999E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/0totl: 0.000E+00 02/0totl: 0.000E+00 02/0totl: 0.000E+00 02/0totl: 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/0totl: 0.000E+
Oxygen 5.674E-05 9.999E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.380
Neon 6.480E-04 9.994E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 3.916E-05 6.186E-03 9.938E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 5.605E-05 1.771E-02 9.822E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Silicon 0 4.281E-06 5.654E-03 9.943E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Sulphur 0 2.136E-04 9.998E-01 2.068E-09 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Argon 0 3.433E-05 1.000E+00 0.000E+00
Calcium 0 3.794E-03 2.941E-02 9.668E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Iron 0 1.641E-05 1.343E-02 9.866E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calculation stopped because NZONE reached.
Geometry is plane-parallel.
W-Heating - cooling mismatch = 1.51E+00 Whats wrong???

Geometry is plane	-pararrer.			
W-Heating - cooling	mismatch =	1.51E+00	Whats	wrong???

Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2)

				s ,			
TOTL 4861-23.240	1.0000	TOTL 4861-23.240	1.0000	TOTL 1216-21.759	30.2723	e sc40512-24.418	0.0664
TOTL 1216-21.759	30.2723	TOTL 4340-23.477	0.5797	TOTL 1026-22.094	14.0095	nFnu 4860-22.473	5.8554
TotH 0-21.347	78.3174	TOTL 4102-23.670	0.3717	TOTL 973-22.392	7.0539	nFnu 1215-24.626	0.0412
BFH1 0-21.347	78.3173	TOTL18751-23.798	0.2769	TOTL 950-22.623	4.1480	BA C 0-22.283	9.0724
CA B 4861-22.907	2.1544	TOTL12818-24.008	0.1708	TOTL 938-22.812	2.6791	PA C 0-22.796	2.7853
CA B 1216-21.373	73.6431	TOTL10938-24.193	0.1115	INWD 1216-21.862	23.8954	H FF 0-22.757	3.0461
DU B 4861-22.907	2.1544	TOTL40512-24.419	0.0663	INWD 6563-23.235	1.0134	H FB 0-22.349	7.7882
Q(H) 4861 -2.323	*****	TOTL26252-24.578	0.0460	INWD 4861-23.542	0.5000	Cool 1216-25.145	0.0125
Q(H) 1216 -0.789*	*****	TOTL74578-24.907	0.0215	INWD18751-24.099	0.1384	Toff 0-22.757	3.0461
TOTL 6563-22.934	2.0267	2 NU 0-22.103	13.7278	e sc18751-23.798	0.2771		

Cooling: H FF Heating: BFH1	л 0:0.281 Н F 0:1.000	CEST OF H IONIZAT B 0:0.718	ION IS OPTICAL	LY THIN LIMIT			
IONIZE PARMET: ENERGY BUDGET:	U(1-) -1.4768 Heat: -21.347	U(4-):-37.0000		Q(ion): 10.000 Compt H: -28.062		Q(low):-19.29 F-F H-27.335	P(low)-30.03 PRADMX:7.50E-04
Column density		H II:9.998E+00 Heff:0.000E+00	HI:1.980E-03			H2+:2.441E-11	He H+:1.418E-21
<nh>:1.000E+01</nh>	<tp>:1.00E+04</tp>	<to3>:0.00E+00</to3>	Ne:0.000E+00	ti(snd):7.76E-07	NeN+dl:1.00E+02	<t(c3)>:0.00E+00</t(c3)>	<e(c3)>:0.00E+00</e(c3)>
He/Ha:0.00E+00	= 0.00*true	N/Oap:0.00E+00	= 0.00true	T(O3R):0.000E+00	L THIN:1.00E+30	<t(s2)>:1.00E+04</t(s2)>	<e(s2)>:1.00E+01</e(s2)>
T He+:0.00E+00	EHe+:0.00E+00	T(O+):1.00E+04	EO+:1.00E+01	iter/zn: 1.000	Te-low:1.00E+04	Te-high:1.00E+04	Hlu/zn:1.00E+00
<a>:0.00E+00	erdeFe0.0E+00	Tcompt1.50E+13	Tthr6.64E+11	<tden>: 1.00E+04</tden>	<dens>:1.66E-23</dens>	<mol>:5.00E-01</mol>	
Mean Jeans	l(cm)2.17E+21	M(sun)4.47E+07	smallest:	len(cm):2.17E+21	M(sun):4.47E+07	Alf(ox-tran):	0.0000

	*
title thermal equil black body limit from Ferland and Rees 1988	*
c this tests whether thermal processes go to lte	*
stop zone 1	*
hden 10	*
stop lyman optical depth -6	*
black body, t=50,000 lte	*
abundances -10	*
print departure coef	*
print last short	*
iterate	*
drmax 0	*
drmin 0	*
c hlte.in	*
c cray	*
	*

 Her.000 C11.00E-10 Nil.00E-10 Nil.00E-10 Nell.00E-10 Ngl1.00E-10 Nil.00E-10 Sil.00E-10 Ail.0E-10 Cil.0E-10 Fell.00E-10 333Cell Peakl.24E+00 Lo 1.00E-05-0.9105cm Hi-Conil.16E+01 Ryd E(hi): 7.35E+06Ryd E(hi): 100.01 MeV P(nuDiryd): 14.9097 Average nuil.491E+00 F(X-ray): 0.0000 P(BalC): 14.7629 (Balmer C): 25.6389 Q(1.0-1.6): 25.3046 Q(1.8-4.0): 24.6823 Q(4.0-20): 22.2662 Q(20): 0.0000 Ion pht fix:2.301E+25 L(gam ray): 0.0000 (Gqm ray): 0.0000 L(Infred): 10.420 Alf(Co): 14.7629 (Galmer C): 25.6389 Q(1.0-1.6): 25.3046 Q(1.8-4.0): 24.6823 Q(4.0-20): 22.2662 Q(20): 0.0000 Ion pht fix:2.351E+25 L(gam ray): 0.0000 (Gqm ray): 0.0000 L(Infred): 10.420 Alf(Co): 4.0000 Ion pht fix:2.351E+25 U(ray): 0.0000 (Gqm ray): 0.0000 L(Infred): 10.002+00 Alf(20): 4.0000 Ion pht fix:2.351E+16 Tbr(FarIR): 4.999E+04 Tbr(H =6): 4.791E+04 Tbr(Hyd): 7.020E+03 Tbr(A): 2.027E+06 Occ (Nu-hi): 4.197E-10 #### 1 Te: 5.038E+04 Hden: 1.000E+10 Ne: 1.000E+10 R: 1.000E+25 R-R0: 5.000E-01 dk: 1.000E+00 NTK: 1 Htot: 4.290E-04 T912: 5.527E-19### -5.60 4666 0.00 5876 0.00 1909 0.00 1549 0.00 6584 0.00 2326 0.00 3727 0.00 6300 0.00 2789 0.00 1035 0.00 Hydrogen 1.030E+00 Hu/Hden: 1.000E+10 8.262E-24 H H2 2.435E-31 L867E-24 H H2 4.2433E+11 H col den 1.000E+10 Hydrogen 1.030E+00 Hu/Hden: 1.000E+00 8.96EE-01 H H2 3.297E+01 H2+ 5.665E+08 H H= 4.2433E+14 H 25P 3-6 1.110E+00 Hu/Hden: 1.020E+01 1.016E+00 1.01E+00 Heilim 0.276E-18 1.207E+07 1.000E+00 He I 233 1.667E-18 1.07H H2 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 Heilim 1.182E+00 1.158E+00 1.002E+00 He I 233 2.669E+00 Com H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 Heilim 1.182E+00 1.027E+00 1.062E+00 He I 233 2.669E+00 Com H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 Heilim 1.182E+00 1.027E+01 1.042E+09 3.248E+19 4.2458E+19	Chemical composition									
P[nu>lryd]: 14.9097 Average nu:1.491E+00 P(X-ray): 0.0000 P[aic): 14.7629 O[ainer C]: 25.6389 G(1.0-1.8): 25.3048 O(1.8-4.0): 24.6623 O(4.0-20): 22.2862 O(20-1): 0.0000 Inp H flx:2.501E+25 U(1.0):8.341E+04 U(4.0):8.441E+04 Occ(H n=6):1.079E+01 T(Comp):4.445E+02 Occ (A):1.207E+06 Occ (Nu-hi):2.335E+16 Tbr(FarIR):4.999E+04 Occ(H n=6):4.791E+04 Occ(H):1.000E+10 Tbr(IRyd):4.445E+02 Occ (A):1.207E+06 Occ (Nu-hi):2.335E+16 -5.60 6686 0.00 5876 0.00 1549 0.00 6326 0.00 3227 0.00 6300 0.00 1030 0.00 Hydrogen 1.030E+00 H0/Hden: 1.000E+00 8.26E+24 H=2 1.267E+24 HE+1 He1 1.00E+10 1.000E+00 H.001 He1 1.00E+10 He1 1.030E+01 He1 He1 1.046E+01 He1 1.00E+10 He1 He1 He1 He1 He1 He1 He1 H	He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 Al:1.0E-10 Si:1.00E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10									
Q(1.0-1.8): 25.3048 Q(1.8-4.0): 24.6823 Q(4.20): 22.2822 Q(20-1): 0.0000 Ton pht fix:2.501E425 L(gam ray): 0.0000 Q(gam ray): 0.0000 L(Infred): 13.4202 Alf(0x): 0.0000 Total lumin: 15.1516 Ccc(FarIR):3.00E+04 Qcc(H = 6;1:1.079E+04 TCD=np1:5.000E+04 TCC(Car(H):1.2:33E=16 Totr(Har1): 0.00E+10 Totr(Har2): 0.02(11:4.445E=02 Occ(AR):1.4:45E=02 Occ(AR):1.4:45E=02 Occ(AR):1.4:290E=04 Totr(Nu-hi):4.197E=10 ##### 1 Tet5.038E+04 Hden:1.000E+10 Ne:1.000E+10 Ne:1.000E+10 Detta:1.000E+00 Detta:1.000E+00 Detta:1.000E+10 Ne:1.00E+10 Detta:1.000E+00 Detta:1.000E+10 Detta:1.000E+10 Detta:1.000E+10 Detta:1.000E+10 Detta:1.00E+10 Deta	333Cell Peak1.24E+00 Lo 1.00E-05=0.9105cm Hi-Con:1.16E+01 Ryd E(hi):7.35E+06Ryd E(hi): 100.01 MeV									
 Lígam rayj: 0.0000 (jgam rayj: 0.0000 Línfred): 13.4202 hif(ox): 0.0000 Total lumin: 15.1516 U(1.0): 8.3418+04 U(4.0): 6.446E+10 T(En-Den): 5.000E+04 T(Comp): 4.997E+04 nulu(912A): 95.38E+14 Occ(HarIR): 3.00E+04 Occ(H = 6): 1.079E+01 Occ(1Ryd): 7.020E+03 Tbr(4R): 2.029E+00 Tbr(Nu-hi): 4.335E-16 Tbr(FarIR): 4.999E+04 Tbr(H = 6): 4.791E+04 Tbr(1Ryd): 7.020E+03 Tbr(4R): 2.029E+00 Tbr(Nu-hi): 4.197E-10 ##### 1 Te: 5.038E+04 Hden: 1.000E+10 R: 1.000E+10 R: 1.000E+25 R-R0: 5.000E-01 dR: 1.000E+00 NTR: 1 Htot: 4.290E-04 T912: 5.527E-19### -5.60 4666 0.00 5876 0.00 1909 0.00 1549 0.00 6584 0.00 2326 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00 Hydrogen 4.928E-11 1.000E+00 H+0/Hden: 1.000E+00 8.968E-01 H- H2 2.432E-32 1.867E-24 H2+ HeH 2.433E-41 H col den 1.000E+10 Hydrogen 1.030E+00 H+0/Hden: 1.000E+00 8.968E-01 H- H2 2.327F+01 H2+ 5655F+08 HE H+ 2.433E-41 H 2SP 3-6 8.934E-13 2.428E-12 4.793E-12 7.287E-12 1.057E-11 1.457E-11 Texc(La): 4.975E+04 T(contn): 5.000E+04 T(diffs): 1.067E+03 H 2SP 3-6 1.110E+00 1.000E+00 H = 1 233 1.6687E-18 Comp H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 Helium 6.276E-18 1.207E-07 1.000E+00 H = 1 233 2.669E+00 Comp H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 He singlet 1.182E+00 1.057E+01 2.248E-19 3.248E-19 4.466E-19 He triplt 2.663E+19 1.561E-19 1.742E-19 9.467E-19 1.439E-19 He singlet 1.100E+00 0.00E+00 0.002E+00 1.073E+00 1.03E+00 1.072E+00 1.600E+00 6.958E+00 6.107E-10 He Singlet 1.100E+00 0.000E+00 1.034E+00 1.03E+00 1.03E+00 1.172E+00 9.83E=01 1.230E=07 FRAD/GAS; 1.158E-15 Pressure NgasTgas; 1.006E+15 F(total): 1.389E-01 P(gas) 1.389E-01 F(Radtn): 1.609E+16 Rad accel 1.894E+04 Force Mul 1.000E+00 Note+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Note+00 0.000E+00 0.000E+00 0.356E=05										
U(1.0): 8.341E+04 U(1.0): 8.341E+04 U(1.0): 8.341E+04 U(1.0): 8.341E+04 U(1.0): 8.341E+04 U(1.00E+00 U(1.0): 1.07E+04 U(1.0): 1.07E+04 U(1.0): 1.07E+04 U(1.0): 1.00E+04 U(1.0): 1.00E+04										
Occ (FarIR): 3.006E+04 Occ (H n=6): 1.079E+01 Occ (H Ng): 4.445E-02 Occ (A S): 2.07E-06 Occ (Nu-h): 2.335E-16 ##### 1 Te: 5.03E+04 Hden: 1.000E+10 R: 1.000E+10 Tir (Hyd): 4.445E-02 Tir (Hyd): 2.029E+00 Tir (Nu-h): 4.197E-10 ##### 1 Te: 5.03E+04 Hden: 1.000E+10 R: 1.000E+10 R: 1.000E+00 Tir (Hyd): 7.020E+03 Tir										
<pre>##### 1 Te:5.03BE+04 Hden:1.000E+10 Ne:1.000E+10 R:1.000E+25 R=R0;5.000E=01 dR:1.000E+00 NTR: 1 Hto:1.4290E=04 T912: 5.527E=19### -5.60 4686 0.00 5876 0.00 1909 0.00 1549 0.00 6584 0.00 2326 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00 Hydrogen 4.928E=11 1.000E+00 H=0/Hden: 1.000E+00 8.968E=01 H= H2 2.458E=32 1.867E=24 H2+ HeHt 2.433E=41 H col den 1.000E+10 Hydrogen 1.030E+00 1.000E+00 H=0/Hden: 1.000E+00 8.968E=01 H= H2 2.458E=32 1.867E=24 H2+ HeHt 2.433E=41 H col den 1.000E+10 Hydrogen 8.934E=13 2.428E=12 4.793E=12 7.287E=12 1.057E=11 1.457E=11 Texc(La); 4.975E+04 T(contn): 5.000E+04 T(diffs): 1.067E+03 H 2SP 3-6 1.110E+00 1.006E+00 1.024E+00 1.020E+00 1.01E+00 Helium 6.276E=18 1.207E=07 1.000E+00 He I 2S3 1.667E=18 Comp H, C 3.180E=04 3.206E=04 Fill Fact 1.000E+00 Gam 1/tot 3.622E=01 He singlet 3.335E=18 1.071E=19 1.507E=19 2.248E=19 3.248E=19 4.466E=19 He tripit 2.663E=19 1.561E=19 1.742E=19 9.467E=19 1.439E=19 He singlet 1.182E+00 1.027E+00 1.066E+00 1.042E+00 1.032E+01 4.466E=19 He tripit 2.663E=10 1.251E=07 13.407E+00 6.55E=06 6.107E=01 HeII 1.160E=07 3.728E=11 1.451E=11 1.390E=11 1.627E=11 1.432E=10 9.53E=10 1.235E=07 FRAD/GAS; 1.158E=15 HeII 1.158E=100 1.096E+00 1.088E+00 1.032E+00 1.032E+00 1.057E+00 1.117E+00 9.984E=01 1.000E+00 1.112E+00 FRAD/GAS; 1.158E=15 HeII 1.158E=100 1.096E+00 1.088E+00 1.038E+00 1.032E+01 9.521E=01 0.000E+00 0.000E+00 1.012E+00 FRAD/GAS; 1.158E=15 HeII 0.000E+00 0.000E+00 1.719E=10 1.73E=01 P(asI) 1.600E+10 1.000E+00 1.000E+00 0.000E+00 0.000E+00 Carbon 0.000E+00 0.000E+00 1.719E=10 1.73E=01 P(asI) 1.302E=10 FRAD/GAS 1.158E=15 HeII 0.000E+00 0.000E+00 0.000E+00 3.506E=05 4.791E=02 9.521E=01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Carbon 0.000E+00 0.000E+00 0.000E+00 0.356E=05 4.791E=02 9.521E=01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Carbon 0.000E+00 0.000E+00 0.220E=16 8.38E=01 4.370E=02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Carbon 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Carbon 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+0</pre>										
 5.60 4686 0.00 5876 0.00 1909 0.00 1549 0.00 1549 0.00 2326 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00 Hydrogen 4.928E-11 1.000E+00 H+0/Hden: 1.000E+00 8.968E-01 H= H2 2.458E-32 1.867E-24 HEH + 2.433E-41 H cold the H H cold the H A30E+00 Held the H A30E+00 Held the H A30E+01 L202E+02 A33E-13 A2428E-12 A33E-12 A287E-12 A37E-11 L457E-11 L457E-10 L467E-10 L467E-10 L457E-11 <lil457e-11< li=""> <lil457e-11< li=""> L457E-11</lil457e-11<></lil457e-11<>	Tbr(FarIR):4.999E+04 Tbr(H n=6):4.791E+04 Tbr(1Ryd):7.020E+03 Tbr(4R):2.029E+00 Tbr (Nu-hi):4.197E-10									
Hydrogen 4.928E-11 1.000E+00 H+/Hden: 1.000E+00 8.26E-24 H H2 2.458E-32 1.867E-24 H2+ HeH+ 2.433E-41 H col den 1.000E+10 Hydrogen 1.030E+00 1.000E+00 H.97EE-12 1.057E-11 1.457E-11 Texc(La); 4.975E+04 T(contn): 5.000E+04 T(diffs): 1.067E+03 H 2SP 3-6 1.100E+00 1.002E+00 1.022E+00 1.067E-11 1.457E-11 Texc(La); 4.975E+04 T(contn): 5.000E+04 T(diffs): 1.067E+03 Helium 6.276E-18 1.207E-07 1.000E+00 HE 2 3.266E+04 S.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 He singlet 1.158E+00 1.002E+00 He 2 3.248E-19 3.248E-19 He Comp H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 He singlet 1.182E+00 1.027E+00 1.042E+09 3.248E-19 4.466E+19 He triplt 2.663E+01 1.307E+00 6.595E+06 6.107E-19 1.413E+19 Heis 1.158E+01 1.158E+01 1.0	##### 1 Te:5.038E+04 Hden:1.000E+10 Ne:1.000E+10 R:1.000E+25 R-R0:5.000E-01 dR:1.000E+00 NTR: 1 Htot:4.290E-04 T912: 5.527E-19###									
Hydrogen 1.030E+00 1.000E+00 H+0/Hden: 1.000E+00 8,96E=01 H- H2 3.927E+01 H2+ 5.685E+08 He H+ 2.433E=41 H 2SP 3-6 1.110E+00 1.006E+00 1.024E+00 1.027E+01 1.457E=11 1ext(La); 4.975E+04 T(contn): 5.000E+04 T(diffs): 1.067E+03 H 2SP 3-6 1.110E+00 1.006E+00 1.024E+00 1.020E+00 1.016E+00 1.011E+00 Helium 1.182E+00 1.158E+00 1.000E+00 He I 2S3 1.667E+18 Comp H, C 3.180E=04 3.206E=04 Fill Fact 1.000E+00 Gam 1/tot 3.622E=01 He singlet 3.335E=18 1.071E=19 1.507E=19 2.248E=19 3.2669E+00 Comp H, C 3.180E=04 3.206E=04 Fill Fact 1.000E+00 Gam 1/tot 3.622E=01 He singlet 1.182E+00 1.027E+00 1.066E+00 1.042E+00 1.0324E=00 4.466E=19 He triplt 2.663E=19 1.561E=19 1.742E=19 9.467E=19 1.439E=19 He singlet 1.182E+00 1.027E+00 1.066E+00 1.042E+00 1.032E+00 1.057E+00 He triplt 2.663E=01 0.5796E=01 3.407E+00 6.595E=00 6.107E=01 HeII 1.206E=07 3.728E=11 1.451E=11 1.390E=11 1.627E=11 1.979E=11 1.432E=10 9.583E=10 1.235E=07 PRAD/GAS; 1.158E=15 HeII 1.158E+00 1.096E+00 1.080E+00 1.073E+00 1.057E+00 1.117E+00 9.984E=01 1.000E+00 1.1122H00 PRAD/GAS; 1.158E=15 HeII 1.158E+00 0.000E+00 0.000E+00 1.080E+00 1.007E+00 1.017E+00 1.017E+00 9.984E=01 1.000E+00 1.1122H0 PRAD/GAS; 1.158E=15 HeII 0.000E+00 0.000E+00 0.000E+00 3.506E=05 4.791E=02 9.521E=01 0.000E+00 0.000E+00 0.000E+00 0.4/Otot1 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 3.506E=05 4.791E=02 9.521E=01 0.000E+00 0										
H 2SF 3-6 8.934E-13 2.428E-12 4.793E-12 7.287E-12 1.057E-11 1.457E-11 Texc(La); 4.975E+04 T(contn): 5.000E+04 T(diffs): 1.067E+03 H 2SF 3-6 1.110E+00 1.00E+00 1.024E+00 1.01E+00 1.057E-19 2.248E-19 3.248E-19 3.248E-19 H c 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 He singlet 1.182E+00 1.027E+00 1.066E+00 1.042E+09 3.248E-19 4.466E-19 He triplt 2.669E+00 6.790E-01 3.407E+09 9.467E-19 1.439E-19 He singlet 1.162E+01 1.026E+07 3.728E-11 1.451E-19 1.451E-11 1.000E+00 1.017E+01 1.637E+01 1.057E+01 1.452E-01 0.00E+00 1.012E+00 1.088E+00 1.088E+00 1.037E+00 1.057E+00 1.117E+00 9.984E-01 1.000E+00 1.112E+00 PRAD/GAS; 1.158E-15 Pressure NgasTgas; 1.066E+15 P(tota) 1.356E-07 F(tota) 1.356E-07 F(tota) 1.139E-01 P(gas) 1.389E-01 P(gas) 1.389E-01 P(gas) 1.389E-01 P(gas) 1.389E-01 P(gas) 1.389E-01 P(gas) 1.000E+00 0.000E+00 0										
H2SP 3-61.110E+001.026E+001.022E+001.01E+00Helium6.276E-181.207E-071.000E+00He I 2S31.687E-18Comp H, C3.180E-043.206E-04Fill Fact1.000E+00Gam 1/tot3.622E-01Helium1.182E+001.158E+001.000E+00He I 2S32.669E+00Comp H, C3.180E-043.206E-04Fill Fact1.000E+00Gam 1/tot3.622E-01He singlet3.335E-181.071E-191.507E-192.248E-193.248E-194.466E-19He triplt2.669E+006.790E-013.407E+006.595E+006.107E-01He singlet1.182E+001.027E+001.066E+001.042E+001.032E+001.032E+001.235E-07PRAD/GAS;1.158E-15HeII1.266E-073.728E-111.451E-111.339E-011.677E+001.17E+009.583E-101.235E-07PRAD/GAS;1.158E-15HeII1.158E+001.006E+15P(total):1.339E-01P(gas):1.339E-01P(Gadn):1.609E-16Rad accel1.894E+04Force Mul1.000E+00Carbon0.000E+000.										
Helium 6.276E-18 1.207E-07 1.000E+00 He I 253 1.687E-18 Comp H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 Helium 1.182E+00 1.58E+00 1.000E+100 He X 3.266E-104 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 He singlet 3.335E-18 1.071E-19 1.507E-19 2.248E-19 3.248E-19 He triplt 2.663E-19 1.561E-19 1.742E-19 9.467E-19 1.439E-19 He singlet 1.182E+00 1.027E+00 1.042E+00 1.024E+00 1.026E+07 3.407E+00 6.595E+06 1.072E-19 HeII 1.206E-07 3.728E-11 1.439E-10 1.026E+07 1.439E-15 1.158E-15 HeII 1.158E+10 1.006E+07 1.080E+00 1.037E+00 1.172E+00 9.94E-01 1.100E+10 0.30E+00 1.107E+01 Yorken 0.000E+00 0.000E+00 0.000E+00 1.751E-04 9.998E-01 0.000E+00 0.000E+00 0.400E+00 0.000E+00 0.400E+00										
Helium 1.182E+00 1.158E+00 1.000E+00 He I 2S3 2.669E+00 Comp H, C 3.180E-04 3.206E-04 Fill Fact 1.000E+00 Gam 1/tot 3.622E-01 He singlet 3.335E-18 1.071E-19 1.507E-19 2.248E-19 3.248E-19 4.466E-19 He triplt 2.669E+00 6.790E-01 3.407E+00 6.595E+00 6.107E-01 He singlet 1.182E+00 1.027E+00 1.066E+00 1.032E+00 1.027E+00 1.1742E-19 9.583E-10 1.235E-07 PRAD/GAS; 1.158E+05 HeII 1.158E+00 1.096E+00 1.032E+00 1.072E+00 1.172H09 9.984E-01 1.000E+00 1.012E+00 PRAD/GAS; 1.158E-15 Pressure NgasTgas; 1.006E+15 P(total): 1.389E-01 P(gas): 1.389E-01 P(Radn): 1.609E+16 Rad accel 1.894E+04 Force Mul 1.000E+00 Nitrogen 0.000E+00										
He singlet 3.335E-18 1.071E-19 1.507E-19 2.248E-19 3.248E-19 4.466E-19 He triplt 2.663E-19 1.561E-19 1.742E-19 9.467E-19 1.432E-19 He singlet 1.182E+00 1.027E+00 1.066E+00 1.042E+00 1.026E+00 He triplt 2.663E-19 1.561E-19 1.742E-19 9.467E-19 1.432E-10 He II 1.206E-07 3.728E-11 1.451E-11 1.390E-11 1.627E-11 1.979E-11 1.432E-10 9.583E-10 1.235E-07 PRAD/GAS; 1.158E-15 He II 1.158E+00 1.096E+00 1.080E+00 1.073E+00 1.057E+00 1.117E+00 9.583E-10 1.235E-07 PRAD/GAS; 1.158E-15 He II 1.158E+00 1.006E+00 1.080E+00 1.073E+00 1.057E+00 1.117E+00 9.583E-10 1.000E+00 1.112E+00 PRAD/GAS; 1.158E-15 He II 1.158E+00 0.000E+00 1.096E+00 1.080E+00 1.037E+00 1.057E+00 1.117E+00 9.583E-10 1.000E+00 1.112E+00 PRAD/GAS; 1.158E-15 He II 0.000E+00 0.00										
He singlet 1.182E+00 1.027E+00 1.066E+00 1.042E+00 1.034E+00 1.026E+00 He triplt 2.669E+00 6.790E-01 3.407E+00 6.595E+00 6.107E-01 HeII 1.206E+07 3.728E+11 1.451E+11 1.390E+11 1.627E+11 1.979E+11 1.432E+10 9.583E+10 1.235E+07 PRAD/GAS; 1.158E+15 HeII 1.158E+00 1.096E+00 1.088E+00 1.080E+00 1.073E+00 1.057E+00 1.117E+00 9.984E+01 1.000E+00 1.112E+00 PRAD/GAS; 1.158E+15 Pressure NgaSTgas; 1.006E+15 P(total): 1.339E+01 P(gas): 1.389E+01 P(Radtn): 1.609E+16 Rad accel 1.894E+04 Force Mul 1.000E+00 Oxogen 0.000E+00 0.000E+00 0.000E+00 3.566E+05 4.791E+02 9.521E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Nitrogen 0.000E+00 0.000E+00 0.000E+00 3.566E+05 4.791E+02 9.521E+01 0.000E+00 0.										
HeII 1.206E-07 3.728E-11 1.451E-11 1.390E-11 1.627E-11 1.979E-11 1.432E-10 9.583E-10 1.235E-07 PRAD/GAS; 1.158E-15 HeII 1.158E+00 1.096E+00 1.080E+00 1.073E+00 1.077E+00 9.583E-10 1.235E-07 PRAD/GAS; 1.158E-15 Pressure NgasTgas; 1.006E+15 P(total): 1.389E-01 P(gas): 1.389E-01 P(Radtn): 1.609E-16 Rad accel 1.894E+04 Force Mul 1.000E+00 Carbon 0.000E+00 0.000E+00 <td< td=""><td></td></td<>										
HeII 1.158E+00 1.096E+00 1.080E+00 1.072E+00 1.117E+00 9.984E-01 1.000E+00 1.112E+00 PRD/GAS; 1.158E-15 Pressure NgaSTgas; 1.006E+15 P(total): 1.389E-01 P(gas): 1.389E-01 P(gas): 1.389E-01 P(gas): 1.389E-01 P(gas): 1.600E+00 0.00E+00										
Pressure NgasTgas; 1.006E+15 P(total): 1.389E-01 P(gas): 1.389E-01 P(Radtn): 1.609E-16 Rad accel 1.894E+04 Force Mul 1.000E+00 Carbon 0.000E+00 0.000E+00 1.719E-10 1.751E-04 9.998E-01 0.000E+00 0.000E+00 <td></td>										
Carbon 0.000E+00 0.000E+00 1.719E-10 1.751E-04 9.98E-01 0.000E+00 1.000E+00 0.000E+00 0.										
Nitrogen 0.000E+00 0.000E+00 <th< td=""><td></td></th<>										
Oxygen 0.000E+00 0										
Neon 0.000E+00 0.000E+00 0.000E+00 0.477E-03 9.488E-01 4.370E-02 0.000E+00 0.0										
Magnesium 0 0.000E+00 0.000E+00 3.220E-05 1.569E-01 8.318E-01 1.126E-02 0.000E+00 0.000E+00 <td></td>										
Al_minium 0 0.000E+00 0.000E+00 1.370E-07 5.863E-01 4.137E-01 0.000E+00 0.000E+00 <td></td>										
Silicon 0 0.000E+00 0.000E+00 2.578E-12 7.219E-06 1.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Sulphur 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Argon 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 1.327E-04 2.392E-02 9.581E-01 1.790E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Calcium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 8.046E-05 1.218E-01 8.263E-01 5.184E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Calculation stopped because NZONE reached. NZONE reached. 3.016E-07 9.191E-03 8.414E-01 1.494E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00										
Argon 0 0.000E+00 0.000E+00<										
Argon 0 0.000E+00 0.000E+00<	Sulphur 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 6.657E-06 9.938E-03 9.901E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00									
Iron 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 3.016E-07 9.191E-03 8.414E-01 1.494E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Calculation stopped because NZONE reached.										
Calculation stopped because NZONE reached.	Calcium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 8.046E-05 1.218E-01 8.263E-01 5.184E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00									

Photoionization of He 2TriS reached 100.0 percent of the total rate out.
IThe largest continuum occupation number s3.006E+04 at 1.053E-05 Ryd.
The continuum occupation number fell below 1 at 4.101E+03 Angstroms.
IThe largest continuum brightness temperature was 4.999E+04K at 1.053E-05 Ryd.
The continuum brightness temperature fell below 10,000K at 1.065E+03 Angstroms.
Continuum occupation number reached 2.09E+03 for some fine structure transitions.
Some fine structure lines were a heat source.
Induced recombination was 85.8% of the total for H level 7
Stimulated emission was 97.7% of the total for H level 7
Population of H =2 reached 4.19E-01 relative to the ground state.
Compton heating was 74.1% of the total.
Irduced recombination cooling was 1.6% of the total.
Free-free heating was 10.1% of the total. Photoionization of He 2TriS reached 100.0 percent of the total rate out.

* title thermal equil black body limit from Ferland and Rees 1988 * c this tests whether thermal processes go to lte c this tests whether therma. stop zone 1 hden 10 stop lyman optical depth -6 black body, t=50,000 lte abundances -10 abungances -10 print departure coef print last short iterate drmax 0 drmin 0 c hlte.in Emission Line Spectrum. Constant Open geometry. Iteration 2 of 2. Densitv Model. Intensity (erg/s/cm^2) Inci 4861 13.521******** Inci 1216 14.851******** BA C 0 -5.377 1.6748 H FF 0 -4.378 16.7045 ComC 0 -3.495 127.7448 H FB 0 -4.227 23.6657 ToFF 0 -4.378 16.7045 TOTL 6563 -5.194 TOTL 4861 -5.601 TOTL 4340 -5.912 TOTL 4102 -6.163 TOTL18751 -6.159 TOTL12818 -6.443 TOTL10938 -6.687 TOTL 950 -5.040 TOTL 938 -5.295 CION 0 -8.406 INWD 1216 -3.906 INWD 6563 -5.495 INWD 4861 -5.902 INWD18751 -6.460 TOTL 4861 -5.601 1.0000 TOTL 1216 -3.604 99.2126 TotH 0 -3.368 171.1970 BFH1 0 -4.427 14.9292 2.5518 3.6392 2.0252 1.0000 0.0016 0.4883 0.2739 0.2769 0.1438 0.0821 49,6063 1.2759 0.5000 0.1384
 COMH
 0
 -3.498
 126.9092
 TOTL10938
 -6.687

 CA
 B
 8261
 -5.602
 0.9981
 TOTL10512
 -6.854

 CA
 B
 1216
 -3.999
 39.9575
 TOTL26252
 -7.071

 DU
 B
 4861
 -5.605
 0.9904
 TOTL74578
 -7.400

 Q(H)
 4861
 13.075********
 TOTL 1216
 -3.604

 Q(H)
 1216
 14.609********
 TOTL 973
 -4.721

 Lines with negative intensities;
 283 Mg 4
 4

 1kwD18/51 - 6.400
 0.1384

 Strk 1216 - 8.225
 0.0024

 Strk 6563 - 8.034
 0.0037

 Strk 4861 - 8.171
 0.0027

 nFnu 4860 - 4.703
 7.9149

 nFnu 1215 - 4.593
 10.1817
 0.0558 0.0339 0.0159 7.5891

				FROM FERLAND AND R	EES 1988		
Cooling: H FF	0:0.098 Com						
Heating: BFH1	0:0.087 BFH	x 0:0.070 FF	н 0:0.101	ComH 0:0.741			
IONIZE PARMET:	U(1-) 4.9212	U(4-): 1.8093	U(sp): 4.92	Q(ion): 25.398	L(ion): 14.910	Q(low): 25.71	P(low) 14.78
ENERGY BUDGET:	Heat: -3.368	Coolg: -3.369	Error: 0.2%	Compt H: -3.498	WorkF: -3.572	F-F H -4.361	PRADMX:1.27E-01
Column density	H12:1.000E+10	H II:1.000E+10	HI:4.928E-01	H-: 4.826E-14	H2: 2.458E-22	H2+:1.867E-14	He H+:2.433E-31
	OH: 0.000E+00	Heff:0.000E+00					
<nh>:1.000E+10</nh>	<tp>:5.04E+04</tp>	<to3>:0.00E+00</to3>	Ne:0.000E+00	ti(snd):3.46E-07	NeN+dl:1.00E+20	<t(c3)>:5.04E+04</t(c3)>	<e(c3)>:1.00E+10</e(c3)>
He/Ha:2.64E-10	= 2.64*true	N/Oap:0.00E+00	= 0.00true	T(O3R):0.000E+00	L THIN:1.00E+30	<t(s2)>:0.00E+00</t(s2)>	<e(s2)>:0.00E+00</e(s2)>
T He+:5.04E+04	EHe+:1.00E+10	T(O+):0.00E+00	EO+:0.00E+00	iter/zn: 1.000	Te-low:5.04E+04	Te-high:5.04E+04	Hlu/zn:1.00E+00
<a>:0.00E+00	erdeFe0.0E+00	Tcompt1.98E-12	Tthr4.87E+02	<tden>: 5.04E+04</tden>	<dens>:1.66E-14</dens>	<mol>:5.00E-01</mol>	
Mean Jeans	l(cm)1.54E+17	M(sun)1.60E+04	smallest:	len(cm):1.54E+17	M(sun):1.60E+04	Alf(ox-tran):	0.0000

-	
title constant temper black body limit from Ferland and Rees 1988	
c tests whether departure coef are forced to unity by induced processes	
constant temper 50,000	
stop zone 1	
grains -5 no heating no cooling	
hden 10	
stop lyman continuum optical depth -6	
black body, t=50,000 lte	
metals -10	,
print departure coef	,
faint -1	,
print short last	,
iterate	,
drmax 0	,
drmin 0	,
c induc.in	,
c cray	,

Chemical composition He:.098 C:3.63E-14 N:1.12E-14 O:8.51E-14 Ne:1.23E-14 Mg:3.80E-15 Al:3.0E-16 Si:3.55E-15 S:1.62E-15 A:3.6E-16 Ca:2.3E-16 Fe:4.68E-15

333Cell Peak1.24E+00 Lo 1.00E-05=0.9105	cm Hi-Con:1.16E+01 Ryd E	(hi):7.35E+06Ryd E	(hi): 100.01 MeV
P(nu>1ryd): 14.9097 Average nu:1.491E+	00 P(X-ray): 0.0000 F	(BalC): 14.7629 Q	(Balmer C): 25.6389
Q(1.0-1.8): 25.3048 Q(1.8-4.0): 24.68	23 Q(4.0-20): 22.2862 Q	(20): 0.0000 I	on pht flx:2.501E+25
L(gam ray): 0.0000 Q(gam ray): 0.00	00 L(Infred): 13.4202 A	lf(ox): 0.0000 T	otal lumin: 15.1516
U(1.0):8.341E+04 U(4.0):6.446E+	01 T(En-Den):5.000E+04 T	(Comp):4.997E+04 n	uJnu(912A):9.638E+14
Occ(FarIR):3.006E+04 Occ(H n=6):1.079E+	01 Occ(1Ryd):4.445E-02 C	cc(4R):3.207E-06 0	cc (Nu-hi):2.335E-16
Tbr(FarIR):4.999E+04 Tbr(H n=6):4.791E+	04 Tbr(1Ryd):7.020E+03 1	br(4R):2.029E+00 T	br (Nu-hi):4.197E-10
Grain(Pal):4.423E-28 Grain(Bal):1.783E-	27 Grain Mg2:4.381E-27 G	rain R:1.527E-26 G	rain(HeII):5.214E-27
##### 1 Te:5.000E+04 Hden:1.000E+10 Ne:1.196E+10 F			
-5.52 4686 3.31 5876 0.00 1909 0.00 1549 0.00			
Hydrogen 5.933E-11 1.000E+00 H+0/Hden: 1.000E+00			3.446E-32 H col den 1.000E+10
Hydrogen 1.007E+00 1.000E+00 H+0/Hden: 1.000E+00			
H 2SP 3-6 1.075E-12 2.922E-12 5.769E-12 8.773E-12); 4.976E+04 T(contn):	5.000E+04 T(diffs): 4.230E+02
H 2SP 3-6 1.102E+00 9.981E-01 1.019E+00 1.016E+00			
Helium 9.037E-18 1.449E-07 1.000E+00 He I 2S3			
Helium 1.135E+00 1.068E+00 1.000E+00 He I 2S3			
He singlet 4.797E-18 1.540E-19 2.167E-19 3.238E-19			
He singlet 1.135E+00 1.015E+00 1.056E+00 1.035E+00			
HeII 1.448E-07 4.474E-11 1.739E-11 1.668E-11			
HeII 1.068E+00 1.070E+00 1.072E+00 1.068E+00			
Gra-ISM Dust temp 5.002E+04 Pot(Volt) 5.313E+01			
Sil-ISM Dust temp 5.002E+04 Pot(Volt) 5.566E+01			
Pressure NgasTgas; 1.147E+15 P(total): 1.584E-01			
Carbon 0.000E+00 0.000E+00 2.466E-10 2.097E-04			
Nitrogen 0.000E+00 0.000E+00 0.000E+00 5.040E-05			
Oxygen 0.000E+00 0.000E+00 0.000E+00 8.605E-04			
Neon 0.000E+00 0.000E+00 0.000E+00 9.042E-03			
Magnesium 0 0.000E+00 0.000E+00 4.484E-05 1.826E-01			
Aluminium 0 0.000E+00 0.000E+00 1.760E-07 6.292E-01			
Silicon 0 0.000E+00 0.000E+00 3.690E-12 8.643E-06	1.000E+00 0.000E+00 0.000E+	00 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.000E+00

Sulphur 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 9.629E-06 1.205E-02 9.879E-01 0.000E+00 0.000E Calculation stopped because NZONE reached. Geometry is plane-parallel. Photoionization of He 2TriS reached 100.0 percent of the total rate out. !The largest continuum occupation number was 3.006E+04 at 1.053E-05 Ryd. The continuum occupation number fell below 1 at 4.101E+03 Angstroms. !The largest continuum brightness temperature was 4.999E+04K at 1.053E-05 Ryd. !The largest continuum brightness temperature was 4.999E+04K at 1.053E-05 Ryd. The continuum brightness temperature fell below 10,000K at 1.065E+03 Angstroms. W-A physical process has been disabled. C-Heating - cooling mismatch = 5.9%. Whats wrong? Continuum occupation number reached 2.09E+03 for some fine structure transitions. Some fine structure lines were a heat source. Induced recombination was 85.8% of the total for H level 7 Stimulated emission was 97.7% of the total for H transition 7 - 6 Population of H n=2 reached 3.85E-01 relative to the ground state. Compton heating was 65.1% of the total. W-Maximum tempertaure of grain Gra-ISM was 5.00E+04, above sublimation temperature? Induced recombination cooling was 1.4% of the total. Free-free heating was 12.5% of the total. C-Free-free heating significant and frequency out of range of gaunt factor routine.

constant temper set, stop zone 1 grains -5 no heating no cooling hden 10 stop lyman continuum optical depth -6 black body, t=50,000 lte ==t=le =10 metals -10 print departure coef faint -1 print short last iterate drmax 0 drmin 0 c induc.in Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2) Emergent line intensities TOTL 4861 -5.522 TOTL 1909-22.453 O 1 6300-35.000 1.0000
 TOTL
 6563
 -5.115
 2.5518
 TOTL
 4340
 -5.833
 0.4883

 C
 4
 1549-15.507
 0.0000
 N
 2
 6584-35.000
 0.0000

 O
 1
 6363-35.000
 0.0000
 TOTL
 3727-35.000
 0.0000

 TOTL
 4363-35.000
 0.0000
 Emis
 2798-35.000
 0.0000
 TOTL18751 -6.079 N 2 6548-35.000 O 3 5007-35.000 S 2 6720-35.000 0.2769 0.0000 0.0000 ο 3 4959-35.000 0.0000 0.0000 s 3 9532-35.000 0.0000 Intrinsic line intensities TOTL 6563 -5.114 2.5508 INWD18751 -6.379 0.1384 TOTL 4861 -5.520 1.0000 nFnu 4860 -3.074 279.4284 TOTL 430 -5.832 0.4884 nFnu 1215 -1.129******** TOTL 4102 -6.083 0.2741 Inci 4861 13.521******** TOTL18751 -6.078 0.2769 Inci 1216 14.851******** TOTL1218 -6.362 0.1439 BA C 0 -4.710 6.4657 TOTL 1216 -3.524 99.1318 PA C 0 -5.297 1.6730 TOTL 950 -4.959 3.6403 H FF 0 -4.302 16.5391 TOTL 938 -5.214 2.0263 Comc 0 -3.420 126.1371 INWD 1216 -3.825 49.5559 H FB 0 -4.140 23.4943 TOTL 4861 -5.520 1.0000 TOTL 1216 -3.524 99.1318 TOTH 0 -3.233 193.7339 BFH1 0 -4.347 14.9127 BFHx 0 -4.442 11.9930 BFHe 0 -4.301 16.5903 FF H 0 -4.137 24.1733 COMH 0 -3.420 126.0645 CA B 4861 -5.521 0.9993 HeFF 0 -4.709 HeFB 0 -4.704 6.4833 6.5475 ToFF 0 -4.158 HeII 228 -3.543 He2C 911 -4.511 TOTL 1640 -3.836 23.0224 94.9844 10.2274 48.4009 TOTL 1640 -3.836 TOTL 4686 -5.001 TOTL 1216 -4.443 Ca B 1640 -4.659 DevB 1640 -4.669 Ca B 4686 -5.640 DevB 4686 -5.656 3.3094 11.9472 CA B 4861 -5.521 CA B 1216 -3.919 DU B 4861 -5.695
 TOTL
 973
 -4.640
 7.5891

 TOTL
 950
 -4.959
 3.6403

 TOTL
 938
 -5.214
 2.0263

 INWD
 1216
 -3.825
 49.5659
 0.9993 7.2752 DU B 4861 -5.695 0.6696 INWD 12 Q(H) 4861 13.075******* INWD 65 Q(H) 1216 14.609******* INWD 44 Lines with negative intensities; 283 Mg 4 H FB 0.7596 INWD 6563 -5.415 INWD 4861 -5.821 B3 Mg 4 4 1.2754 Hind 0.7320 Heli

<****

		NSTANT TEMPER BI		F FROM FERLAND AND	REES 1988		
Cooling: H FF	0:0.091 Com0						
Heating: BFH1	0:0.077 BFH2	c 0:0.062 BFI	le 0:0.086	FF H 0:0.125	ComH 0:0.651		
IONIZE PARMET: U	(1-) 4.9212	U(4-): 1.8093	U(sp): 4.92	Q(ion): 25.398	L(ion): 14.910	Q(low): 25.71	P(low) 14.78
ENERGY BUDGET: He	eat: -3.233	Coolg: -3.259	Error: 5.7%	Compt H: -3.420	WorkF: -0.639	F-F H -4.137	PRADMX:1.11E-01
Column density Hi	12:1.000E+10	H II:1.000E+10	HI:5.933E-01	H-: 6.958E-14	H2: 2.931E-22	H2+:2.234E-14	He H+:3.446E-22
OI	H: 0.000E+00	Heff:0.000E+00					
<nh>:1.000E+10 <1</nh>	<pre>Fp>:5.00E+04</pre>	<to3>:0.00E+00</to3>	Ne:0.000E+00	ti(snd):3.82E-07	NeN+dl:1.20E+20	<t(c3)>:5.00E+04</t(c3)>	<e(c3)>:1.20E+10</e(c3)>
He/Ha:2.58E-01 =	2.63*true	N/Oap:0.00E+00	= 0.00true	T(O3R):0.000E+00	L THIN:1.00E+30	<t(s2)>:0.00E+00</t(s2)>	<e(s2)>:0.00E+00</e(s2)>
T He+:5.00E+04 EH	He+:1.20E+10	T(O+):0.00E+00	EO+:0.00E+00	iter/zn: 1.000	Te-low:5.00E+04	Te-high:5.00E+04	Hlu/zn:1.00E+00
<a>:0.00E+00 e1	rdeFe0.0E+00	Tcompt1.65E-12	Tthr4.31E+02	<tden>: 5.00E+04</tden>	<dens>:2.31E-14</dens>	<mol>:6.07E-01</mol>	
Mean Jeans l	(cm)1.18E+17	M(sun)1.00E+04	smallest:	len(cm):1.18E+17	M(sun):1.00E+04	Alf(ox-tran):	0.0000
L(dust):-1.108E+	+00						
Gra-IS	SM Sil-ISM	Gra-Ori Sil-O	Dri Sil-0.01	Sil-0.1 Silica	tPN		
<tdust>: 5.002E+</tdust>	+04 5.002E+04	0.000E+00 0.000E	E+00 0.000E+00	0.000E+00 0.000E+	-00		
<vel d="">: 3.807E+</vel>	+09 3.590E+09	0.000E+00 0.000E	E+00 0.000E+00	0.000E+00 0.000E+	-00		
<pot d="">: 5.313E+</pot>	+01 5.566E+01	0.000E+00 0.000E	E+00 0.000E+00	0.000E+00 0.000E+	-00		

	*
title interstellar cloud irradiated by ism background	*
table ism	*
extinguish by a column of 22	*
cosmic rays, background	*
hden 0	*
abundances hii region; this turns on Orion grains by default	*
grains ism ;this over rides above default, forcing ism grains	*
sphere ;set sphere since matter in all directions	*
stop temperature linear 10	*
stop thickness 0.1 linear parsecs	*
iterate	*
print last	*
faint .1	*
c ism.in	*
c cray	*
	*

Chemical composition He:.095 C:3.00E-04 N:7.00E-05 O:4.00E-04 Ne:1.10E-04 Mg:3.00E-05 Al:2.0E-07 Si:3.00E-06 S:1.00E-05 A:3.0E-06 Ca:2.0E-08 Fe:3.00E-06

546Cell Peak5.62E-05 Lo 1.00E-05=0.9105cm Hi-Con:7.33E+06 Ryd E(hi):7.35E+06Ryd E(hi): 100.01 MeV P(nu>Iryd): -6.0706 Average nu:3.498E+01 P(X-ray): -6.0947 P(BalC): -2.5136 Q(Balmer C): 8.5139 Q(1.0-1.8): 2.9599 Q(1.8-4.0): 1.7594 Q(4.0-20): 0.2544 Q(20): 2.1588 Ion pht flx:1.115E+03 L(gam ray): -7.7247 Q(gam ray): -1.2176 L(Infred): -1.4664 Alf(ox): -2.4590 Total lumin: -1.4290 U(1.0):3.720E-08 U(4.0):4.868E-09 T(En-Den):3.580E+00 T(Comp):4.398E+03 nuJnu(912A):9.999E-08 Occ(FarIR):1.080E+00 Occ(H n=6):1.419E-13 Occ(IRyd):4.603E-24 Occ(4R):1.009E-23 Occ (Nu-h):3.721E-55 Tbr(FarIR):1.796E+00 Tbr(H n=6):6.301E-10 Tbr(1Ryd):7.271E-19 Tbr(R):6.383E-23 Tbr (Nu-h):4.105E-43
Grain(Pal):4.423E-23 Grain(Bal):1.782E-22 Grain Mg2:4.379E-22 Grain R:1.527E-21 Grain(HeII):5.214E-22
Grain (Pal):4.423E-23 Grain (Pal):1.782E-22 Grain Mg2:4.379E-22 Grain R:1.527E-21 Grain (HeII):5.214E-22 ##### 1 Te:8.808E+01 Hden:1.000E+00 Ne:2.220E-02 R:1.000E+25 R=R0:8.121E+15 dR:1.624E+16 NTR: 1 Htot:2.770E-26 T912: 1.786E+00### -10.60 4666 0.00 5876 0.4 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00 Hydrogen 9.782E-01 2.176E-02 H+0/Hden: 1.000E+00 9.792E-12 H H2 3.372E-07 2.845E-12 H2+ HEH+ 7.061E-10 H col den 1.624E+16 H 2SP 3-6 5.284E-15 6.823E-18 2.924E-21 2.065E-21 2.391E-21 3.083E-21 Texc(La); 2.663E+03 T(contn): 3.580E+00 T(diffs): 1.495E-01 Heiium 9.991E-01 1.714E-18 2.718E-24 1.920E-24 2.223E-24 2.00E+12 Comp H, C 1.606E-33 3.216E-33 F11 Fact 1.000E+00 Gam 1/tot 1.000E+00 Heii 9.387E-04 2.335E-24 2.421E-31 1.710E-31 1.980E-31 2.553E-31 0.000E+00 0.000E+00 0.000E+00 PRAD/GAS; 4.939E-06 Grain Nust temp 1.973E+01 Pot(Volt) 2.933E-01 Nelectron 6.111E+01 drft cm/s 1.312E+03 Heating: 6.542E-27 Frac(tot) 2.768E-01 Sil-ISM Dust temp 1.595E+01 Pot(Volt) 3.231E-01 Nelectron 6.732E+01 drft cm/s 1.312E+03 Heating: 7.669E-27 Frac(tot) 2.768E-01 Sil-ISM Dust temp 1.973E+01 Pot(Volt): 1.347E-14 P(gas): 1.347E-14 P(Radtn): 6.654E-20 Rad accel 1.065E-10 Force Mul 1.346E+04 Carbon 1.031E-03 9.989E-01 9.524E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Nitrogen 9.994E-01 5.634E-04 2.896E-08 2.725E-12 1.537E-15 0.000E+00 0.000E+00 0.000E+00 0.000E+00
1700 0 8.251E-03 9.917E-01 1.525E-06 0.000E+00 0.00E+00 0.00E
-9,58 4686 0.00 5876 0.06 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.00
Hydrogen 9.877E-01 1.225E-02 H+0/Hden: 1.000E+00 6.528E-12 H- H2 3.568E-07 8.780E-13 H2+ HeH+ 1.063E-09 H col den 3.001E+17

H 2SP 3-6			1.447E-21									
Helium			2.649E-08									
He singlet			1.823E-24									
HeII			2.373E-30									
Gra-ISM			Pot(Volt)									
Sil-ISM			Pot(Volt)									
Pressure			P(total):									2.320E+04
Carbon			9.239E-05									
Nitrogen	9.957E-01	4.333E-03	6.685E-09	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/0totl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9.995E-01	4.983E-04	2.713E-08	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	4.982E-29	A:-11.140
Neon	9.951E-01	4.865E-03	1.486E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Magnesium O	1.860E-03	9.979E-01	2.427E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Aluminium 0	1.660E-04	9.997E-01	1.421E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Silicon 0	1.115E-04	9.999E-01	2.164E-07	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Sulphur 0	1.527E-04	9.995E-01	3.146E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Argon 0	8.798E-01	1.201E-01	1.243E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Calcium 0	1.111E-03	1.863E-01	8.126E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Iron 0	4.190E-03	9.958E-01	1.026E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Calculati	on stopped	because of	uter radiu:	s reached.								
Geometry	is plane-pa	arallel.										
!The large	st continu	um occupat	ion number	was 1.080	E+00 at 1.0	053E-05 RV	d.					
W-Temperatu	re fell be	iow 100k, ·	this calcu	lation is [.]	tentative.	1						
Local gra	in-gas phot	coelectric	heating ra	ate reache	d 67.4% o:	f the tota	1.					
	in photoele											
	toelectric											
	re out of 1				r routine.							
	out of rai											
	ve level po											
	low and mat				nes. Low-de	ensity Cas	e B assume	 11 тні 	0 = 1.000E	+03		
	low and mat									E1LO= 1.000)E+03	
	low and mat											
Temb coo	10. and ma		bed for ne	1011 111 201		son densite	, cass b a.	sounde .		1.3331.03		

				Y 80.08 <************************************	*****
	* title inte	erstellar cloud irra	diated by	ism background	*
	* table ism				*
	* extinguish	by a column of 22			*
	* cosmic ray	s, background			*
	* hden 0	. ,			*
	* abundances	hii region; this t	urns on Or	ion grains by default	*
	* grains ism	this over rides a	bove defau	lt, forcing ism grains	*
	* sphere ;se	t sphere since matt	er in all	directions	*
		erature linear 10			*
		ness 0.1 linear par	secs		*
	* iterate	F			*
	* print last				*
	* faint .1				*
	* c ism.in				*
	* c crav				*
		*****	**> LOG(U)	: -7.43 <************************************	*****
		Marnings exist, this			
		arningo chibe, chib	ourouruor	on ib babpoot	
En	ission Line	Spectrum, Constan	t Density	Model. Closed geometry. Itera	ation 2 of 2.
	internet internet		tensity (e		
TOTL 4861 -9.577	1.0000	DU B 4861 -9.543	1.0822	2 NU 0 -8.576 10.0320	Inci 1216 -2.637********
TOTL 1216 -7.975	40.0415	O(H) 4861 -9.276	2.0005	TOTL 1216 -7.975 40.0415	BA C 0 -9.254 2.1059
TotH 0 -8.173	25.3316	Q(H) 1216 -7.742	68.3975	INWD 1216 -8.218 22.8366	PA C 0 -9.700 0.7527
BFH1 0 -8.579	9,9570	TOTL 6563 -8.841	5.4428	INWD 6563 -9.142 2.7214	Grai 0 -6.4791253.5774
BFHe 0-10.234		TOTL 4861 -9.577	1.0000	INWD 4861 -9.878 0.5000	REC 1656-10.280 0.1984
TotM 0-10.567		TOTL 4340 -9.985	0.3907	INWD18751-10.436 0.1384	C 2 158 -8.176 25.1774
GraH 0 -8.401		TOTL 4102-10.265		e sc18751-10.134 0.2771	Si 2 35-10.545 0.1076
CA B 4861 -9.543		TOTL18751-10.135		nFnu 4860 -9.431 1.3989	
CA B 1216 -7.977		TOTL12818-10.516	0.1151	Inci 4861 -2.138********	
Lines with negative in		205 T OI 0	0.1101	1.01 1001 2.100	
Lines with negative in		200 1 01 0			

INTERSTELLAR CLOUD IRRADIATED BY ISM BACKGROUND 2 158:0.987 Cooling: C 2 Heating: BFH1 0:0.393 GraH TONTZE PARMET: U(1-) -7.4295 U(4-): -8.3126 U(sp): -7.43 Q(ion): 2.664 L(ion): -6.079 Q(low): 12.99 Heat: -8.173 Coolg: -8.170 Error: 0.7% Compt H: -15.391 WorkF: -7.831 F-F H-14.997 H12:3:001E+17 H II:4.970E+15 HI:2.951E+17 H-: 2.558E+06 H2: 1.039E+11 H2+:4.998E+05 OH: 0.000E+00 Heff:2.684E+17 P(low) -1.43 PRADMX:4.44E-03 ENERGY BUDGET: He H+:2.525E+08 Column density <TO3>:9.46E+01 Ne:1.708E-02 NeN+dl:8.76E+13 <T(C3)>:9.46E+01 <E(C3)>:1.71E-02 <NH>:1.000E+00 ti(snd):3.82E+12 <Tp>:9.38E+01
 KHIA-14:00
 KIA-17:00
 <thKIA-17:00</th>
 <thKIA-17:00</th>
 <th
 L THIN:1.00B+30
 <T(S2)>:9.47E+01
 <E(S2)>:1.70E-02

 Te-low:8.81E+01
 Te-high:1.04E+02
 Hlu/zn:1.04E+01

 <dens>:2.32E-24
 <Mol>:1.25E+00
 M(sun):2.51E+04
 Alf(ox-tran):
 -2.4590
 L(dust):-6.479E+00 Sil-ISM Gra-Ori Sil-Ori Sil-0.01 Sil-0.1 Gra-ISM SilicatPN
 Gra-ISM
 Sil-ISM
 Gra-Ori
 Sil-Ori
 Sil-Ol
 Sil

 Optical Depths: CONTN; COMP: 1.70E-09
 H-: 4.99E-11 R(1300): 1.98E-06 H2+ 3.50E-12
 Herri:2.33E-04

 Pfa:3.80E-06
 Pa:1.73E-05
 Ba:8.76E-05
 Hb:1.20E-04
 La:4.23E-04
 1r:1.772E+00
 1.8:5.47E-01
 4

 10830: 7.62E-07
 3889: 3.25E-08
 5876: 4.72E-18
 7065: 2.61E-18
 1.00E-20
 1335: 1.25E+02
 97

 1550: 1.00E-20
 2800: 1.30E+02
 774: 1.00E-20
 1240: 1.00E-20
 1035: 1.00E-20
 1335: 1.25E+02
 97

 789: 5.26E-12
 1207: 3.81E-06
 1085: 4.08E-02
 1194: 5.13E-05
 1909: 1.08E-08
 1895: 1.02E-10
 232

 1750: 2.54E-14
 1025: 1.12E+01
 352: 1.00E-20
 347: 1.00E-20
 1360: 7.87E-05
 630: 1.65E-14
 849

 1808: 1.48E+01
 1256: 1.36E+00
 -34: 4.85E-01
 -48: 1.00E-20
 394: 1.00E-20
 396: 1.02E-20
 396: 1.02E 4.:8.285E-02 21R:9.449E-04 977: 2.72E-02 1397: 3.65E-09

 1035:
 1.00E-20
 1335:
 1.22E+02
 9/7:
 2.72E-02

 1909:
 1.08E-08
 1895:
 1.02E-10
 2326:
 6.23E-05

 1860:
 7.87E-05
 630:
 1.65E-14
 834:
 1.11E-01

 3934:
 1.00E-20
 3969:
 1.00E-20
 8498:
 1.00E-20

 990:
 1.12E-07
 1402:
 7.02E-17
 1214:
 9.91E-20

 8727:
 1.00E-20
 6300:
 1.01E-07
 5577:
 1.00E-20

 1666: 1.40E-11 835: 6.79E-07 -3: 4.85E-01 1304: 3.83E+01 1656: 7.88E-02 -48: 1122: 9830: 1.00E-20 1.00E-20 6.82E-07 1.31E-11 1808: 1.18E+01 1256: 1.36E+00 8542: 1.00E-20 8662: 1.00E-20 2335: 2.82E-05 353: 1.00E-20 1406: 9.30E-14 1486: 1.88E-15 7291: 1.98E-09 1039: 5.43E+00 -8446: 2.19E-20 -4368: 765: 1.14E-09 -1198: 2.03E-17 786: 7324: 1.37E-09 -245: 1.00E-20 1.01E-20 -132: 1.27E-20 -113: 1.43E-20 -29: 1.00E-20 -46: 2.01E-20 -4368: 1.01E-20 -132: 1.27E-20 -113: 1.43E-20 -29: 1.00E-20 -46: 2.01E-20 786: 6.04E-14 N57: 1.97E-12 0146: 1.31E-11 063: 1.16E-03 088: 1.31E-10 052: 2.46E-15 NE16: 3.83E-09 MG4: 1.00E-20 MG14: 1.00E-20 MG6: 1.14E-17 SI35: 1.56E-05 AR7: 1.00E-20 AR9: 1.43E-09 AR22: 1.00E-20 AR13: 2.08E-18 AR8: 1.00E-20 Ne14: 1.00E-20 Ne24: 6.38E-19 Si3: 1.00E-20 Si4: 1.00E-20 Fe7: 1.00E-20 C157: 1.00E-03 026: 2.37E-16 N122: 2.29E-09 NE13: 9.90E-07 N205: 8.93E-06 NE36: 1.78E-19

 S19:
 1.65E-14
 S34:
 4.43E-08
 S11:
 1.00E-20
 RA7:
 1.00E-20
 RA9:
 1.43E-09
 R22:
 1.00E-20

 CA3:
 1.00E-20
 CA12:
 1.00E-20
 CA4:
 1.00E-20
 Ne14:
 1.00E-20
 Ne24:
 6.38E-19
 Si3:
 1.00E-20

 Fe61:
 1.00E-20
 Fe23:
 1.00E-20
 Fe13:
 1.00E-20
 Si2.5:
 1.00E-20
 Si6.5:
 1.00E-20
 C610:
 2.41E-09

 C370: 1.37E-06
 Old hydro optical depths:
 1 1.69E+00
 2 9.27E-05
 3 3.77E-05
 4 1.81E-05

 Lines:
 2-1 1.64E+05
 3-2 1.00E-10
 4-3 1.22E-16
 5-4 9.93E-17

 New hydro optical depths:
 1 1.77E+00
 2 9.74E-05
 3 3.96E-05
 4 1.90E-05

 Lines:
 2-1 8.98E+04
 3-2 5.06E-11
 4-3 6.20E-17
 5-4 5.05E-17
 5 8.90E-06 6-5 1.02E-16 5 9.35E-06 6-5 5.19E-17 6 4.83E-06 7 1.64E-06 7-6 1.56E-16 8-7 1.00E-20 6 5.07E-06 7 1.72E-06 7-6 7.92E-17 8-7 5.00E-21
 Old He Is optical depths:
 1 2.60E-01
 2 6.60E-05
 3 5.00E-21
 4 5.00E-21
 5 5.00E-21
 6 5.00E-21
 7 5.00E-21

 Lines:
 2-1 1.01E+04
 3-2 3.67E-13
 4-3 1.29E-18
 5-4 1.05E-18
 6-5 1.08E-18
 7-6 1.65E-18
 8-7 1.00E-20

 New HE Is optical depths:
 1 2.87E-01
 2 7.27E-05
 3 5.00E-21
 4 5.00E-21
 5 5.00E-21
 6 5.00E-21
 7 5.00E-21

 Lines:
 2-1 1.10E+04
 3-2 3.91E-13
 4-3 1.37E-18
 5-4 1.12E-18
 6-5 1.15E-18
 7-6 1.65E-18
 8-7 1.00E-20

 Old He II optical depths:
 1
 3.94E-02
 2
 8.43E-01
 3
 5.00E-21
 4
 5.00E-21

 Lines:
 2-1
 8.99E+00
 3-2
 1.12E-18
 4-3
 1.00E-20
 5-4
 1.00E-20

 New HE II optical depths:
 1
 4.34E-02
 2
 9.29E-01
 3
 5.00E-21
 4
 5.00E-21

 Lines:
 2-1
 8.96E+00
 3-2
 1.26E-18
 4-3
 1.00E-20
 5-4
 1.00E-21
 5 5.00E-21 6 5.00E-21 7 5.00E-21 6-5 1.00E-20 7-6 1.00E-20 8-7 1.00E-20 5 5.00E-21 6 5.00E-21 7 5.00E-21 6-5 1.00E-20 7-6 1.00E-20 8-7 1.00E-20 Hydrogen -0.007 -1.781 Helium 0.000 -2.984 -7.804 Log10 Mean Ionisation (over volume) Hellum 0.000 -2.984 -7.804 Carbon -3.125 0.000 -4.016 Nitrogen -0.003 -2.153 -8.110-10.618 Oxygen 0.000 -3.267 -7.552-12.831-16.080 Neon -0.002 -2.379 -4.972-11.566-15.347-17.711-21.720 Magnesium -2.574 -0.001 -3.593 -9.278-12.985-15.542-19.437-22.157-26.250 Aluminum -3.628 0.000 -3.916 -7.007-11.361-13.471-18.076-20.336-25.312-27.714

Silicon -3.799 0.000 -6.494 -9.083-16.055-15.405-21.415-22.206-28.219-29.382-35.466 -3.664 0.000 -3.568 -9.879-13.830-15.965-20.292-22.652-27.290-29.857-34.600-37.269-42.238 -0.062 -0.875 -3.960 -9.367-13.415-15.922-20.060-22.133-26.507-29.105-34.046-36.676-41.661-41.954-41.954 -2.656 -0.603 -0.126 -2.222 -0.003 -5.899 Sulphur Argon Calcium Iron 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 -0.007 -1.781 0.000 -2.984 -7.804 -3.125 0.000 -4.016 Hydrogen Log10 Mean Ionisation (over radius) Helium Carbon Carbon -3.125 0.000 -4.016 Nitrogen -0.003 -2.153 -8.110-10.618 Oxygen 0.000 -3.267 -7.552-12.831-16.080 Neon -0.002 -2.379 -4.972-11.566-15.347-17.711-21.720 Magnesium -2.574 -0.001 -3.593 -9.278-12.985-15.542-19.437-22.157-26.250 Aluminum -3.628 0.000 -3.916 -7.007-11.361-13.471-18.076-20.336-25.312-27.714 Silicon -3.799 0.000 -6.494 -9.083-16.055-15.405-21.415-22.206-28.219-29.382-35.466 -3.664 -3.664 0.000 -3.568 -9.879-13.830-15.965-20.292-22.652-27.290-29.857-34.600-37.269-42.238 -0.062 -0.875 -3.960 -9.367-13.415-15.922-20.060-22.133-26.507-29.105-34.046-36.676-41.661-41.954-41.954 Sulphur Argon -2.656 -0.603 -0.126 -2.222 -0.003 -5.899 Calcium Iron 0.5-1.0KEV:6.18E+00 1.0-1.5:2.50E+01 1.5-2.0:2.38E+01 2.0-2.5:1.88E+01 2.5-3:1.60E+01 3-5:3.16E+01 5-7.5:1.24E+01 7.5-10:4.64E+00 Normalised continuum 0.25 1.000 0.27 1.000 0.30 1.000 0.33 1.000 0.36 1.000 0.39 1.000 0.43 1.000 0.47 1.000 0.62 1.000 0.67 1.000 0.74 1.000 0.81 1.000 0.88 1.000 0.97 1.000 0.98 1.000 0.99 1.000 0.51 1.000 0.56 1.000 1.00 1.000 Emergent continuum - phot/ryd/cm2 (r in) 0.26 2.78E+09 1.00 7.13E+02 0.29 1.62E+09 1.01 7.08E+02 0.33 9.40E+08 1.02 7.03E+02 0.37 5.67E+08 1.10 6.29E+02 3.9 1.74E+00 4.0 1.43E+00 4.2 1.17E+00 4.7 6.37E-01 17.3 9.66E-03 19.5 6.82E-03 22.0 4.82E-03 24.8 3.40E-03 75.3 5.14E-01 81.6 6.00E-01 88.3 6.64E-01 95.7 7.04E-01 3.24E+05 1.82E-10 4.81E+05 5.53E-11 7.15E+05 1.68E-11 1.06E+06 5.13E-12 1.26E+03 3.07E-03 1.87E+03 9.37E-04 2.78E+03 2.85E-04 4.14E+03 8.69E-05 0.42 4.80E+08 0.47 4.06E+08 1.24 4.72E+02 5.3 3.26E-01 27.9 2.40E-03 103.7 7.20E-01 6.15E+03 2.65E-05 9.15E+03 8.06E-06 1.58E+06 1.56E-12 1.40 3.19E+02 5.9 2.15E-01 31.5 1.71E-03 112.3 7.14E-01 2.35E+06 4.75E-13 31.5 1.71E-03 35.5 1.48E-03 40.0 4.04E-03 45.0 1.95E-02 50.5 6.52E-02 54.7 1.24E-01 59.3 2.07E-01 1.57 2.03E+02 1.78 1.16E+02 2.00 5.46E+01 6.7 1.53E-01 7.5 1.09E-01 8.5 7.72E-02 9.5 5.47E-02 121.6 6.91E-01 131.7 6.56E-01 142.7 6.12E-01 173.9 4.89E-01 0.53 3.44E+08 0.60 2.91E+08 1.36E+04 2.45E-06 2.02E+04 7.47E-07 3.49E+06 1.45E-13 5.19E+06 4.41E-14 3.00E+04 2.28E-07 4.46E+04 6.93E-08 0.67 2.46E+08 0.76 1.81E+08 2.25 3.09E+01 0.86 1.12E+08 0.97 5.62E+07 2.54 1.70E+01 2.86 9.15E+00 10.8 3.87E-02 12.1 2.74E-02 258.5 2.72E-01 383.9 1.05E-01 6.63E+04 2.11E-08 9.86E+04 6.43E-09 0.99 4.96E+07 0.99 4.75E+07 3.22 4.84E+00 3.63 2.53E+00 13.6 1.93E-02 15.4 1.37E-02 64.2 3.06E-01 69.5 4.12E-01 570.6 3.28E-02 848.1 1.01E-02 1.47E+05 1.96E-09 2.18E+05 5.96E-10

****	*********************************91Aug03************************************
*	-
* ti	itle Kwan+Krolick Ap.J. 250, 478 BLR model
* cc	onstant gas pressure
* f((nu) -7.32148
* ab	bundances he-1 c-3.699 n-4 o-3.1549 ne-4 mg-4.5229
* cc	ontinue al-10 si-4.4229 s-10 ar-10 ca-10 fe-4.5229
* st	top column density 23
* in	nterpolate (0 -5) (.05 -5) (.1 0) (1 -0.5) (7.353 -2.233)
* CC	ONTINUE (735 -3.233) (800 -015) (8,000,000 -15)
* pr	rint last iteration
* nc	ormalise 1216 100
* it	terate
* pl	lot continuum -3
* hd	den 9.60206
* с	kk.in
* с	cray
*	

Chemical composition He:.100 C:2.00E-04 N:1.00E-04 O:7.00E-04 Ne:1.00E-04 Mg:3.00E-05 Al:1.0E-10 Si:3.78E-05 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:3.00E-05

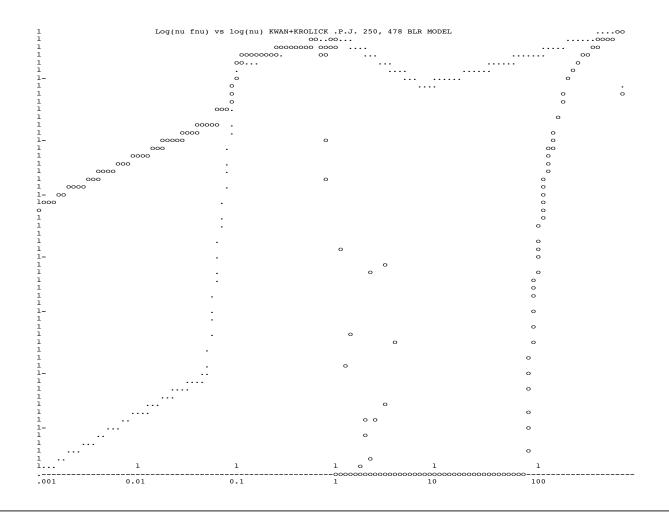
455Cell Peak6.96E+02	Lo 1.00E-05=0.9120cm	Hi-Con:8.92E+02 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 8.7170	Average nu:6.338E+00	P(X-ray): 8.5529	P(BalC): 8.1955	Q(Balmer C): 19.1584
Q(1.0-1.8): 18.3979	Q(1.8-4.0): 17.9425	Q(4.0-20): 17.4232	Q(20): 17.1248	Ion pht flx:3.774E+18
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): 7.7816	Alf(ox): -1.0009	Total lumin: 8.8684
U(1.0):3.147E-02	U(4.0):3.321E-03	T(En-Den):1.343E+03	T(Comp):5.487E+06	nuJnu(912A):1.568E+08
Occ(FarIR):1.969E+02	Occ(H n=6):1.030E-08	Occ(1Ryd):7.228E-09	Occ(4R):7.013E-12	Occ (Nu-hi):3.736E-32
Tbr(FarIR):3.270E+02	Tbr(H n=6):4.573E-05	Tbr(1Ryd):1.142E-03	Tbr(4R):4.437E-06	Tbr (Nu-hi):5.011E-24

1 Te:2.109E+04 Hden:4.000E+09 Ne:4.802E+09 R:1.000E+25 R-R0:8.393E+07 dR:1.679E+08 NTR: 2 Htot:1.543E-04 T912: 3.213E-04###
2.39 4686 0.87 5876 0.01 1909 2.21 1549 58.54 6584 0.00 2326 0.01 3727 0.00 6300 0.00 2798 0.00 1035 6.62
Hydrogen 7.603E-05 9.999E-01 H+0/Hden: 1.000E+00 6.253E-16 H- H2 1.512E-14 7.930E+03 H2 HeHH 3.274E-14 H col den 6.715E+17
H2 5B 3-6 1.272E-10 7.225E-11 1.664E-11 2.113E-11 2.815E-11 3.713E-11 Texc(La); 7.905E+03 T(contn); 1.343E+03 T(diffs) 3.264E-01
He singlet 1.030E-05 4.123E-02 9.588E-01 He I 253 8.947E-08 Comp H, C 8.557E-09 3.289E-11 Fill Fact 1.000E+00 Gam 1/tot 9.294E-01
He singlet 1.021E-05 7.990E+12 7.859E-14 1.067E-13 1.572E-13 2.242E-13 He triplt 8.941E-08 5.423E-11 4.374E-13 9.717E-13 2.638E-13
HeII 4.123E-02 9.318E-10 3.398E-12 5.159E-12 8.225E-12 1.256E-11 1.140E-10 1.644E-09 2.105E-07 PRAD/GAS; 1.696E-02
Pressure NgasTgas; 1.932E+14 P(total); 2.712E-02 P(gas) : 2.667E-02 P(Radtn); 4.523E-04 Rad accel 1.774E+00 Force Mul 2.127E+02
Carbon 0.000E+00 3.295E-04 6.316E-02 3.147E-01 3.202E-01 5.686E-02 1.753E-03 H20+Ydott 0.000E+00 0H+/dott) 0.000E+00
Nitrogen 0.000E+00 3.295E-04 6.316E-02 3.147E-01 3.202E-01 1.834E-02 2.405E-04 02/Votot 0.000E+00 0.2+/dott 0.000E+00
Nitrogen 0.000E+00 3.101E-05 1.350E-02 1.464E-01 5.172E-01 3.090E-01 1.837E-02 6.632E-04 0.000E+00 0.4+/dott 0.000E+00
Nitrogen 0.000E+00 3.101E-05 1.350E-02 1.464E-01 5.172E-01 3.090E-01 1.837E-02 6.622E-04 0.000E+00 0.000E+00
Nitrogen 0.000E+00 3.101E-05 1.350E-02 1.464E-01 5.172E-01 3.090E-01 1.837E-02 6.632E-04 0.000E+00 0.000E+00 0.14/50t-01 0.000E+00
Nitrogen 0.000E+00 3.101E-05 1.350E-02 1.464E-01 5.172E-01 3.000E-01 1.837E-02 6.632E-04 0.000E+00 0.000E+00
Nitrogen 0.000E+00 3.101E-05 1.350E-02 1.464E-01 5.172E-01 3.000E-01 1.537E-04 0.000E+00
Nitrogen 0.000E+00 3.101E-05 1.350E-02 1.466E-01 5.172E-01 3.060E-01 1.837E-02 6.622E-04 0.000E+00
Nagnesium 0 0.000E+00 3.101E-05 2.770E-03 1.668E-02 7.608E-02 3.370E-01 1.318E-01 1.318E-01 1.332E-04 0.000E+00
Nagnesium 0 0.000E+00 1.538E-05 2.645E-03 1.69

Sulphur 0 0.000E+00 7.256E-05 1.010E-02 3.044E-02 4.012E-02 1.687E-01 2.674E-01 2.908E-01 1.550E-01 3.390E-02	2 3.347E-03 1.912E-04
Argon 1 2.897E-05 2.995E-03 1.598E-02 3.291E-02 1.028E-01 2.076E-01 2.543E-01 2.862E-01 8.295E-02 1.326E-02	2 8.861E-04 3.404E-05
Calcium 0 0.000E+00 2.191E-05 1.646E-03 1.062E-02 2.319E-02 1.272E-01 2.843E-01 2.988E-01 1.662E-01 6.469E-02	2.123E-02 2.092E-03
Iron 1 0.000E+00 1.502E-05 1.071E-03 9.922E-03 1.022E-01 2.860E-01 3.886E-01 1.232E-01 6.809E-02 1.739E-02	2 3.098E-03 4.275E-04
#####154 Te:7.137E+03 Hden:2.288E+10 Ne:1.368E+09 R:1.000E+25 R-R0:5.647E+12 dR:1.377E+11 NTR: 6 Htot:7.758E-0)6 T912: 5.053E+05###
6.57 4686 0.06 5876 0.11 1909 3.26 1549 15.03 6584 0.00 2326 0.42 3727 0.00 6300 0.01 2798 2.77 1035	0.45
Hydrogen 9.408E-01 5.916E-02 H+0/Hden: 1.000E+00 2.262E-09 H- H2 3.600E-07 5.901E-09 H2+ HeH+ 1.503E-09	H col den 1.000E+23
H 2SP 3-6 8.096E-07 2.429E-06 1.135E-07 1.837E-08 5.364E-09 2.080E-09 Texc(La); 7.044E+03 T(contn): 1.085E+03	
Helium 9.982E-01 1.841E-03 2.687E-07 He I 2S3 9.035E-09 Comp H, C 1.545E-09 1.397E-12 Fill Fact 1.000E+00) Gam 1/tot 1.013E-02
He singlet 9.982E-01 6.924E-13 3.077E-15 3.727E-15 5.717E-15 8.647E-15 He triplt 8.767E-09 2.659E-10 1.004E-12	2 9.345E-14 1.045E-12

HeII	1.841E-03 2.516E-16 5.041E-19 7.793E-19 1.332E-18 2.208E-18 2.350E-17 6.330E-16 8.996E-14 PRAD/GAS; 2.053E-02
Pressure	NgasTgas; 1.914E+14 P(total): 2.697E-02 P(gas): 2.643E-02 P(Radtn): 5.427E-04 Rad accel 1.300E-02 Force Mul 7.244E+01
Carbon	1.105E-04 9.995E-01 4.191E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 H20+/Otot 0.000E+00 OH+/Ototl 0.000E+00
Nitroger	1.918E-01 8.082E-01 1.682E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen	9.475E-01 5.250E-02 3.155E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.537
Neon	8.949E-01 8.514E-02 2.000E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesiu	n 0 4.820E-04 7.559E-01 2.436E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Alumini	n 0 5.673E-05 9.591E-01 3.191E-02 8.695E-03 1.816E-04 4.742E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Silicon	0 5.155E-05 9.997E-01 2.662E-04 2.277E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Sulphur	0 2.957E-05 9.624E-01 3.761E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Argon	0 7.621E-01 2.363E-01 1.573E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calcium	0 7.90E-05 2.844E-02 9.714E-01 7.463E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Iron	0 1.245E-03 2.344E-02 9.11795E-03 7.731E-06 2.430E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
	tion stopped because column dens reached.
	ry is plane-parallel.
	JII photoionization of H N=2 reached 34.8 percent of the total rate out.
	onization of He 2TriS reached 67.4 percent of the total rate out.
	rgest continuum occupation number was 1.969E+02 at 1.052E-05 Ryd.
	en self ionization by alpha transitions reached 1.8% of the destruction rate for level 3.
	writed state HeII lines are thick.
	ine struc lines are optically thick, largest=1.06E+00
Contir	uum occupation number reached 3.25E+02 for some fine structure transitions.
Freque	ncy out of range of free-free gaunt factor routine.
Balmer	continuum optical depth is 5.47E-01
Balmer	continuum stimulated emission correction to optical depths reached 0.08
Contir	uum optical depth at low nu (1.052E-05 Ryd) was 5.332E+03
The or	tical depth to Rayleigh scattering at 1300A is 5.39E-01

Optical depth to negative hydrogen ion is 1.12E-02 The ratio of radiation to gas pressure reached 8.17E-01. Caused by Lyman alpha. C-This is the last iteration and H(a) optical depth changed by 15.7% (was 2.54E+04). Try another iteration Line radiation pressure capped by thermalization length.



Emission Line Spectrum. Constant Pressure Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2)

				1 (3 ,					
TOTL 4861	6.566 6.3673	H-FB 0	6.104	2.1945	C 4 4659	2.663	0.0008	Ne 4 1602	4.087	0.0211
TOTL 1216	7.762 100.0000	H2+ 0	5.777	1.0349	C 6r 34	3.993	0.0170	Ne 5 3426	3.963	0.0159
TotH 0	8.409 443.5726	HEH+ 0	2.840	0.0012	N 1 1200	2.663	0.0008	Ne 5 3346	3.530	0.0059
BFH1 0	7.603 69.2160	HeFF 0	5.995	1.7076	N 2 6584	3.320	0.0036	Ne 5 2976	3.200	0.0027
BFHx 0	6.907 13.9554	HeFB 0	6.080	2.0755	N 2 6548	2.843	0.0012	Ne 5 1575	3.675	0.0082
BFHe 0	7.805 110.2877	MeFB 0	4.521	0.0574	N 2 5755	3.789	0.0106	Ne 5 1134	5.095	0.2151
TotM 0	8.156 247.3015	MeFF 0	4.930	0.1472	N 2 4239	2.834	0.0012	Ne 6 76	1.827	0.0001
FF H 0	4.288 0.0335	Toff 0	7.196	27.1215	N 2 5680	3.333	0.0037	Ne 6 1007	4.451	0.0489
ComH 0	4.487 0.0530	HeIC 584	2.842	0.0012	N 2 2140	5.483	0.5252	Ne 7 895	3.218	0.0029
н-н 0	6.156 2.4771	esc 584	5.539	0.5975	N 2 1084	3.950	0.0154	Ne 8 774	3.022	0.0018
CA B 4861	7.006 17.5164	He I 504	6.363	3.9865	N 3 1750	6.392	4.2567	Mg 1 4571	2.877	0.0013
CA B 1216	8.537 594.6159	He I 4471	5.026	0.1833	N 3 990	5.274	0.3243	Emis 2798	7.009	17.6452
DU B 4861	7.006 17.5158	TOTL 5876	5.605	0.6965	N 4 1486	6.451	4.8791	Cool 2798	7.122	22.8991
Q(H) 4861	6.253 3.0974	Ca B 5876	5.456	0.4938	N 4 765	5.183	0.2631	Mg 4 4	2.823	0.0011
Q(H) 1216	7.787 105.8999	TOTL10830	6.219	2.8619	N 4 1718	3.902	0.0138	Mg 5 56	2.619	0.0007
TOTL 6563	7.061 19.8636	INWD10830	6.037	1.8794	N 5 1240	6.321	3.6149	Mg 5 2751	3.641	0.0076
TOTL 4861	6.566 6.3673	TOTL 3889	4.926	0.1456	N 7r 25	3.089	0.0021	Mg 6 1806	2.942	0.0015
TOTL 4340	6.099 2.1699	TOTL 7065	5.484	0.5272	O 1 6300	4.454	0.0491	Mg 7 2629	4.402	0.0436
TOTL 4102	5.745 0.9595	CcHE 0	6.217	2.8462	O 1 6363	3.977	0.0164	Mg 8 3	2.679	0.0008
TOTL18751	6.021 1.8143	He I 2	4.866	0.1269	O 1 5577	4.549	0.0612	Mg 9 705	1.939	0.0002
TOTL12818	5.903 1.3820	DevB 2	4.380	0.0415	O 1 7774	4.178	0.0260	Si 2 2335	6.105	2.1993
TOTL10938	5.623 0.7246	He I 5016	4.826	0.1157	6lev 8446	4.707	0.0880	Si 2 1808	5.003	0.1742
TOTL40512	5.189 0.2672	DevB 5016	4.640	0.0754	6lev 1304	6.366	4.0129	Si 3 1207	6.178	2.6039
TOTL26252	5.225 0.2903	He I 3965	4.540	0.0599	6lev 1039	1.894	0.0001	Si 3 1895	6.926	14.5666
TOTL74578	4.532 0.0589	DevB 3965	4.190	0.0268	6lev 4368	3.531	0.0059	PHOT 1895	3.892	0.0135
2 NU 0	6.115 2.2527	He I 3614	4.256	0.0312	6lev 13	3.725	0.0092	Si 4 1397	6.916	14.2384
TOTL 1216	7.762 100.0000	DevB 3614	4.039	0.0189	6lev 11	5.491	0.5352	Si 6 19	4.050	0.0194
TOTL 1026	5.677 0.8221	He I 3448	4.038	0.0188	6lev 29	2.722	0.0009	Si 7 2148	4.592	0.0675
TOTL 973	4.946 0.1524	DevB 3448	3.690	0.0085	TOTL 3727	1.808	0.0001	Si 7 25	3.822	0.0115
TOTL 950	4.531 0.0586	HeII 228	6.122	2.2896	TOTL 7325	3.522	0.0058	Si 7 65	2.013	0.0002
TOTL 938	4.388 0.0422	HE2C 304	2.253	0.0003	O II 2471	3.435	0.0047	Si 8 1446	3.671	0.0081
LA X 1216	6.221 2.8769	ESC 304	5.772	1.0223	O II 7323	3.275	0.0033	Si 9 1985	4.010	0.0177
Ind2 1216	2.647 0.0008	He2C 911	5.685	0.8373	O II 7332	3.160	0.0025	Si 9 949	2.511	0.0006
C13c 6563	5.144 0.2405	TOTL 1640	6.263	3.1684	O II 834	4.081	0.0208	Si 9 3	2.040	0.0002
C14c 4861	4.130 0.0233	TOTL 4686	5.325	0.3654	O 2 4651	4.063	0.0200	Si 9 2	2.135	0.0002
CION 0	7.736 94.1725	TOTL 1216	5.780	1.0412	O 3 1663	7.027	18.3905	Si 9 691	2.351	0.0004
INWD 1216	7.762 99.8228	Ca B 1640	6.077	2.0622	Phot 1663	2.260	0.0003	Si1014300	2.992	0.0017
INWD 6563	6.992 16.9750	DevB 1640	6.076	2.0589	Augr 1663	4.547	0.0609	Ca 2 3933	1.979	0.0002

KWAN+KROLICK AP.J. 250, 478 BLR MODEL Cooling: CION 0:0.212 H FF 0:0.057 H FB 0:0.063 C 4 1549:0.215 Cool 2798:0.051 TOT 0:0.080
Heating: BFH1 0:0.156 BFHe 0:0.249 TotM 0:0.558
IONIZE PARMET: U(1-) -1.5021 U(4-): -2.4787 U(sp): -2.26 Q(ion): 16.182 L(ion): 8.138 Q(low): 19.46 P(low) 8.25
ENERGY BUDGET: Heat: 8.409 Coolg: 8.411 Error: 0.3% Compt H: 4.487 WorkF: 10.635 F-F H 4.288 PRADMX:8.17E-01 Column density H12:1.000E+23 H II:1.974E+22 HI:8.028E+22 H-: 2.876E+14 H2: 3.010E+16 H2+:7.289E+14 He H+:1.106E+14
OH: 0.000E+00 Heff:8.517E+22
<pre><nd>:1.750E+10 <tp>:1.04E+04 <to3>:1.73E+04 Ne:5.599E+09 ti(snd):6.92E+06 NeN+d1:8.00E+31 <t(c3)>:1.65E+04 <e(c3)>:5.65E+04 He/Ha:8.53E-02 = 0.88*true N/Oap:0.000E+00 = 0.00true T(O3R):1.000E+01 L THIN:1.62E-02 <t(s2)>:7.35E+03 <e(s2)>:3.03E+04</e(s2)></t(s2)></e(c3)></t(c3)></to3></tp></nd></pre>
T He+1:169E+04 EHe+15.52E+09 T(0+):7.52E+03 EO+3.52E+09 iter/an: 3.040 Te-100*7.14E+03 Te-high:2.38E+04 Hu/an:4.23BE+04
<a>:0.00E+00 erdeFe0.0E+00 Tcompt8.64E-06 Tthr1.31E+02 <tden>: 7.94E+03 <dens>:4.09E-14 <mol>:1.10E+00</mol></dens></tden>
Mean Jeans l(cm)2.20E+16 M(sun)1.50E+02 smallest: len(cm):2.09E+16 M(sun):1.28E+02 Alf(ox-tran): -1.6107
Optical Depths: CONTN; COMP: 1.36E-02 H-: 1.12E-02 R(1300): 5.39E-01 H2+ 5.10E-03 HeTri:2.39E-01
Pfa:1.42E-02 Pa:1.66E-02 Ba:4.93E-02 Hb:3.23E-02 La:1.33E+01 lr:5.053E+05 1.8:1.69E+05 4.:2.749E+04 21R:3.003E+02 10830: 5.24E+02 3889: 2.42E+01 5876: 7.97E+01 7065: 4.39E+01
1550: 3.58E+02 2806; 2.50E+06 774: 1.57E+01 1240: 2.39E+03 1035: 3.31E+03 1335: 2.96E+06 977: 1.56E+05 1397: 2.82E+04
789: 9.72E+03 1207: 6.31E+04 1085: 2.61E+05 1194: 3.29E-03 1909: 6.23E-02 1895: 1.69E+00 2326: 1.48E+00 1666: 9.52E-01
1750: 3.68E-03 1025: 6.05E+05 352: 1.26E+01 347: 1.00E-20 1860: 5.28E-01 630: 2.04E+04 834: 1.73E+06 835: 4.63E+01 1808: 5.30E+06 1256: 4.69E+01 -3: 1.73E+05 -48: 4.79E+00 3934: 6.21E-01 3969: 3.13E-01 8498: 1.62E+03 8542: 1.47E+02
8662: 8.23E-03 353: 3.00E+01 1304: 2.07E+06 1122: 1.56E+03 990: 1.62E+04 1402: 1.30E-01 1214: 1.10E-01 1486: 4.21E-02
2335: 1.27E+01 1406: 2.61E-06 1656: 5.06E+02 9830: 8.43E-08 8727: 2.50E-06 6300: 5.49E-03 5577: 8.16E-03 7291: 5.08E-08
7324: 3.52E-08 1039: 2.94E+05 -8446: 4.33E+02 -4368: 1.67E+00 -132: 6.13E+00 -113: 2.70E+01 -29: 2.95E=02 -46: 6.45E-01 -245: 1.15E-01 765: 2.55E+04 -1198: 1.01E-06 786: 3.01E-03
245: 1.01E-01 /05: 2.06F04 -1195: 1.01E-02 /05: 0.10E-02 /05: 1.01E-01 /063: 1.06E+00 /088: 9.36E-03 /052: 1.58E-02 /05: 1.04E-03 /046: 3.53E-01 /063: 1.06E+00 /088: 9.36E-03 /052: 1.58E-02
026: 4.14E-03 NE13: 1.00E-01 NE36: 1.16E-02 NE16: 3.69E-02 MG4: 1.74E-03 MG14: 3.91E-04 MG6: 2.27E-04 SI35: 1.32E-01
S19: 3.35E-08 S34: 1.59E-08 S11: 5.68E-09 AR7: 4.02E-07 AR9: 1.65E-08 AR22: 4.84E-09 AR13: 8.77E-10 AR8: 1.68E-09 CA3: 1.24E-08 CA12: 1.12E-09 CA4: 4.60E-09 Ne14: 1.12E-03 Ne24: 5.51E-04 S31: 1.04E-03 S4: 8.91E-03 Fe7: 6.51E-07
CAS: 1.24E-00 CAI: 1.1EE-09 CA: 4.00E-09 Wei4: 1.1EE-05 Ne24: 5.3E-04 Sis: 1.04E-03 Si4: 6.9IE-03 Fe/: 6.3IE-07 Fe61:-3.40E-02 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 6.06E-04 Si65: 1.90E-04 C610: 4.53E-06 C370: 3.01E-06
Old hydro optical depths: 1 5.13E+05 2 6.53E-01 3 6.44E-02 4 1.68E-02 5 5.20E-03 6 2.26E-03 7 2.03E-03
Lines: 2-15.62E+09 3-22.54E+04 4-3 4.37E+03 5-4 1.65E+03 6-5 1.10E+03 7-6 6.76E+01 8-7 6.63E+01
New hydro optical depths: 1 5.05E+05 2 5.47E-01 3 5.76E-02 4 1.57E-02 5 5.03E-03 6 2.25E-03 7 2.18E-03
Lines: 2-1 5.55E+09 3-2 2.14E+04 4-3 3.88E+03 5-4 1.73E+03 6-5 1.05E+03 7-6 6.62E+01 8-7 6.99E+01
Old He Is optical depths: 1 1.71E+05 2 2.66E-01 3 3.14E-10 4-3.42E-09 5-7.28E-09 6-1.16E-08 7-5.44E-08
Lines: 2-1 4.17E+08 3-2 6.83E+02 4-3 9.51E=04 5-4 3.15E=04 6-5-1.45E=03 7-6 6.03E=03 8-7 9.88E=02 New HE Is optical depths: 1 1.69E+05 2 2.24E=01 3 7.91E=10 4-4.52E=09 5-9.71E=09 6-1.53E=08 7-6.66E=08
New HE Is optical depths: 1 1.69E+05 2 2.24E-01 3 7.91E-10 4-4.52E-09 5-9.71E-09 6-1.53E-08 7-6.66E-08 Lines: 2-1 4.14E+08 3-2 1.08E-01 4-3 1.48E-03 5-4 4.62E-04 6-5-2.03E-03 7-6 8.34E-03 8-7 1.37E-01
Old He II optical depths: 1 2.77E+04 2 5.13E+05 3 1.12E-09 4-2.25E-09 5-4.60E-09 6-7.74E-09 7-7.28E-08 Lines: 2-1 9.54E+06 3-2 3.08E+00 4-3 2.56E-04 5-4 2.56E-05 6-5.8.70E-05 7-6 3.31E-04 8-7 5.08E-03
New HE II optical depths: 1 2.75E+06 2 5.05E+05 3 3.51E-09 4-2.21E-09 5-4.68E-09 6-7.94E-09 7-7.50E-08
Lines: 2-1 1.21E+07 3-2 4.78E+00 4-3 5.59E-04 5-4 4.37E-05 6-5-7.50E-05 7-6 3.43E-04 8-7 5.23E-03
Hydrogen -0.095 -0.705 Log10 Mean Ionisation (over volume)
Helium -0.026 -1.280 -2.180
Carbon -3.716 -0.026 -1.488 -1.684 -2.497 -3.364 -4.912 Nitrogen -0.977 -0.076 -1.502 -1.783 -2.398 -2.482 -3.773 -5.660
Nillogen $-0.088 - 0.892 - 1.352 - 1.592 - 2.5402 - 3.773 - 3.660$ Oxygen $-0.088 - 0.892 - 1.355 - 2.154 - 2.574 - 2.954 - 3.361 - 5.441$
Neon -0.105 -0.897 -1.135 -2.139 -2.207 -2.681 -3.964 -4.420 -5.375
Magnesium -3.265 -0.296 -0.326 -2.067 -2.526 -2.334 -2.401 -2.914 -3.756 -4.742 -5.949 Aluminum -3.982 -0.042 -1.309 -1.585 -2.369 -2.276 -2.275 -2.629 -3.470 -4.565 -5.804
Aluminum $-3.982 -0.042 -1.309 -1.585 -2.309 -2.276 -2.275 -2.629 -3.470 -4.505 -5.804$ Silicon $-4.078 -0.025 -1.791 -1.677 -2.396 -2.293 -2.265 -2.427 -2.966 -3.913 -5.101 -6.444$
Sulphur -4.353 -0.040 -1.279 -1.810 -2.498 -2.226 -2.369 -2.421 -2.731 -3.389 -4.372 -5.586
Argon -0.135 -0.683 -1.704 -1.863 -2.551 -2.132 -2.308 -2.302 -2.370 -2.926 -3.736 -4.894 -6.305
Calcium -3.792 -1.469 -0.029 -2.044 -2.421 -2.209 -2.324 -2.434 -2.753 -3.167 -3.654 -4.629 Iron -2.652 -0.029 -2.073 -1.509 -2.275 -2.085 -2.348 -2.446 -2.979 -3.238 -3.819 -4.541 -5.371

INWD 4861	6.492	5.3602	Ca B 4686	5.181	0.2619	Rec 1663	4.826	0.1158	Ca2K 3934	1.799	ο.
INWD 4861 INWD18751	5.944	1.5201	Ca B 4686 DevB 4686	5.181	0.2598	Rec 1663 O 3 5007	4.826	0.0392	Ca2K 3934 Fe 2 48	7.143	24.
Strk 1216	4.488	0.0531	DevB 4686 Mion 0	2.220	0.2598	0 3 5007	4.355	0.0392	Fe 2 48 Fe 2 7	5.215	24.
Strk 6563 Strk 4861	6.368 5.806	4.0362	C 1 1656 REC 1656	2.251	0.0003	LOST 5007 TOTL 4363	4.002	0.0173	Emis 3 Cool 3	6.744 6.984	9. 16.
Strk18751	5.294	0.3400	C 2 2326	6.193	2.6975	0 3 2321	4.231	0.0294	TOT 0	7.311	35.
Strk40512	4.424	0.0459	INWD 2326	5.978	1.6437	C EX 5592	2.697	0.0009	FEIR 0	2.250	0.
Dest 1216	6.415	4.4967	C 2 1335	5.400	0.4339	0 3 834	6.021	1.8115	Fe 3 0	3.378	0.
Dest 6563	6.267	3.1941	REC 1335	5.140	0.2387	0 3 3341	3.394	0.0043	Fe 3 5270	2.698	0.
Dest40516	2.487	0.0005	C II 3134	2.966	0.0016	0 4 1402	6.445	4.8099	Fe 3 4658	2.943	0.
Dest 4861	5.495	0.5405	C 2 4267	3.488	0.0053	CONT 1401	4.898	0.1366	Fe 3 1122	4.140	0.
Dest18751	4.068	0.0202	TOTL 977	6.639	7.5298	O 4 789	5.978	1.6440	Fe 5 3892	3.068	0.
nFnu 4860	7.302	34.6297	C3 C 977	6.625	7.2933	0 4 3412	3.793	0.0107	Fe 6 0	3.780	0.
nFnu 1215	6.226	2.9081	C3 R 977	5.136	0.2365	O 5 630	5.041	0.1897	Fe 6 5177	3.329	0.
Inci 4861		117.3445	TOTL 1909	7.079	20.7397	TOTL 1218	6.250	3.0713	Fe 7 6087	3.252	0.
Inci 1216		234.6889	INWD 1909	6.781	10.4319	0 5 1218	6.250	3.0711	Fe10 6374	4.335	0.
BAC 0	7.351	38.7734	C 3 1907	3.108	0.0022	0 5 1214	2.162	0.0003	Coll 6374	4.330	Ο.
PAC 0	7.069	20.2496	C 3 1909	7.079	20.7374	0 5 5112	2.678	0.0008	Pump 6374	2.385	Ο.
H FF 0	7.165	25.2667	C3 R 1909	4.644	0.0762	O 6 1035	6.217	2.8451	Fe11 7892	3.625	0.
H FB 0	7.208	27.9180	Phot 1909	4.424	0.0459	Ne 2 128	2.679	0.0008	Coll 7892	3.621	Ο.
Cool 1216	6.669	8.0544	C 3 2297	4.621	0.0721	Ne 3 156	2.254	0.0003	Fe11 2649	3.215	Ο.
Heat 1216	6.264	3.1750	C 3 4187	2.753	0.0010	Ne 3 3869	4.373	0.0408	Fe12 1242	2.357	Ο.
Crst 960	4.635	0.0745	C 3 4649	3.598	0.0069	Ne 3 3968	3.860	0.0125	Fe12 2170	3.329	0.
Cool 6563	6.860	12.5157	C 4 1549	7.743	95.6785	Ne 3 3343	3.816	0.0113	Fe12 2568	1.856	Ο.
Crst 4861	5.929	1.4656	INWD 1549	7.521	57.3062	Ne 3 1815	3.955	0.0156	Totl 2	6.087	2.
Cool18751	6.247	3.0488	DEST 1549	5.365	0.4000	Ne 4 2424	2.195	0.0003	AugC 2	6.087	2.
Crst 0	6.089	2.1199	C4 r 1549	4.304	0.0348	Ne 4 4720	3.472	0.0051			
es with nega	tive i	ntensities;	205 T OI	0							

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
Hydrogen	-0.095	-0.705				Lo	og10 Me	an Ionis	ation	(over r	adius)						
Helium	-0.026	-1.280	-2.180				-										
Carbon			-1.488														
Nitrogen																	
Oxygen			-1.355														
Neon								-4.420									
Magnesium																	
Aluminum																	
	-4.078 -4.353																
Argon								-2.421									
	-3.792																
Tron								-2.446									
11011	-2.052	-0.025	-2.075	-1.505	-2.275	-2.005	-2.540	-2.440	-2.575	-5.250	-5.015		-5.571				
0.5-1.0KE	V:4.25E-	+06 1.0	-1.5:2.5	56E+12 1	.5-2.0:	9.80E+3	3 2.0-	2.5:4.37	/E+14 2	.5-3:9.	95E+14	3-5:5.0	4E+15 5	-7.5:5	5.13E+15	7.5-10	:3.41E+15
								malised									
0.25 1.		.27 1.2		30 1.142		1.060		1.008		0.979	0.43 0		0.47 0.		0.51 0.9		.56 0.956
0.62 0.	926 0.	.67 0.8	59 0.1	74 0.020	0.81	0.789	0.88	0.830	0.97	0.730	0.98 0	.737	0.99 0.	738	1.00 0.7	40	
Inward co	ntinua	(at hoad	1 of Bal	mor Tr		ior.	5 468+07	1 1 21	R+07							
inwaru co	ncinua ((nurnu)	at nead	I OI BAI	mer, by	man sei	tes,	5.405+07	4.51	E+07							
Outwrd co	ntinua	(nuFnu)	at head	d of Bal	mer. Ly	man sei	ies:	6.09E+07	0.00	E+00							
		(,					,										
						Eme	ergent	continuu	um - ph	ot/ryd/	cm2 (r	in)					
0.26 7.	51E+19	0.86 7	.90E+18	1.6	2.97E+	09	4.2 0.	00E+00	13.7	0.00E+	00 4	.50E+01	7.68E-	10	1.04E+02	2 1.44E	+11
0.29 5.	43E+19	0.97 5	.57E+18	1.8	1.24E-	16	4.7 0.	00E+00	15.4	1.20-2	88 5	.05E+01	2.89E-	03	1.12E+02	2 5.58E	+11
			.44E+18) 1.92E+		5.3 0.			5.79-1			2.46E-		1.22E+02		
0.37 3.			.39E+18		1.13E+		5.9 0.			1.34-1			2.24E+		1.32E+02		
0.42 2.			.00E+00		4.43E-		6.7 4.			7.55E-			2.13E+		1.43E+02		
			.73E-09		3.18E-		7.5 0.			1.68E-			3.16E+		1.74E+02		
	79E+19				9.22E-		8.5 4.			2.47E-			1.72E+		2.59E+02		
0.60 1.			.08E-10		1.83E+		9.5 0.			8.96E-			4.18E+		3.84E+02		
0.67 1.			.51E-11		0.00E+		10.8 0.			4.78E-			5.35E+		5.71E+02		
0.76 3.	63E+16	1.40 7	.UUE-13	4.0	0.00E+	00 .	2.1 0.	005+00	40.0	2.10E-	19 9	.5/E+01	4.08E+	10	8.49E+02	2.34E	+01

**************************************	* *
*	*
* title Ly alpha forest cloud	*
* c ionized by AGN power law plus cosmic background	*
* background, $z=2$; this includes both black body and AGN parts	*
* double ; mimic two-siced photoionization	*
* hden -2	*
* stop neutral column density 15	*
* metals -1.5 ;reduce all heavy elements by 1.5 dsex	*
* faint -1	*
* iterate ; must iterate since optically thin	*
* print last	*
* c lalpha.in	*
* c cray	*
*	*

Chemical composition He:.098 C:1.15E-05 N:3.54E-06 O:2.69E-05 Ne:3.89E-06 Mg:1.20E-06 Al:9.3E-08 Si:1.12E-06 S:5.12E-07 A:1.1E-07 Ca:7.2E-08 Fe:1.48E-06

546Cell Peak2.03E-04	Lo 1.00E-05=0.9106cm	Hi-Con:7.34E+06 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): -3.4516	Average nu:1.584E+01	P(X-ray): -3.8828	P(BalC): -4.5096	Q(Balmer C): 6.4875
Q(1.0-1.8): 5.6607	Q(1.8-4.0): 5.4919	Q(4.0-20): 5.3137	Q(20): 4.6992	Ion pht flx:1.024E+06
L(gam ray): -3.8090	Q(gam ray): 2.1572	L(Infred): 0.0267	Alf(ox): -1.0000	Total lumin: 0.0269
U(1.0):3.417E-03	U(4.0):8.537E-04	T(En-Den):8.276E+00	T(Comp):2.248E+04	nuJnu(912A):2.231E-05
Occ(FarIR):4.574E+00	Occ(H n=6):1.648E-15	Occ(1Ryd):1.029E-21	Occ(4R):3.997E-24	Occ (Nu-hi):4.305E-49
Tbr(FarIR):7.606E+00	Tbr(H n=6):7.317E-12	Tbr(1Ryd):1.625E-16	Tbr(4R):2.529E-18	Tbr (Nu-hi):4.753E-37

1 Te:2.138E+04 Hden:1.000E-02 Ne:1.183E-02 R:1.000E+25 R-R0:8.762E+17 dR:1.752E+18 NTR: 2 Htot:6.190E-28 T912: 1.661E-04###
-10.66 4686 0.54 5876 0.01 1909 1.23 1549 1.30 6584 0.01 5007 1.15 3727 0.06 6300 0.00 2798 0.01 1035 0.02
Hydrogen 1.506E-03 9.985E-01 H+0/Hden: 1.000E+00 3.136E-11 H- H2 2.670E-12 2.227E-11 H2+ HeH+ 1.028E-11 H col den 1.752E+16
H 2SP 3-6 1.847E-16 9.555E-23 3.606E-23 3.619E-23 4.601E-23 5.895E-23 Texc(La); 2.611E+03 T(contn): 8.276E+00 T(diffs): 2.489E+02
Helium 2.528E-04 1.229E-01 8.768E-01 He I 2S3 1.611E-12 Comp H, C 1.269E-31 1.207E-31 Fill Fact 1.000E+00 Gam 1/tot 6.005E-01
He singlet 2.528E-04 1.750E-18 3.798E-25 5.117E-25 7.382E-25 1.031E-24 He triplt 1.611E-12 1.235E-23 3.388E-25 2.148E-24 4.498E-25
HeII 1.229E-01 2.715E-17 8.352E-24 1.127E-23 1.596E-23 2.211E-23 1.699E-22 1.167E-21 2.230E-19 PRAD/GAS; 5.846E-06
Pressure NgasTgas; 4.820E+02 P(total): 6.655E-14 P(gas): 6.655E-14 P(Radtn): 3.890E-19 Rad accel 1.544E-11 Force Mul 1.280E+00
Carbon 1.636E-04 5.293E-02 6.110E-01 2.728E-01 6.024E-02 2.817E-03 1.925E-05 H2O+/Otot 0.000E+00 OH+/Ototl 0.000E+00
Nitrogen 2.931E-05 1.840E-02 4.243E-01 4.225E-01 8.817E-02 4.633E-02 3.360E-04 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 1.251E-05 1.157E-02 4.000E-01 4.276E-01 1.339E-01 2.226E-02 4.655E-03 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.622
Neon 1.904E-06 1.450E-03 1.724E-01 4.034E-01 3.550E-01 6.659E-02 1.027E-03 1.435E-04 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 5.486E-05 3.550E-03 1.288E-01 2.618E-01 1.752E-01 2.948E-01 1.220E-01 1.316E-02 6.067E-04 2.095E-05 0.000E+00 0.000E+00
Aluminium 0 7.842E-04 8.028E-02 4.639E-02 1.825E-01 1.635E-01 3.114E-01 1.847E-01 2.917E-02 1.218E-03 2.896E-05 0.000E+00 0.000E+00
Silicon 0 1.453E-04 1.648E-02 2.170E-01 1.005E-01 1.276E-01 2.742E-01 2.026E-01 5.624E-02 5.104E-03 1.673E-04 0.000E+00 0.000E+00
Sulphur 0 2.316E-05 4.995E-02 4.039E-01 1.900E-01 9.689E-02 1.146E-01 1.047E-01 3.444E-02 5.232E-03 3.168E-04 8.832E-06 0.000E+00
Argon 1 1.228E-02 2.273E-01 2.136E-01 1.264E-01 1.645E-01 1.377E-01 7.289E-02 4.195E-02 3.277E-03 1.448E-04 2.634E-06 2.865E-08
Calcium 0 1.846E-04 7.850E-03 7.713E-02 1.472E-01 9.252E-02 2.602E-01 2.570E-01 1.216E-01 2.985E-02 5.475E-03 8.916E-04 2.256E-05
Iron 0 0.000E+00 1.234E-05 2.037E-03 2.165E-02 6.407E-02 3.058E-01 3.787E-01 2.015E-01 2.157E-02 4.209E-03 3.605E-04 2.420E-05
5 Te:2.140E+04 Hden:1.000E-02 Ne:1.182E-02 R:1.000E+25 R-R0:4.979E+19 dR:3.292E+19 NTR: 1 Htot:6.224E-28 T912: 6.296E-03###
-9.18 4686 0.51 5876 0.01 1909 1.53 1549 1.60 6584 0.01 5007 1.43 3727 0.07 6300 0.00 2798 0.02 1035 0.03
Hydrogen 1.511E-03 9.985E-01 H+0/Hden: 1.000E+00 3.215E-11 H- H2 2.682E-12 2.234E-11 H2+ HeH+ 1.021E-11 H col den 6.625E+17
H 2SP 3-6 1.613E-16 4.255E-22 2.481E-23 2.670E-23 3.800E-23 5.179E-23 Texc(La); 2.700E+03 T(contn): 8.276E+00 T(diffs): 2.439E+02
Helium 2.531E-04 1.241E-01 8.756E-01 He I 2S3 1.614E-12 Comp H, C 1.269E-31 1.208E-31 Fill Fact 1.000E+00 Gam 1/tot 5.993E-01
He singlet 2.531E-04 1.705E-18 3.535E-25 4.954E-25 7.277E-25 1.026E-24 He triplt 1.614E-12 1.236E-23 3.399E-25 2.150E-24 4.485E-25
HeII 1.241E-01 2.044E-17 5.428E-24 8.007E-24 1.238E-23 1.839E-23 1.504E-22 1.185E-21 2.227E-19 PRAD/GAS; 2.632E-05
Pressure NgasTgas; 4.875E+02 P(total): 6.731E-14 P(gas): 6.730E-14 P(Radtn): 1.771E-18 Rad accel 1.545E-11 Force Mul 1.281E+00
Carbon 1.628E-04 5.263E-02 6.127E-01 2.717E-01 6.001E-02 2.807E-03 1.918E-05 H20+/Otot 0.000E+00 OH+/Ototl 0.000E+00

Nitrogen	2.906E-05 1.826E-0	2 4.260E-01 4.214E-01	1 8.781E-02 4.617E-0	2 3.349E-04 0.000E+00	02/0totl:	0.000E+00 02+/Otot:	0.000E+00
Oxygen	1.235E-05 1.140E-0	2 4.015E-01 4.268E-0	1 1.335E-01 2.218E-0	2 4.640E-03 0.000E+00	0.000E+00	Hex(tot): 0.000E+00	A:-12.622
Neon	1.833E-06 1.425E-0	3 1.730E-01 4.034E-0	1 3.545E-01 6.648E-0	2 1.026E-03 1.432E-04	0.000E+00	0.000E+00 0.000E+00	
Magnesium C	5.498E-05 3.562E-0	3 1.292E-01 2.619E-0	1 1.750E-01 2.945E-0	1 1.219E-01 1.315E-02	6.063E-04	2.094E-05 0.000E+00	0.000E+00
Aluminium C	0 7.818E-04 8.027E-0	2 4.639E-02 1.826E-0	1 1.635E-01 3.114E-0	1 1.847E-01 2.917E-02	1.218E-03	2.897E-05 0.000E+00	0.000E+00
Silicon (0 1.432E-04 1.647E-0	2 2.166E-01 1.010E-0	1 1.275E-01 2.741E-0	1 2.026E-01 5.623E-02	5.104E-03	1.673E-04 0.000E+00	0.000E+00
Sulphur 0	2.147E-05 4.968E-0	2 4.029E-01 1.910E-0	1 9.678E-02 1.148E-0	1 1.048E-01 3.447E-02	5.236E-03	3.171E-04 0.000E+00	0.000E+00
Argon 0	0 7.314E-06 1.205E-0	2 2.258E-01 2.145E-0	1 1.264E-01 1.649E-0	1 1.379E-01 7.303E-02	4.202E-02	3.283E-03 1.451E-04	0.000E+00
Calcium C	1.852E-04 7.882E-0	3 7.751E-02 1.474E-0	1 9.248E-02 2.601E-0	1 2.567E-01 1.215E-01	2.983E-02	5.470E-03 8.910E-04	2.254E-05
Iron 0	0.000E+00 1.223E-0	5 2.024E-03 2.176E-02	2 6.418E-02 3.059E-0	1 3.786E-01 2.014E-01	2.156E-02	4.207E-03 3.605E-04	2.420E-05
Calculati	ion stopped because	column dens reached.					
Geometrv	is plane-parallel.						

Geometry is plane-parallel. 17he largest continuum occupation number was 4.574E+00 at 1.053E-05 Ryd. Continuum occupation number reached 5.94E-02 for some fine structure transitions. Frequency out of range of free-free gaunt factor routine. OI negative level populations 10 times.

nden -2
stop neutral column density 15
metals -1.5 ;reduce all heavy elements by 1.5 dsex
faint -1 Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2) TOTL 973 -8.966 1.6257 TOTL 973 -8.966 1.6257 TOTL 938 -9.231 0.8829 Cl3c 6563 -9.199 0.9510 CION 0 -8.614 3.6537 INWD 1216 -7.546 42.7599 INWD 6563 -8.921 1.8055 INWD 4861 -9.478 0.5000 INWD18751-10.036 0.1384 e sc 6563 -9.992 0.1533 e sc 4861 -9.708 0.2946 e sc18751 -9.735 0.2771 Pru 4860 -8.334 6.9654 C 3 1907 -9.212 C 3 1909 -9.397 C 4 1549 -8.972 INWD 1549 -9.189 N 4 1486-10.086 O 3 1663 -9.853 O 3 5007 -9.023 O 3 4959 -9.500 O 3 800-10.048 O 4 26 -9.330 O 4 1402 -9.869 TOTT, 1218-10.136 $\begin{array}{ccccc} \text{Cool} & 1216 & -7.700\\ \text{Crst} & 960 & -9.709\\ \text{HeFF} & 0 & -9.135\\ \text{HeFB} & 0 & -8.972\\ \text{TOFF} & 0 & -8.554\\ \text{esc} & 584 & -9.626\\ \text{HeII} & 228 & -7.594\\ \text{He2C} & 911 & -8.500\\ \text{TOTL} & 1640 & -8.492\\ \text{TOTL} & 4686 & -9.469\\ \text{TOTL} & 1640 & -8.459\\ \text{TOTL} & 126 & -8.911\\ \text{Ca B} & 1640 & -8.459\\ \text{DevB} & 1640 & -8.459\\ \text{DevB} & 1640 & -8.459\\ \text{DevB} & 1646 & -9.356\\ \text{DevB} & 4686 & -9.354\\ \end{array}$ TOTL 4861 -9.177 1.0000 Cool 1216 -7.700 29.9987 0.9233 0.2938 1.1019 1.6026 4.1979 0.9233 0.6034 1.6043 0.9731 0.1233 0.3560 0.2109 0.6146 1,4255 38.3187 4.7501 4.8449 0.4752 0.1347 0.7033 Q(H) 1216 -4.779******** TOTL 6563 -8.620 3.6111 0.5108 0.2033 TOTL 1218-10.136 Ne 4 2424 -9.947 Ne 5 3426-10.075 3.6111 1.8440 0.1101 TOTL 4861 -9.177 TOTL 4340 -9.510 TOTL 4102 -9.774 TOTL18751 -9.735 nFnu 4860 -8.334 6.9654 nFnu 1215 -8.888 1.9443 Inci 4861 -4.652******** Inci 1216 -4.652******** 1.0000 5.2312 0.1700 0.2529 0.6631 Ne 5 242 -9.942 Ne 5 143-10.008 0.1717 0.2769 0.6514 0.1475 TOTL12818-10.041 2 NU 0 -7.829 TOTL 1216 -7.455 TOTL 1026 -8.718 BA C PA C H FF H FB 0 -8.612 0 -9.158 0 -8.687 0 -8.387 3.6777 1.0463 3.0945 6.1710 TOTL 1977 -9.547 C3 C 977 -9.549 TOTL 1909 -8.993 INWD 1909 -9.294 Si 3 1895 -9.844 S 3 9532-10.173 0.1368 0.4271 0.2153 0.4271 0.4250 1.5267 0.7634 22.2846 0.1009 2.8813

LY ALPHA FOREST CLOUD
Cooling: CION 0:0.059 H FF 0:0.050 H FB 0:0.100 Cool 1216:0.486
Heating: BFH1 0:0.329 BFHe 0:0.663
IONIZE PARMET: U(1-) -2.4664 U(4-): -3.0687 U(sp): -2.47 Q(ion): 6.009 L(ion): -3.452 Q(low): 14.53 P(low) 0.03
ENERGY BUDGET: Heat: -7.386 Coolg: -7.387 Error: 0.2% Compt H: -11.075 WorkF: -6.928 F-F H-14.178 PRADMX:7.98E-05
Column density H12:6.625E+17 H II:6.615E+17 HI:1.000E+15 H=: 2.124E+07 H2: 1.775E+06 H2+:1.479E+07 He H+:6.754E+06
OH: 0.00E+00 Heff:2.528E+16
<pre><nh>:1.000E-02 <tp>:2.14E+04 <to3>:2.14E+04 Ne:1.182E-02 ti(snd):3.88E+13 NeN+dl:7.82E+15 <t(c3)>:2.14E+04 <e(c3)>:1.18E-04</e(c3)></t(c3)></to3></tp></nh></pre>
He/Ha:4.75E-02 = 0.48*true N/Oap:1.29E-01 = 0.98true T(O3R):2.047E+04 L THIN:1.00E+30 <t(s2)>:2.14E+04 <e(s2)>:1.18E-02</e(s2)></t(s2)>
T He+:2.14E+04 EHe+:1.18E-02 T(O+):2.14E+04 EO+:1.18E-02 iter/zn: 1.000 Te-low:2.14E+04 Te-high:2.14E+04 Hlu/zn:1.00E+0
<a>:0.00E+00 erdeFe3.7E+25 Tcompt3.71E+11 Tthr1.73E+14 <tden>: 2.14E+04 <dens>:2.31E-26 <mol>:6.11E-01</mol></dens></tden>
Mean Jeans l(cm)7.70E+22 M(sun)2.78E+09 smallest: len(cm):7.70E+22 M(sun):2.78E+09 Alf(ox-tran): -1.0001
Optical Depths: CONTN; COMP: 5.21E-07 H-: 8.28E-10 R(1300): 6.71E-09 H2+ 1.04E-10 HeTri:5.21E-07
Pfai5.21E-07 Pai5.21E-07 Pai5.22E-07 Hb:5.22E-07 Hb:5.22E-07 La:6.89E-07 lr:6.296E-03 1.8:1.32E-03 4.:1.275E-02 21R:1.245E-04
10830: 9.74E-08 3889: 4.15E-09 5876: 4.63E-19 7065: 2.60E-19
1550: 1.68E-01 2800: 2.73E-03 774: 1.56E-05 1240: 1.19E-02 1035: 1.68E-02 1335: 3.69E-02 977: 9.68E-01 1397: 2.36E-02
789: 1.45E-01 1207: 1.41E-01 1085: 7.83E-04 1194: 5.77E-04 1909: 3.86E-07 1895: 3.76E-06 2326: 1.85E-08 1666: 1.97E-06
1750: 1.03E-08 1025: 1.37E-06 352: 3.04E-05 347: 1.00E-20 1860: 2.06E-03 630: 2.53E-01 834: 2.33E-02 835: 9.58E-02
1808: 1.07E-02 1256: 5.09E-04 -3: 4.33E-07 -48: 1.49E-19 3934: 4.94E-04 3969: 2.49E-04 8498: 1.18E-14 8542: 1.06E-13
8662: 5.99E-14 353: 2.38E-06 1304: 4.69E-06 1122: 7.92E-05 990: 4.55E-02 1402: 1.94E-06 1214: 1.36E-06 1486: 2.35E-07
2335: 2.55E-08 1406: 9.74E-07 1656: 9.59E-05 9830: 1.60E-14 8727: 1.78E-18 6300: 1.24E-14 5577: 1.13E-20 7291: 3.30E-11
7324: 2.298-11 1039: 6.66E-07 -8446: 1.00E-20 -4368: 1.00E-20 -132: 1.00E-20 -113: 1.00E-20 -29: 1.00E-20 -46: 1.00E-20
-245: 2.22E-11 105: 0.00E-07 -040: 1.00E-20 -102: 1.00E-20 -113: 1.00E-20 -25: 1.00E-20 -40: 1.00E-20 -20: 1.00E-20 -20: 1.00E-20 -40: 1.00E-20 -20: 1.00E-20: 1.00E-2
C157: 2.98E-07 N122: 5.52E-12 N205: 1.72E-07 N57: 7.99E-07 O146:-1.99E-16 O63: 1.43E-10 O88: 1.85E-05 O52: 1.24E-10
026: 6.55E-06 NE13: 1.77E-09 NE36:-3.03E-14 NE16: 3.24E-07 MG4: 1.10E-07 MG14:-4.93E-16 MG6: 1.10E-07 SI35: 1.41E-08
S19: 1.06E-12 S34: 4.99E-07 S11: 7.81E-08 AR7: 5.95E-10 AR9: 1.66E-08 AR22:-5.96E-16 AR13: 3.71E-08 AR8: 6.40E-16
CA3: 4.81E-09 CA12:-1.06E-17 CA4: 4.48E-09 Ne14: 1.20E-12 Ne24: 2.48E-06 Si3: 1.01E-18 Si4: 1.21E-08 Fe7: 7.15E-13
Fe61:-2.34E-17 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 2.53E-08 Si6.5:-3.80E-18 C610: 8.80E-17 C370: 1.69E-09
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.23E-17 8-7 3.85E-16
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.24E-10 5 1.40E-20 6 1.65E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.07E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 8-7 8
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.23E-17 8-7 3.85E-16
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.24E-10 5 1.40E-20 6 1.65E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.07E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 8-7 8
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.23E-17 8-7 3.85E-16 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.23E-17 8-7 3.85E-16 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 1.0E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 6 5 2.89E-17 7 6 8.07E-17 8 - 7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.23E-17 8 - 7 3.85E-16 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.99E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 9.27E-20 6-5 1.59E-17 7-6 3.65E-19 8 - 7 1.55E-18 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 3.2E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 4.16E-18 New HE Is optical depths: 1 3.2E-03 2.79E-14 4-3 2.32E-27 5-4 2.43E-20 6-5 2.64E-20 7 6 1.00E-20 7 9.95E-21 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21 New HE Is optical depths: 1 2.97E-02 3-2 7.49E-14 4-3 2.32E-20 5-4 9.27E-20 6-5 1.00E-20 7 0.99E-21 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 5 4 2.43E-20 6-5 6-5 1.00E-20 7 0.76 8.79E-18 Old He II optical depths: 1 2.97E-02 3-2 2.10E-13 4-3 2.32E-20 5-4 4.20E-20 5 2.00E-20 6 1.00E-20 7 0.79E-218
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 7 4.07E-20 7 5.98E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 1.32E-03 2 5.43E-10 3 2.00E-20 4 2.04E-20 5 1.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 1.32E-03 2 5.749E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 1.09E-20 7 6 1.01E-20 7 4.16E-18 New HE Is optical depths: 1 1.27E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.39E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.77E+02
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21 New HE Is optical depths: 1 2.97E-02 3-2 7.49E-14 4-3 2.32E-20 5-4 9.27E-20 6-5 1.00E-20 7 0.99E-21 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 5 4 2.43E-20 6-5 6-5 1.00E-20 7 0.76 8.79E-18 Old He II optical depths: 1 2.97E-02 3-2 2.10E-13 4-3 2.32E-20 5-4 4.20E-20 5 2.00E-20 6 1.00E-20 7 0.79E-218
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 7 4.07E-20 8.7 9.70E-16 Old He Is optical depths: 2 1.405E+01 3 2.543E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.27E-01 3-2 7.49E-14 4-3 2.32E-27 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 7 6 1.31E-19 8-7 1.55E-18 New HE II optical depths: 1 2.77E+02
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.79E-03 2 2.79E-14 4 2.32E-20 5-4 2.00E-20 5 2.00E-20 7 4.16E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.97E-02 2 1.26E-02 3 1.00E-20
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 7 4.07E-20 8.7 9.70E-16 Old He Is optical depths: 2 1.405E+01 3 2.543E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.27E-01 3-2 7.49E-14 4-3 2.32E-27 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 7 6 1.31E-19 8-7 1.55E-18 New HE II optical depths: 1 2.77E+02
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 New HE Is optical depths: 1 2.79E-03 2 2.79E-14 4 2.32E-20 5-4 2.00E-20 5 2.00E-20 7 4.16E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 New HE II optical depths: 1 2.97E-02 2 1.26E-02 3 1.00E-20
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.79E-10 3 2.00E-20 4 2.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 2.00E-20 5 2.00E-20 6 1.00E-20 7 9.99E-21 Lines: 2-1 4.02E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 1.00E-20 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 4 2.43E-20 6-5 2.66E-20 7 6 1.03E-20 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 6.03E-13 4-3 1.28E-19
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.23E-17 8-7 3.85E-16 Old He Is optical depths: 1 2.66E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 7 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 3-2 6.03E-13 4-3 1.28E-19 5-4 8.46E-20 6-5-8.57E-20 7-6 1.41E-18 8-7 1.87E-17 New HE II optical depths: 1 1.22E-02 2 6.30E-03 3 1.00E-20 4 9.99E-21 5 9.99E-21 6 9.98E-21 7 9.76E-21 Lines: 2-1 1.62E+02 3-2 0.32E-33 3 1.00E-20 4 9.99E-21 5 9.99E-21 7.06 5.77E-19 8-7 7.55E-18 Hydrogen -2.821 -0.001 Log10 Mean Ionisation (over volume) Helium -3.598 -0.908 -0.057 Carbon -3.787 -1.278 -0.213 -0.565 -1.221 -2.551 -4.717 Nitrogen -4.535 -1.737 -0.371 -0.375 -1.056 -1.325 -3.475
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Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.63E-19 8-7 4.16E-18 New HE Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 7 7-6 3.65E-19 8-7 4.16E-18 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 2.64E-20 7-6 1.131E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 3-2 6.03E-13 4-3 1.28E-19 5-4 8.46E-20 6-5-8.57E-20 7-6 1.41E-18 8-7 1.87E-17 New HE II optical depths: 1 1.27E-02 2 6.03E-13 4-3 1.00E-20 5 9.99E-21 6 9.99E-21 7 9.76E-21 Lines: 2-1 1.62E+02 3-2 6.03E-13 4-3 4.99E-20 5-4 2.53E-20 6-5-5.17E-20 7-6 5.77E-19 8-7 7.55E-18 Hydrogen -2.821 -0.001 Helium -3.598 -0.908 -0.057 Carbon -3.787 -1.278 -0.371 -0.375 -1.056 -1.325 -3.475 Oxygen -4.535 -1.737 -0.371 -0.375 -1.056 -1.325 -3.475 Oxygen -4.535 -1.737 -0.371 -0.375 -1.056 -1.325 -3.475 Oxygen -4.506 -1.944 -0.762 -0.394 -0.450 -1.177 -2.989 -3.844 Magnesium -3.106 -1.095 -1.334 -0.739 -0.787 -0.507 -0.734 -1.535 -2.914 -4.538 Silicon -3.842 -1.783 -0.664 -0.996 -0.894 -0.562 -0.693 -1.250 -2.292 -3.776 Sulphur -4.657 -1.330 -0.584 -0.720 -0.104 -0.0940 -0.980 -1.463 -2.2281 -3.499 -6.631
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.65E-19 8-7 3.85E-16 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 3-2 6.03E-13 4-3 1.28E-19 5-4 8.46E-20 6-5-8.57E-20 7-6 1.41E-18 8-7 1.65TE-17 New HE II optical depths: 1 1.27E-02 2 6.03E-03 3 1.00E-20 4 9.99E-21 5 9.99E-21 6 9.99E-21 7 9.76E-21 Lines: 2-1 1.62E+02 3-2 2.33E-13 4-3 1.28E-19 5-4 2.53E-20 6-5-5.17E-20 7-6 5.77E-19 8-7 7.55E-18 Hydrogen -2.821 -0.001 Helium -3.598 -0.908 -0.057 Carbon -3.787 -1.278 -0.213 -0.565 -1.221 -2.551 -4.717 Nitrogen -4.535 -1.737 -0.337 -0.375 -0.565 -1.221 -2.551 -4.717 Nitrogen -4.505 -1.334 -0.737 -0.561 -1.535 -3.475 Oxygen -4.906 -1.941 -0.397 -0.376 -0.561 -1.556 -1.321 -2.551 -4.717 Nitrogen -4.535 -1.737 -0.334 -0.737 -0.561 -1.555 -2.214 -4.538 Silicon -3.482 -1.783 -0.664 -0.966 -0.596 -0.699 -0.693 -1.520 -2.292 -3.776 Sulphur -4.657 -1.334 -0.720 -0.767 -0.531 -0.914 -1.881 -3.217 -4.679 Aluminum -3.106 -1.095 -1.334 -0.737 -0.561 -0.571 -2.294 -3.776 Sulphur -4.657 -1.333 -0.669 -0.688 -0.787 -0.531 -0.914 -1.535 -2.914 -4.538 Silicon -3.484 -1.785 -0.669 -0.698 -0.680 -0.696 -0.698 -0.680 -2.099 -1.463 -
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.25E-17 8-7 3.85E-16 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 2.68E-03 2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.00E-20 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 3-2 6.03E-13 4-3 1.28E-19 5-4 8.46E-20 6-5-8.57E-20 7-6 1.41E-18 8-7 1.87E-17 New HE II optical depths: 1 1.27E-02 2 6.03E-03 3 1.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 1.62E+02 3-2 2.33E-13 4-3 1.28E-19 5-4 8.46E-20 6-5-8.57E-20 7-6 1.41E-18 8-7 1.87E-17 Net HE II optical depths: 1 1.07E-02 2 6.30E-03 3 1.00E-20 4 9.99E-21 5 9.99E-21 6 9.99E-21 7 9.76E-21 Lines: 2-1 1.62E+02 3-2 2.33E-13 4-3 4.99E-20 5-4 2.53E-20 6-5-5.17E-20 7-6 5.77E-19 8-7 7.55E-18 Hydrogen -2.821 -0.001 Log10 Mean Ionisation (over volume) Helium -3.598 -0.098 -0.057 Carbon -3.787 -1.278 -0.213 -0.565 -1.221 -2.551 -4.717 Nitrogen -4.535 -1.737 -0.371 -0.375 -0.567 -1.335 -3.375 Oxygen -4.906 -1.941 -0.387 -0.577 -0.537 -0.531 -0.914 -1.581 -3.217 -4.679 Aluminum -3.106 -1.095 -1.334 -0.739 -0.787 -0.507 -0.734 +1.555 -2.914 -4.538 Silicon -3.842 -1.783 -0.664 -0.996 -0.694 -0.562 -0.693 -1.220 -2.292 -3.776 Sulphur -4.657 -1.303 -0.540 -0.789 -0.568 -0.783 -0.661 -1.137 -1.37
Old hydro optical depths: 1 6.30E-03 2 4.08E-10 3 8.07E-10 4 2.28E-10 5 1.52E-20 6 2.12E-20 7 5.99E-20 Lines: 2-1 8.07E+01 3-2 8.43E-11 4-3 2.01E-17 5-4 1.63E-17 6-5 2.89E-17 7-6 8.07E-17 8-7 9.70E-16 New hydro optical depths: 1 6.30E-03 2 4.19E-10 3 8.29E-10 4 2.34E-10 5 1.40E-20 6 1.85E-20 7 4.77E-20 Lines: 2-1 4.05E+01 3-2 3.70E-11 4-3 8.99E-18 5-4 7.60E-18 6-5 1.39E-17 7-6 3.65E-19 8-7 3.85E-16 Old He Is optical depths: 1 2.68E-03 2 5.43E-10 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 2.00E-20 7 2.00E-20 Lines: 2-1 9.89E-01 3-2 2.10E-13 4-3 6.93E-20 5-4 9.27E-20 6-5 1.59E-19 7-6 3.65E-19 8-7 4.16E-18 New HE Is optical depths: 1 1.32E-03 2 2.79E-10 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 9.99E-21 Lines: 2-1 4.22E-01 3-2 7.49E-14 4-3 2.32E-20 5-4 2.43E-20 6-5 2.64E-20 7-6 1.31E-19 8-7 1.55E-18 Old He II optical depths: 1 2.97E-02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 2 1.26E-02 3 2.00E-20 4 2.00E-20 5 2.00E-20 6 1.99E-20 7 1.93E-20 Lines: 2-1 3.77E+02 3-2 6.03E-13 4-3 1.28E-19 5-4 8.46E-20 6-5-8.57E-20 7-6 1.41E-18 8-7 1.65TE-17 New HE II optical depths: 1 1.27E-02 2 6.03E-03 3 1.00E-20 4 9.99E-21 5 9.99E-21 6 9.99E-21 7 9.76E-21 Lines: 2-1 1.62E+02 3-2 2.33E-13 4-3 1.28E-19 5-4 2.53E-20 6-5-5.17E-20 7-6 5.77E-19 8-7 7.55E-18 Hydrogen -2.821 -0.001 Helium -3.598 -0.908 -0.057 Carbon -3.787 -1.278 -0.213 -0.565 -1.221 -2.551 -4.717 Nitrogen -4.535 -1.737 -0.337 -0.375 -0.565 -1.221 -2.551 -4.717 Nitrogen -4.505 -1.334 -0.737 -0.561 -1.535 -3.475 Oxygen -4.906 -1.941 -0.397 -0.376 -0.561 -1.556 -1.321 -2.551 -4.717 Nitrogen -4.535 -1.737 -0.334 -0.737 -0.561 -1.555 -2.214 -4.538 Silicon -3.482 -1.783 -0.664 -0.966 -0.596 -0.699 -0.693 -1.520 -2.292 -3.776 Sulphur -4.657 -1.334 -0.720 -0.767 -0.531 -0.914 -1.881 -3.217 -4.679 Aluminum -3.106 -1.095 -1.334 -0.737 -0.561 -0.571 -2.294 -3.776 Sulphur -4.657 -1.333 -0.669 -0.688 -0.787 -0.531 -0.914 -1.535 -2.914 -4.538 Silicon -3.484 -1.785 -0.669 -0.698 -0.680 -0.696 -0.698 -0.680 -2.099 -1.463 -

Normalised continuum												
0.25 1.000 0.62 1.001	0.27 1.000 0.67 1.000	0.30 1.000 0.74 1.000	0.33 1.000 0.81 1.000	0.36 1.000 0.88 1.000	0.39 1.000 0.97 1.000	0.43 1.000 0.98 1.000	0.47 1.000 0.99 1.000	0.51 1.000 1.00 1.000	0.56 1.001			

Inward continua (nuFnu) at head of Balmer, Lyman series; 6.19E-09 6.89E-08

LY ALPHA FOREST CLOUD

Outwrd continua (nuFnu) at head of Balmer, Lyman series; 6.19E-09 7.01E-08

			Emergent continuu	um - phot/ryd/cm2	(r in)	
0.26 1.54E+07	1.00 1.02E+06	3.9 6.77E+04	17.3 3.41E+03	75.3 1.81E+02	1.26E+03 6.44E-01	3.24E+05 9.76E-06
0.29 1.21E+07	1.01 1.00E+06	4.0 6.31E+04	19.5 2.68E+03	81.6 1.54E+02	1.88E+03 2.91E-01	4.82E+05 4.42E-06
0.33 9.51E+06	1.02 9.88E+05	4.2 5.82E+04	22.0 2.11E+03	88.3 1.31E+02	2.79E+03 1.32E-01	7.16E+05 2.00E-06
0.37 7.48E+06	1.10 8.46E+05	4.7 4.67E+04	24.8 1.67E+03	95.7 1.12E+02	4.14E+03 5.97E-02	1.06E+06 9.05E-07
0.42 5.89E+06	1.24 6.66E+05	5.3 3.69E+04	27.9 1.31E+03	103.7 9.53E+01	6.16E+03 2.70E-02	1.58E+06 4.09E-07
0.47 4.63E+06	1.40 5.30E+05	5.9 2.91E+04	31.5 1.03E+03	112.3 8.12E+01	9.15E+03 1.22E-02	2.35E+06 1.85E-07
0.53 3.65E+06	1.57 4.13E+05	6.7 2.29E+04	35.5 8.14E+02	121.6 6.92E+01	1.36E+04 5.54E-03	3.49E+06 8.39E-08
0.60 2.87E+06	1.78 3.24E+05	7.5 1.81E+04	40.0 6.41E+02	131.7 5.90E+01	2.02E+04 2.51E-03	5.19E+06 3.80E-08
0.67 2.26E+06	2.00 2.56E+05	8.5 1.43E+04	45.0 5.05E+02	142.7 5.03E+01	3.01E+04 1.13E-03	
0.76 1.77E+06	2.25 2.02E+05	9.5 1.12E+04	50.5 4.02E+02	173.9 3.39E+01	4.47E+04 5.14E-04	
0.86 1.40E+06	2.54 1.59E+05	10.8 8.85E+03	54.7 3.42E+02	258.5 1.53E+01	6.64E+04 2.32E-04	
0.97 1.10E+06	2.86 1.25E+05	12.1 6.97E+03	59.3 2.92E+02	384.2 6.94E+00	9.87E+04 1.05E-04	
0.99 1.05E+06	3.22 9.85E+04	13.7 5.49E+03	64.2 2.49E+02	571.0 3.14E+00	1.47E+05 4.76E-05	
0.99 1.04E+06	3.63 7.76E+04	15.4 4.33E+03	69.5 2.12E+02	848.8 1.42E+00	2.18E+05 2.16E-05	

e The second	*
title check that equilibrium works at very low densities	*
* hden = -1 , proportional to radius to the -2	*
* stop eden -5	*
filling factor -5	*
* radius 15	*
* blackbody, t=5	*
* luminosity 38	*
sphere	*
c ldl.in	*
c cray	*
e de la companya de l	*

Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

Lo 1.00E-05=0.9105cm	Hi-Con:2.30E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
Average nu:2.177E+00	P(X-ray): 27.7886	P(BalC): 37.0669	Q(Balmer C): 47.9086
Q(1.8-4.0): 48.0180	Q(4.0-20): 47.0910	Q(20): 37.1273	Ion pht flx:1.679E+17
Q(gam ray): 0.0000	L(Infred): 35.4829	Alf(ox): 0.0000	Total lumin: 38.0492
Abs bol mg: -6.4461	Abs V mag: -0.0356	Bol cor: -6.4105	nuFnu(Bbet): 35.5847
U(4.0):3.273E+06	T(En-Den):4.452E+02	T(Comp):9.574E+04	nuJnu(912A):2.215E+06
Occ(H n=6):8.670E-09	Occ(1Ryd):1.022E-10	Occ(4R):7.057E-13	Occ (Nu-hi):1.169E-25
Tbr(H n=6):3.850E-05	Tbr(1Ryd):1.614E-05	Tbr(4R):4.464E-07	Tbr (Nu-hi):4.175E-19
	Average nu:2.177E+00 Q(1.8-4.0): 48.0180 Q(gam ray): 0.0000 Abs bol mg: -6.4461 U(4.0):3.273E+06 Occ(H n=6):8.670E-09	Average nu:2.177E+00 P(X-ray): 27.7886 Q(1.8-4.0): 48.0180 Q(4.0-20): 47.0910 Q(gam ray): 0.0000 L(Infred): 35.4829 Abs bol mg: -6.4461 Abs v mag: -0.0356 U(4.0):3.273E+06 T(En-Den):4.452E+02 Occ(H n=6):8.670E-09 Occ(1Ryd):1.022E-10	$ \begin{array}{llllllllllllllllllllllllllllllllllll$

1 Te:9.567E+04 Hden:7.901E-02 Ne:9.523E-02 R:1.062E+15 R-R0:6.250E+13 dR:1.250E+14 NTR: 1 Htot:3.647E-23 T912: 9.991E+07###
-18.93 4686 1.99 5876 0.00 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.01
P(LINES): 0.971 0.000 0.000 0.000 0.000 0.000 0.029 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
Hydrogen 9.214E-15 1.000E+00 H+0/Hden: 1.000E+00 4.570E-32 H- H2 5.117E-41 1.271E-30 H2+ HeH+ 1.271E-43 H col den 9.877E+07
H 2SP 3-6 1.174E-16 2.956E-23 2.388E-23 3.063E-23 4.106E-23 5.313E-23 Texc(La); 5.731E+03 T(contn): 3.958E+02 T(diffs): 4.073E+02
Helium 4.106E-25 2.155E-12 1.000E+00 He I 2S3 3.136E-26 Comp H, C 3.647E-23 3.644E-23 Fill Fact 1.000E-05 Gam 1/tot 9.947E-01
He singlet 3.770E-25 2.248E-27 4.934E-34 8.533E-34 1.498E-33 2.517E-33 He triplt 3.136E-26 5.930E-34 2.086E-35 1.007E-34 1.206E-35
HeII 2.155E-12 9.118E-17 2.997E-23 3.495E-23 4.518E-23 5.863E-23 4.146E-22 2.140E-21 3.217E-19 PRAD/GAS; 4.301E+05
Pressure NgasTgas; 1.742E+04 P(total): 1.035E-06 P(gas): 2.405E-12 P(Radtn): 1.035E-06 Rad accel 1.011E-04 Force Mul 1.000E+00
Carbon 0.000E+00 0.000E+00 2.278E-19 1.152E-09 1.000E+00 0.000E+00 0.000E+00 H2O+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 0.000E+00 0.000E+00 0.000E+00 1.988E-17 3.781E-09 1.000E+00 0.000E+00 0.000E+00 02/Ototl: 0.000E+
Oxygen 0.000E+00 0.000E+00 0.000E+00 0.000E+00 7.782E-14 3.102E-07 1.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-13.492
Neon 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 2.113E-04 2.832E-02 9.715E-01 0.000E+00 0.000E+00
Magnesium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 1.011E-07 1.946E-03 2.856E-01 7.125E-01 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 1.270E-06 2.437E-02 8.150E-01 1.606E-01 0.000E+00 0.000E+00 0.000E+00
Silicon 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 9.722E-07 1.562E-02 9.145E-01 6.990E-02 0.000E+00 0.000E+00 0.000E+00
Sulphur 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 4.074E-10 1.785E-01 8.215E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Argon 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 3.321E-12 9.650E-07 1.000E+00 0.000E+00 0.000E+00 0.000E+00
Calcium 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 3.559E-05 1.207E-02 9.879E-01 0.000E+00
Iron 0 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 6.678E-06 1.396E-01 6.990E-01 1.603E-01 1.123E-03
#####177 Te:9.566E+04 Hden:7.799E-06 Ne:9.399E-06 R:1.105E+17 R-R0:1.095E+17 dR:5.400E+15 NTR: 1 Htot:2.808E-31 T912: 9.991E+07###
-17.92 4686 2.07 5876 0.00 1909 0.00 1549 0.00 6584 0.00 5007 0.00 3727 0.00 6300 0.00 2798 0.00 1035 0.01
P(LINES): 0.972 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
Hydrogen 1.083E-14 1.000E+00 H+0/Hden: 1.000E+00 4.109E-36 H- H2 7.885E-41 1.637E-30 H2+ HeH+ 2.242E-43 H col den 9.469E+08
H 2SP 3-6 1.212E-20 2.956E-27 2.356E-27 3.041E-27 4.081E-27 5.283E-27 Texc(La); 3.940E+03 T(contn): 4.053E+01 T(diffs): 4.035E+02
Helium 1.097E-26 2.696E-12 1.000E+00 He I 2S3 8.616E-27 Comp H, C 2.807E-31 2.805E-31 Fill Fact 1.000E-05 Gam 1/tot 1.000E+00
He singlet 2.358E-27 1.898E-31 2.381E-38 5.679E-38 1.158E-37 2.126E-37 He triplt 8.616E-27 7.321E-38 2.575E-39 1.243E-38 1.489E-39
HeII 2.696E-12 9.489E-21 3.150E-27 3.647E-27 4.686E-27 6.052E-27 4.254E-26 2.112E-25 3.176E-23 PRAD/GAS; 4.666E+05
Pressure NgasTgas; 1.719E+00 P(total): 1.108E-10 P(gas): 2.374E-16 P(Radtn): 1.108E-10 Rad accel 7.884E-09 Force Mul 1.000E+00

Carbon		0.000E+00	0.000E+00	4.821E-19	1.458E-09	1.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen		0.000E+00	0.000E+00	0.000E+00	4.231E-17	4.782E-09	1.000E+00	0.000E+00	0.000E+00	02/Ototl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen		0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.642E-13	3.925E-07	1.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-13.492
Neon		0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.301E-04	3.556E-02	9.640E-01	0.000E+00	0.000E+00	
Magnesium	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.040E-07	3.640E-03	3.353E-01	6.610E-01	0.000E+00	0.000E+00	0.000E+00
Aluminium	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.321E-06	4.006E-02	8.512E-01	1.088E-01	0.000E+00	0.000E+00	0.000E+00
Silicon	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.227E-06	2.442E-02	9.272E-01	4.838E-02	0.000E+00	0.000E+00	0.000E+00
Sulphur	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.226E-10	2.156E-01	7.844E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Argon	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.003E-12	1.221E-06	1.000E+00	0.000E+00	0.000E+00	0.000E+00
Calcium	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.525E-05	1.928E-02	9.806E-01	0.000E+00
Iron	0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.847E-05	2.285E-01	6.782E-01	9.286E-02	3.873E-04
Calculat	tic	on stopped	because lo	owest EDEN	reached.								
Geometry	7	is spherica	al.										
Photoio	ni:	ation of 1	He 2Tris re	eached 100.	.0 percent	of the to	tal rate ou	ut.					

Photoionization of He 2TriS reached 100.0 percent of the total rate out. Compton heating was100.0% of the total. Frequency out of range of free-free gaunt factor routine. The ratio of radiation to gas pressure reached 4.35E+06. Caused by Lyman alpha. C-The HeII continuum is thin and I assumed that it was thick. Try another iteration. C-The HeI continuum is thin and I assumed that it was thick. Try another iteration.

**************************************	* * * * *
* title check that equilibrium works at very low densities	*
* hden = -1 , proportional to radius to the -2	*
* stop eden -5	*
* filling factor -5	*
* radius 15	*
* blackbody, t=5	*
* luminosity 38	*
* sphere	*
* c ldl.in	*
* c cray	*
**************************************	****
>>>>>> Cautions are present.	
>>>>>>> Another iteration is suggested.	

Emission Line Spectrum. Power Law Density Model. Closed geometry. Iteration 1 of 1. Luminosity (erg/s) emitted by shell with full coverage.

TOTL 4861 13.17	9 1.0000	TOTL 1216	14.783	40.1138	TOTL	1640	14.577	25.0031	Si 9	1815	11.404	0.0168
TOTL 1216 14.78	3 40.1138	TOTL 973	13.787	4.0521	TOTL	4686	13.495	2.0697	Si 9	3	13.136	0.9041
TotH 0 18.73	2****	TOTL 950	13.538	2.2812	TOTL	1216	14.053	7.4717	Si 9	2	12.782	0.4007
BFH1 0 14.54	0 22.9457	TOTL 938	13.358	1.5085	Ca B	1640	14.303	13.2771	Si 9	691	13.056	0.7518
BFHx 0 11.63	9 0.0288	INWD 1216	14.783	40.1138	DevB	1640	14.300	13.2104	Fe 9	171	13.504	2.1097
BFHe 0 14.60	1 26.3754	Dest 1216	10.364	0.0015	Ca B	4686	13.257	1.1950	Fe 9	245	11.939	0.0574
TotM 0 14.68	5 32.0293	e sc 1216	13.411	1.7029	DevB	4686	13.250	1.1764	Fe 9	242	10.678	0.0032
ComH 0 18.73	2*****	e sc 6563	13,237	1.1413	C4 r	1549	13.015	0.6843	Fe10	352	14.864	48.3380
CA B 4861 13.23		e sc 4861		0.8120			11.111	0.0085	Fe10			*******
CA B 1216 14.86		e sc18751		0.2771			11.153	0.0094				13.6946
DU B 4861 13.23		e sc40512		0.0517	Ne 7		12.221	0.1101				*******
												0.8101
Q(H) 4861 36.00		nFnu 4860		27.1389	Ne 8		15.012	67.9799			13.088	
Q(H) 1216 37.53	5*******	nFnu 1215	14.900	52.5638	Mg 7	2629	12.424	0.1757	Fell	7892	21.323*	******
TOTL 6563 13.65	8 3.0118	Inci 4861	35.585*	*******	Mg 7	433	12.351	0.1483	Coll	7892	13.538	2.2809
TOTL 4861 13.17	9 1.0000	Inci 1216	37.175*	*******	Mg 8	435	13.903	5.2899	Pump	7892	21.323*	*******
TOTL 4340 12.83	4 0.4517	BAC 0	14.107	8.4649	Mg 8	3	13.593	2.5929	Fe11	6	12.104	0.0841
TOTL 4102 12.55	6 0.2380	PAC 0	13.489	2.0384	Mg 9	705	14.810	42.7330	Fell	2649	13.355	1.4973
TOTL18751 12.62	2 0.2769	H FF 0	14.914	54.2111	Mq 9	368	14.508	21.3030	Fell	1467	12.435	0.1802
TOTL12818 12.30	4 0.1331	ComC 0	18.732*	*******	Si 7	2148	12.754	0.3753	Fe11	354	14.430	17.8147
TOTL10938 12.03	3 0.0714	HFB 0	14.442	18.3243	Si 7	25	12.202	0.1054	Fe12	1242	11.756	0.0378
TOTL40512 11.89	2 0.0516	HeFF 0	14.507	21,2508	Si 7	65	11.001	0.0066	Fe12	2170	12.080	0.0796
TOTL26252 11.64			14.384	16.0128			14.790	40.7597			11.255	0.0119
TOTL74578 11.31			13.669	3.0876	Si 9		13.351	1.4849	Fe12	357	12.333	0.1425
2 NU 0 14.36	8 15.4465	Toff 0	15.075	78.5495	Si 9	949	12.410	0.1701				

CHECK THAT EQUILIBRIUM WORKS AT VERY LOW DENSITIES
Heating: ComH 0:1.000 IONIZE PARMET: U(1-) 7.7481 U(4-): 6.5150 U(sp): 7.77 Q(ion): 48.248 L(ion): 37.924 Q(low): 47.88 P(low) 37.00
ENERGY BUDGET: Heat: 18.732 Coolg: 18.732 Error: 0.0% Compt H: 18.732 WorkF: 16.227 F-F H 8.285 PRADMX:4.35E+06 Column density H12:9.469E+08 H II:9.469E+08 HI:1.002E-05 H-: 1.563E-23 H2: 6.950E-32 H2+:1.476E-21 He H+:2.008E-34 OH: 0.000E+00 Heff:0.000E+00
<pre><nh>:8.437E-04 <tp>:9.57E+04 <to3>:0.00E+00 Ne:0.000E+00 ti(snd):3.12E+05 NeN+d1:3.48E+07 <t(c3)>:9.57E+04 <e(c3)>:3.30E-02 He/Ha:1.61E-01 = 1.65*true N/Oap:0.00E+00 = 0.00true T(O3R):0.000E+00 L THIN:1.00E+30 <t(s2)>:0.00E+00 <e(s2)>:0.00E+00</e(s2)></t(s2)></e(c3)></t(c3)></to3></tp></nh></pre>
T He+:9.57E+04 EH+:3.55E-02 T(O+):0.00E+00 EO+:0.00E+00 iter/zn: 2.045 Te-low:9.56E+04 Te-high:9.57E+04 Hlu/zn:2.04E+00 <a>:0.00E+00 erdeFe0.0E+00 Tcompt5.22E+07 Tthr9.88E+10 <tden>: 9.57E+04 <dens>:1.99E-27 <mol>:6.16E-01 Mean Jeans l(cm)5.75E+24 M(sun)9.21E+11 smallest: len(cm):5.72E+22 M(sun)9.15E+09 Alf(ox-tran): 0.0000</mol></dens></tden>
Optical Depths: CONTN; COMP: 3.79E-16 H-: 5.00E-21 R(1300): 6.73E-29 H2+ 1.03E-38 HeTri:3.79E-16
Pfa:3.79E-16 Pa:3.79E-16 Ba:3.79E-16 Hb:3.79E-16 La:3.79E-16 lr:4.995E+07 1.8:1.15E+07 4.:1.715E+06 21R:3.176E+04 10830: 1.00E-20 3889: 1.00E-20 5876: 1.00E-20 7065: 1.00E-20 1355: 1.02E-17 1035: 6.20E-15 1335: 1.00E-20 977: 1.00E-20 1397: 1.00E-20
789: 1.00E-20 1207: 1.00E-20 1085: 1.00E-20 1194: 1.00E-20 1999: 1.00E-20 1895: 1.00E-20 2326: 1.00E-20 1666: 1.00E-20 1750: 1.00E-20 1025: 1.00E-20 352: 1.07E-10 347: 1.00E-20 1860: 1.00E-20 630: 1.51E-20 834: 1.00E-20 835: 1.00E-20 1808: 1.00E-20 1256: 1.00E-20 -3: 1.00E-20 -48: 1.00E-20 384: 1.00E-20 8498: 1.00E-20 842: 1.00E-20
8662: 1.00E-20 353: 1.73E-11 1304: 1.00E-20 1122: 1.00E-20 990: 1.00E-20 1402: 1.00E-20 1214: 1.00E-20 1486: 1.00E-20 2335: 1.00E-20 1406: 1.00E-20 1656: 1.00E-20 9830: 1.00E-20 8727: 1.00E-20 6300: 1.00E-20 5577: 1.00E-20 7291: 1.00E-20
7324: 1.00E-20 1039: 1.00E-20 -4368: 1.00E-20 -132: 1.00E-20 -113: 1.00E-20 -29: 1.00E-20 -46: 1.00E-20 -245: 1.41E-13 765: 1.00E-20 1198: 1.00E-20 786: 1.00E-20 0146: 1.00E-20 063: 1.00E-20 088: 1.00E-20 052: 1.00E-20 C157: 1.00E-20 N122: 1.00E-20 N57: 1.00E-20 0146: 1.00E-20 063: 1.00E-20 052: 1.00E-20
026: 1.00E-20 NE13: 1.00E-20 NE36: 1.00E-20 NE16: 1.00E-20 MG4: 1.00E-20 MG4: 1.00E-20 MG6: 1.00E-20 SI35: 1.00E-20 S19: 1.00E-20 S34: 1.00E-20 S11: 1.00E-20 AR7: 1.00E-20 AR9: 1.00E-20 AR22: 1.00E-20 AR13: 1.00E-20 R8: 1.00E-20 CA3: 1.00E-20 CA4: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 CA4: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 CA4: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 CA4: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 NE14: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 S33: 1.00E-20 NE14: 1.00E-20 NE14
Fe61: 9.42E-21 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 5.45E-17 Si6.5: 1.00E-20 C610: 1.00E-20 C370: 1.00E-20 Old hydro optical depths: 1 9.99E+07 2 1.00E-20 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 1.00E-20
Lines: 2-1 9.96E+09 3-2 1.30E+03 4-3 1.30E+01 5-4 6.48E-01 6-5 9.97E-02 7-6 9.97E-03 8-7 9.97E-04 New hydro optical depths: 1 5.00E+07 2 5.00E-21 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7-5 5.00E-21 Lines: 2-1 5.00E-01 3-2 8.47E-21 4-3 5.00E-21 5-4 5.00E-21 6-5 5.00E-21 7-6 5.00E-21 8-7 5.00E-21
Old He Is optical depths: 1 4.15E+05 2 0.00E+00 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7 5.00E-21 Lines: 2-1 9.96E+09 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 0.00E+00
New HE Is optical depths: 1 6.39E-24 2 5.00E-21 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7 5.00E-21 Lines: 2-1 1.00E+00 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 1.00E-20
Old He II optical depths: 1 4.15E+05 2 4.15E+05 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7 5.00E-21 Lines: 2-1 9.96E+09 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 0.00E+00
New HE II optical depths: 1 1.93E-22 2 5.03E-21 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7 5.00E-21 Lines: 2-1 1.00E+00 3-2 1.03E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 1.00E-20
Hydrogen -13.970 0.000 Log10 Mean Ionisation (over volume) Helium -25.099-11.569 0.000 Carbon -30.000-30.000-18.344 -8.836 0.000
Nitrogen -30.000-30.000-30.000-16.396 -8.320 0.000 Oxygen -30.000-30.000-30.000-12.807 -6.406 0.000 Neon -30.000-30.000-30.000-30.000-3.0000-3.386 -1.449 -0.016
Magnesium-30.000-30.000-30.000-30.000 -6.554 -2.458 -0.475 -0.180 Aluminum -30.000-30.000-30.000-30.000 -5.516 -1.416 -0.071 -0.948
Silicon -30.000-30.000-30.000-30.000-30.000 -5.681 -1.629 -0.033 -1.303 Sulphur -30.000-30.000-30.000-30.000-30.000 -9.206 -0.666 -0.105 Argon -30.000-30.000-30.000-30.000-30.000-11.177 -5.913 0.000
Calcium -30.000-30.000-30.000-30.000-30.000-30.000-30.000-30.000 -4.062 -1.734 -0.008 Iron -30.000-30.000-30.000-30.000-30.000-30.000-30.000 -4.776 -0.661 -0.166 -1.006 -3.360

	1	2 3		4 5	6	7	8	9	10	11	12	13	14	15	16 1	7
Hydroge	∋n - 13.975	0.000				Log10 Me	an Ioni	sation	(over r	adius	`					
Helium		-11.578 0				9			(,					
Carbon		-30.000-18		3.846 0.0	0.0											
		-30.000-30				0										
Oxygen		-30.000-30				6 0.000)									
Neon		-30.000-30	.000-30	0.000-30.0	00-30.00	0 -3.467	7 -1.458	-0.016	5							
Magnes	ium-30.000	-30.000-30	.000-30	0.000-30.0	00 -6.69	7 -2.532	2 -0.481	-0.176	5							
Aluminu	am -30.000	-30.000-30	.000-30	0.000-30.0	00 -5.65	3 -1.488	3 -0.077	-0.889	•							
Silicor	n -30.000	-30.000-30	.000-30	0.000-30.0	00 -5.78	8 -1.691	L -0.034	-1.254								
Sulphu	r _30.000	-30.000-30	.000-30	0.000-30.0	00 -9.22	2 -0.674	4 -0.103									
Argon	-30.000	-30.000-30	.000-30	0.000-30.0	00-30.00	0-11.268	3 -5.923	0.000)							
Calciur	n -30.000	-30.000-30	.000-30	0.000-30.0	00-30.00	0-30.000	0-30.000	-4.212	-1.805	-0.0	07					
Iron	-30.000	-30.000-30	.000-30	0.000-30.0	00-30.00	0-30.000	-4.934	-0.738	8 -0.158	-0.9	12 -3.17	75				
						Nor	malised	contir								
0 25	0.839 0	.27 0.839	0 30	0.839 0	.33 0.83		5 0.839		0.839	0 43	0.839	0 47	0.839	0.51 0.83	0 56	0.839
		.67 0.839			.81 0.83		3 0.839		0.839		0.839		0.839	1.00 0.83		0.039
0.02	0.035 0	.07 0.055	0.74	0.035 0	.01 0.05		0.035	0.57	0.000	0.90	0.055	0.55	0.055	1.00 0.03		
					E	mergent	continu	um - ph	ot/ryd/	'cm2 (r in)					
0.26	4.94E+16	0.60 8.49	E+16	1.0 9.6	9E+16	1.8 7.	58E+16	3.9) 1.22E+	-16	7.51E+0	00 1.48	E+14	1.73E+01	1.49E+08	
0.29	5.42E+16	0.67 8.92	E+16	1.0 9.6	9E+16	2.0 6.	63E+16	4.0) 1.04E+	-16	8.46E+0	00 4.19	E+13	1.95E+01	5.94E+06	
0.33	5.92E+16	0.76 9.28	BE+16	1.0 9.6	9E+16	2.3 5.	.56E+16	4.2	8.87E+	-15	9.53E+0	0 9.78	E+12	2.20E+01	1.53E+05	
0.37	6.43E+16	0.86 9.54	E+16	1.1 9.6	5E+16	2.5 4.	45E+16	4.7	5.16E+	-15	1.07E+0	01 1.84	E+12			
0.42	6.96E+16	0.97 9.68	BE+16	1.2 9.4	3E+16	2.9 3.	37E+16	5.3	2.58E+	-15	1.21E+0	01 2.72	E+11			
0.47	7.49E+16	0.99 9.69	E+16	1.4 9.0	1E+16	3.2 2.	40E+16	5.9	1.14E+	-15	1.36E+0	01 3.07	E+10			
0.53	8.00E+16	0.99 9.69	E+16	1.6 8.4	0E+16	3.6 1.	.59E+16	6.7	4.44E+	-14	1.54E+0	01 2.54	E+09			

**************************************	********
*	
* title liner model	
* c a constant pressure (gas+radiation) model of a liner cloud	
* c in the spirit of Ferland and Netzer 1983	
* table agn	
* metals 0.3	
* constant pressure	
* iterate ; must iterate to get radiation pressure correctly	
* hden 6	
* stop column density 23	
* ionization parameter -3	
* print last	
* c liner.in	
* c cray	
*	
*****	*******

Chemical composition He:.098 C:1.09E-04 N:3.36E-05 O:2.55E-04 Ne:3.69E-05 Mg:1.14E-05 Al:8.9E-07 Si:1.07E-05 S:4.86E-06 A:1.1E-06 Ca:6.9E-07 Fe:1.40E-05

546Cell Peak1.78E+00	Lo 1.00E-05=0.9101cm	Hi-Con:7.34E+06 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 3.2980	Average nu:3.038E+00	P(X-ray): 2.4693	P(BalC): 2.8023	Q(Balmer C): 13.7651
Q(1.0-1.8): 13.1738	Q(1.8-4.0): 13.0661	Q(4.0-20): 12.5287	Q(20): 10.7913	Ion pht flx:3.001E+13
L(gam ray): 2.2078	Q(gam ray): 8.6227	L(Infred): 3.0163	Alf(ox): -1.4120	Total lumin: 3.5633
U(1.0):1.001E-03	U(4.0):1.147E-04	T(En-Den):6.338E+01	T(Comp):1.327E+07	nuJnu(912A):6.342E+02
Occ(FarIR):5.638E-05	Occ(H n=6):2.126E-08	Occ(1Ryd):2.924E-14	Occ(4R):1.499E-16	Occ (Nu-hi):2.089E-44
Tbr(FarIR):9.380E-05	Tbr(H n=6):9.439E-05	Tbr(1Ryd):4.619E-09	Tbr(4R):9.484E-11	Tbr (Nu-hi):2.306E-32

1 Te:1.473E+04 Hden:1.000E+06 Ne:1.154E+06 R:1.000E+25 R-R0:8.769E+11 dR:1.754E+12 NTR: 3 Htot:4.613E-12 T912: 5.557E-02###
-0.46 4686 0.24 5876 0.04 1909 1.95 1549 0.50 6584 0.02 5007 3.48 3727 0.01 6300 0.00 2798 0.93 1035 0.00
Hydrogen 5.034E-03 9.950E-01 H+0/Hden: 1.000E+00 1.601E-10 H- H2 1.911E-11 6.657E-11 H2+ HeH+ 1.394E-10 H col den 1.754E+18
H 2SP 3-6 2.937E-10 4.733E-12 6.178E-15 5.944E-15 7.505E-15 9.719E-15 Texc(La); 5.405E+03 T(contn): 6.315E+01 T(diffs): 2.609E+02
Helium 2.510E-03 3.811E-01 6.164E-01 He I 2S3 1.439E-06 Comp H, C 2.387E-17 2.650E-20 Fill Fact 1.000E+00 Gam 1/tot 8.651E-01
He singlet 2.509E-03 1.107E-10 1.979E-16 2.598E-16 3.884E-16 5.551E-16 He triplt 1.439E-06 1.335E-13 5.363E-16 2.231E-15 3.266E-16
HeII 3.811E-01 4.136E-10 5.417E-16 8.101E-16 1.269E-15 1.912E-15 1.635E-14 1.721E-13 4.348E-11 PRAD/GAS; 1.392E-03
Pressure NgasTgas; 3.262E+10 P(total): 4.510E-06 P(gas): 4.504E-06 P(Radtn): 6.268E-09 Rad accel 2.967E-04 Force Mul 7.366E+03
Carbon 5.021E-04 1.348E-01 7.545E-01 1.078E-01 2.325E-03 0.000E+00 0.000E+00 H20+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 3.334E-04 1.136E-01 7.478E-01 1.353E-01 2.884E-03 9.031E-05 0.000E+00 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 4.783E-04 1.039E-01 8.033E-01 8.975E-02 2.536E-03 3.496E-05 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.601
Neon 7.740E-05 2.300E-02 8.259E-01 1.469E-01 4.140E-03 2.654E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 9.819E-04 1.066E-01 8.076E-01 8.304E-02 1.762E-03 6.852E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 1.532E-03 5.038E-01 3.487E-01 1.406E-01 5.116E-03 1.785E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Silicon 0 7.663E-05 1.128E-01 6.966E-01 1.753E-01 1.469E-02 5.160E-04 4.587E-06 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Sulphur 0 8.726E-06 1.202E-01 8.010E-01 7.541E-02 2.564E-03 7.892E-04 2.080E-05 8.329E-08 2.757E-10 0.000E+00 0.000E+00 0.000E+00
Argon 0 2.109E-04 1.086E-01 7.626E-01 1.226E-01 5.327E-03 7.016E-04 2.665E-05 1.155E-06 3.717E-08 7.257E-11 1.424E-13 0.000E+00
Calcium 0 9.275E-04 2.508E-02 7.380E-01 2.235E-01 1.078E-02 1.666E-03 6.119E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Iron 0 8.552E-06 3.686E-03 1.690E-01 4.526E-01 2.623E-01 1.058E-01 6.552E-03 1.226E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00
#####170 Te:3.978E+03 Hden:7.430E+06 Ne:4.552E+04 R:1.000E+25 R-R0:3.958E+14 dR:7.521E+12 NTR: 2 Htot:1.639E-14 T912: 9.752E+03###
1.15 4686 0.12 5876 0.16 1909 2.51 1549 0.31 6584 0.13 5007 4.52 3727 0.04 6300 0.34 2798 3.46 1035 0.00
Hydrogen 9.946E-01 5.435E-03 H+0/Hden: 9.997E-01 5.210E-09 H- H2 1.451E-04 5.566E-08 H2+ HeH+ 8.030E-09 H col den 1.698E+21
H 2SP 3-6 4.275E-10 7.585E-10 2.926E-16 3.947E-16 6.127E-16 9.225E-16 Texc(La); 4.332E+03 T(contn): 5.518E+01 T(diffs): 1.796E+02
Helium 9.946E-01 5.435E-03 4.141E-06 He I 2S3 1.145E-07 Comp H, C 9.657E-19 1.611E-22 Fill Fact 1.000E+00 Gam 1/tot 1.085E-01
He singlet 9.946E-01 1.953E-12 3.586E-19 4.789E-19 7.447E-19 1.114E-18 He triplt 1.145E-07 1.813E-15 2.510E-19 3.674E-18 4.973E-19
HeII 5.435E-03 9.339E-16 2.750E-22 4.393E-22 7.256E-22 1.150E-21 1.094E-20 1.433E-19 4.516E-17 PRAD/GAS; 1.030E-04
Pressure NgasTgas; 3.297E+10 P(total): 4.552E-06 P(gas): 4.552E-06 P(Radtn): 4.744E-10 Rad accel 1.640E-07 Force Mul 1.330E+03

Carbon	8.020E-04 9.989E-0	2.845E-04 0.000E+00	0.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen	9.918E-01 8.225E-03	5.574E-07 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/Ototl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9.953E-01 4.655E-03	3 7.190E-07 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.268
Neon	8.467E-01 1.427E-01	1.062E-02 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Magnesium (0 2.753E-03 9.939E-0	3.355E-03 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Aluminium (0 3.941E-04 9.876E-03	9.062E-03 2.872E-03	2.463E-05	0.000E+00						
Silicon (0 4.660E-04 9.995E-0	9.809E-07 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Sulphur (0 1.673E-04 9.890E-0	1.081E-02 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Argon (0 8.342E-01 1.649E-01	8.430E-04 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Calcium (0 1.913E-03 2.126E-0	7.855E-01 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Iron (0 7.991E-03 9.920E-03	7.791E-06 0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Calculati	ion stopped because 1	owest Te reached.								
Geometry	is plane-parallel.									

Geometry is plane-parallel. FeII-MgII photoionization of H N=2 reached 6.9 percent of the total rate out. Photoionization of He 2TriS reached 14.3 percent of the total rate out. Frequency out of range of free-free gaunt factor routine. The optical depth to Rayleigh scattering at 1300A is 1.04E-02

Emission Line Spectrum. Constant Pressure Model. Open geometry. Iteration 2 of 2.

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	In	tensity (e	erg/s/cm^2)			
TOTL 4861 1.145 1.0000	He2p 910 -1.649	0.0016	N 3 990 -1.268	0.0039	Si 2 2335 0.428	0.1918
TOTL 1216 2.880 54.3167	He I 504 1.011	0.7340	N 4 1486 -0.645	0.0162	Si 2 1808 -0.499	0.0227
Toth 0 2.854 51.1067	He I 4471 -0.232	0.0419	N 4 765 -2.707	0.0001	Si 3 1207 0.105	0.0911
BFH1 0 2.702 35.9808	TOTL 5876 0.341	0.1570	N 5 1240 -2.278	0.0004	Si 3 1895 1.067	0.8343
BFHe 0 2.301 14.2984	Ca B 5876 0.205	0.1148	0 1 6300 0.674	0.3380	PHOT 1895 -1.568	0.0019
TotM 0 1.050 0.8031	TOTL10830 1.494	2.2338	0 1 6363 0.197	0.1127	Si 4 1397 0.122	0.0947
ComH 0 -2.459 0.0002	INWD10830 1.411	1.8446	O 1 5577 -0.969	0.0077	S 2 6720 -0.327	0.0337
н- н 0 -0.617 0.0173	TOTL 3889 0.105	0.0911	0 1 630 -0.445	0.0257	S 2 4074 0.575	0.2686
CA B 4861 1.131 0.9683	TOTL 7065 0.118	0.0939	O 1 1470 -2.006	0.0007	S 210330 0.391	0.1758
CA B 1216 2.675 33.8848	CcHE 0 1.480	2.1590	0 1 7774 -2.329	0.0003	S II 6731 -0.485	0.0234
DU B 4861 1.131 0.9682	He I 2 -0.410	0.0278	T OI 0 -1.302	0.0036	S II 6716 -0.842	0.0103
Q(H) 4861 1.154 1.0198	DevB 2 -1.199	0.0045	6lev 1304 -1.306	0.0035	S II 4070 0.469	0.2108
Q(H) 1216 2.688 34.8654	He I 5016 -0.456	0.0250	TOTL 3727 -0.239	0.0412	S II 4078 -0.093	0.0578
TOTL 6563 1.624 3.0122	DevB 5016 -0.814	0.0110	TOTL 7325 0.952	0.6407	S II10323 -0.034	0.0662
TOTL 4861 1.145 1.0000	He I 3965 -0.745	0.0129	IONZ 7325 -1.617	0.0017	S II10289 -0.163	0.0492
TOTL 4340 0.845 0.5009	DevB 3965 -1.317	0.0034	O II 3729 -0.881	0.0094	S II10373 -0.563	0.0196
TOTL 4102 0.613 0.2935	He I 3614 -1.029	0.0067	O II 3726 -0.353	0.0317	S II10339 -0.243	0.0409
TOTL18751 0.596 0.2825	DevB 3614 -1.452	0.0025	O II 2471 0.853	0.5097	S II 1256 -2.068 S 3 18 -1.126	0.0006
TOTL12818 0.317 0.1485	He I 3448 -1.248	0.0040	O II 7323 0.696	0.3551		0.0054
TOTL10938 0.091 0.0883 TOTL40512 -0.094 0.0576	DevB 3448 -1.857 HeII 228 1.303	1.4377	O II 7332 0.601 O II 834 -1.373	0.2856	S 3 34 -2.193 S 3 9532 0.757	0.0005
		0.7996	0 11 834 - 1.373 0 2 4651 - 1.780	0.0030	S 3 9532 0.757 S 3 9069 0.342	
TOTL26252 -0.293 0.0365 TOTL74578 -0.623 0.0171	ESC 304 1.048 He2C 911 0.493	0.2226	0 2 4651 -1.780	0.0012	S 3 9069 0.342 S 3 6312 0.066	0.1571 0.0832
2 NU 0 0.833 0.4873	TOTL 1640 1.204	1.1444	Phot 1663 -2.479	0.4339	s 3 3722 -0.164	0.0832
TOTL 1216 2.880 54.3167	TOTL 1640 1.204 TOTL 4686 0.232	0.1221	Augr 1663 -2.323	0.0002	S 3 1198 -1.293	0.0491
TOTL 1216 2.880 54.5167 TOTL 1026 -1.590 0.0018	TOTL 1216 0.790	0.4407	Rec 1663 -1.638	0.0003	S 3 1729 -0.608	0.0177
TOTL 973 -1.653 0.0016	Ca B 1640 1.236	1.2323	0 3 5007 1.801	4.5245	s 4 105 -1.500	0.0023
TOTL 950 -1.622 0.0017	DevB 1640 1.233	1.2239	0 3 4959 1.324	1.5082	s 4 1406 -1.381	0.0030
TOTL 938 -1.577 0.0019	Ca B 4686 0.377	0.1706	LOST 5007 -2.453	0.0003	Ar 2 7 -0.758	0.0125
LA X 1216 0.949 0.6355	DevB 4686 0.370	0.1676	TOTL 4363 0.740	0.3934	Ar 3 7135 0.308	0.1453
C13c 6563 0.527 0.2406	Mion 0 -2.634	0.0002	Rec 4363 -2.702	0.0001	Ar 3 7751 -0.322	0.0341
C14c 4861 -0.533 0.0210	C 1 1656 -1.532	0.0021	0 3 2321 0.113	0.0928	Ar 3 22 -2.321	0.0003
CION 0 0.771 0.4225	REC 1656 -1.334	0.0033	C EX 4363 -2.483	0.0002	Ar 3 9 -0.705	0.0141
INWD 1216 2.879 54.0894	C I 9850 -2.017	0.0007	C EX 5592 -2.394	0.0003	Ar 4 4740 -1.159	0.0050
INWD 6563 1.355 1.6210	C 1 8727 -1.290	0.0037	O 3 880 -2.396	0.0003	Ar 4 7335 -1.404	0.0028
INWD 4861 0.851 0.5082	C 2 158 -2.473	0.0002	0 3 520 -1.382	0.0030	Ar 5 7007 -2.372	0.0003
INWD18751 0.295 0.1412	C 2 2326 1.086	0.8723	O 3 834 -0.866	0.0097	Ar 5 6435 -2.739	0.0001
Dest 1216 0.309 0.1458	INWD 2326 0.791	0.4422	0 4 26 -1.764	0.0012	Ca 2 3933 -0.637	0.0165
Dest 6563 -2.018 0.0007	C 2 1335 0.092	0.0884	O 4 1402 -0.798	0.0114	Ca 2 8579 -0.963	0.0078
Dest 4861 -2.741 0.0001	REC 1335 -0.264	0.0390	CONT 1401 -0.889	0.0092	Ca 2 7306 0.275	0.1349

LINER MODEL
Cooling: H FB 0:0.052 Cool 1216:0.337 O 3 5007:0.088 Emis 2798:0.067 Cool 2798:0.067
Heating: BFH1 0:0.704 BFHe 0:0.280
IONIZE PARMET: U(1-) -2.9996 U(4-): -3.9403 U(sp): -3.87 Q(ion): 10.540 L(ion): 2.639 Q(low): 15.31 P(low) 3.22
ENERGY BUDGET: Heat: 2.854 Coolg: 2.856 Error: 0.6% Compt H: -2.459 WorkF: 3.106 F-F H -3.856 PRADMX:8.19E-02
Column density H12:1.698E+21 H II:1.488E+20 HI:1.549E+21 H-: 1.558E+13 H2: 6.477E+16 H2+:5.133E+13 He H+:2.594E+13
OH: 0.000E+00 Heff:7.947E+20 <pre><nh>:4.250E+06 <pre><nh>:4.250E+06 <pre><nh>:4.250E+06 <pre><nh< pre="">:4.250E+06 <pre></pre>:4.250E+06 <pre></pre>:4.250</nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh<></pre></nh></pre></nh></pre></nh></pre>
<pre><nb:4.250e+06 <tp="">:1.25E+04 <tc03:1.42e+04 <t(c3)="" ne1.094e+06="" nen+d1:1.42e+26="" ti(snd):5.60e+08="">:1.38E+04 <e(c3)>:1.09E+06 He/Ha:1.26E-01 = 1.28*true N/0ap:3.73E+00 = 28.36true T(O3R):4.370E+04 L THIN:1.00E+30 <t(s2)>:5.23E+03 <e(s2)>:1.10E+05</e(s2)></t(s2)></e(c3)></tc03:1.42e+04></nb:4.250e+06></pre>
T He+11.18E+04 EHe+19.04E+05 T(O+):1.06E+04 EO+:8.17E+05 iter/zn: 2.890 Te-low:3.98E+03 Te-high:1.51E+04 Hlu/zn:3.87E+00
<a>:0.00E+00 erdeFe2.5E+20 Tcompt6.31E+02 Tthr1.46E+06 <tden>: 5.75E+03 <den>:9.79E-18 <mol>:1.21E+00</mol></den></tden>
Mean Jeans l(cm)1.02E+18 M(sun)4.75E+03 smallest: len(cm):8.44E+17 M(sun):2.73E+03 Alf(ox-tran): -1.4353
Optical Depths: CONTN; COMP: 1.11E-04 H-: 6.07E-04 R(1300): 1.04E-02 H2+ 3.59E-04 HeTri:7.66E-04
PfaillE-04 PaillE-04 PaillE-04 Hb5,43E-04 Lai2.56E-01 1r:9.752E+03 1.8:3.01E+03 4:4.760E+02 21R:4.919E+00
10830: 1.13E+02 3889: 4.80E+00 5876: 3.08E-04 7065: 1.70E-04
1550: 5.52E+01 2800: 3.57E+04 774: 1.00E-20 1240: 2.18E-01 1035: 1.00E-02 1335: 3.30E+04 977: 2.60E+03 1397: 6.62E+01
789: 1.51E+01 1207: 7.72E+02 1085: 1.72E+02 1194: 4.02E+00 1909: 1.04E-03 1895: 2.07E-02 2326: 1.65E-02 1666: 6.66E-03 1750: 3.18E-05 1025: 5.09E+03 352: 1.00E-20 347: 1.00E-20 1860: 6.50E+01 630: 2.06E+00 834: 2.81E+03 835: 3.33E+02
1750: 3.18E-05 1025: 5.09E+03 352: 1.00E-20 347: 1.00E-20 1860: 6.50E+01 630: 2.06E+00 834: 2.81E+03 835: 3.33E+02 1808: 3.08E+04 1256: 4.70E+02 -3: 1.64E+03 -48: 2.61E-04 3934: 7.13E+02 369: 3.59E+02 8498: 1.90E-02 8542: 1.70E-01
8662: 9.68E-02 353: 1.00E-20 1304: 1.74E+04 1122: 3.55E+01 990: 1.40E+02 1402: 2.01E-04 1214: 1.11E-05 1486: 6.06E-05
2335: 7.34E-02 1406: 6.23E-04 1656: 3.91E+01 9830: 6.52E-09 8727: 1.22E-07 6300: 4.62E-05 5577: 1.33E-06 7291: 4.78E-05
7324: 3.31E-05 1039: 2.48E+03 -8446: 4.88E-09 -4368: 1.85E-11 -132: 7.28E-13 -113: 7.27E-12 -29: 1.67E-11 -46: 1.09E-11
-245: 1.00E-20 765: 3.69E+01 -1198: 3.16E-05 786: 9.40E-02 C157: 1.69E-03 N122: 3.48E-05 N205: 4.25E-05 N57: 1.72E-05 0146: 4.20E-03 063: 1.63E-02 088: 8.05E-05 052: 1.64E-04
026: 1.12E-05 NE13: 1.09E-02 NE36: -1.84E-04 NE16: 1.73E-03 MG4: 2.57E-05 MG14: -6.96E-08 MG6: 5.45E-07 S135: 1.34E-03
S19: 7.66E-05 S34: 2.34E-05 S11: 2.54E-06 AR7: 5.35E-04 AR9: 4.46E-05 AR22:-2.55E-06 AR13: 8.43E-08 AR8: 1.57E-07
CA3: 5.71E-06 CA12:-2.77E-08 CA4: 2.31E-07 Ne14: 2.68E-07 Ne24: 6.53E-08 Si3: 1.00E-20 Si4: 1.00E-20 Fe7: 1.00E-20
Fe61: 1.00E-20 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 1.72E-11 Si6.5:-2.32E-13 C610: 1.06E-06 C370: 8.52E-08
Old hydro optical depths: 1 1.06E+04 2 3.19E-04 3 6.27E-04 4 1.77E-04 5 9.66E-11 6 2.22E-10 7 9.84E-10
Lines: 2-1 1.43E+08 3-2 7.73E-02 4-3 1.45E-07 5-4 9.19E-08 6-5 7.33E-09 7-6 9.97E-07 8-7 1.31E-05
New hydro optical depths: 1 9.75E+03 2 3.09E-04 3 6.08E-04 4 1.72E-04 5 9.76E-11 6 2.24E-10 7 9.93E-10
Lines: 2-1 1.30E+08 3-2 5.78E-02 4-3 1.88E-07 5-4 1.06E-07 6-5 1.46E-08 7-6 1.02E-06 8-7 1.34E-05
Old He Is optical depths: 1 3.28E+03 2 6.66E-04 3-1.18E-14 4-4.92E-14 5-1.02E-13 6-1.82E-13 7-2.06E-12
Lines: 2-1 8.90E+06 3-2 4.39E-03 4-3 5.34E-09 5-4 3.41E-09 6-5 1.96E-09 7-6 3.70E-08 8-7 4.82E-07
New HE Is optical depths: 1 3.01E+03 2 6.26E-04 3-1.22E-14 4-5.07E-14 5-1.05E-13 6-1.87E-13 7-2.13E-12
Lines: 2-1 8.06E+06 3-2 4.07E-03 4-3 5.47E-09 5-4 3.50E-09 6-5 2.01E-09 7-6 3.81E-08 8-7 4.95E-07
Old He II optical depths: 1 5.20E+02 2 1.06E+04 3-1.80E-14 4-4.69E-14 5-9.17E-14 6-1.59E-13 7-1.71E-12
Lines: 2-1 4.30E+05 3-2 3.32E-04 4-3 2.30E-10 5-4-1.34E-11 6-5-9.22E-10 7-6 3.65E-09 8-7 5.16E-08
New HE II optical depths: 1 4.76E+02 2 9.75E+03 3-1.76E-14 4-4.61E-14 5-9.00E-14 6-1.56E-13 7-1.67E-12
Lines: 2-1 3.90E+05 3-2 3.05E-04 4-3 2.27E-10 5-4-1.43E-11 6-5-9.15E-10 7-6 3.61E-09 8-7 5.10E-08
Hydrogen -0.040 -1.057 Log10 Mean Ionisation (over volume)
Helium -0.044 -1.083 -1.867
Carbon -2.840 -0.026 -1.268 -2.516 -4.360
Nitrogen -0.068 -1.009 -1.358 -2.433 -4.258 -5.673 Oxygen -0.059 -1.422 -1.330 -2.819 -4.428 -6.340
Oxygen -0.039 -1.422 -1.330 -2.819 -4.428 -6.340 Neon -0.183 -0.628 -0.979 -2.500 -4.101 -6.376
Magnesium -2.541 -0.032 -1.181 -2.645 -4.370 -5.792
Aluminum -3.237 -0.023 -1.414 -1.938 -3.544 -5.189
Silicon -3.380 -0.022 -1.402 -2.020 -3.237 -4.684 -8.324
Sulphur -3.989 -0.038 -1.105 -2.383 -3.968 -4.388 -6.111-10.065-12.546 Argon -0.165 -0.618 -1.183 -2.212 -3.794 -4.48 -6.045 -8.924-10.416-13.125-15.833
Calcium $-2.313 - 0.645 - 0.118 - 2.196 - 3.732 - 4.511 - 6.035$
Iron -1.997 -0.035 -1.532 -1.517 -2.278 -2.804 -4.046 -5.780

e sc18751 -2.500	0.0002	C 2 4267 -1.996	0.0007	O 4 789 -1.994	0.0007	Ca2K 3934 -0.837	0.0104
nFnu 4860 1.594	2.8123	TOTL 977 0.317	0.1484	TOTL 1218 -2.285	0.0004	Ca2H 3969 -1.068	0.0061
nFnu 1215 0.579	0.2711	C3 C 977 0.306	0.1449	0 5 1218 -2.364	0.0003	Ca2X 8498 -2.086	0.0006
Inci 4861 2.459	20.5900	C3 R 977 -1.308	0.0035	Ne 2 128 0.187	0.1100	Ca2Y 8542 -1.174	0.0048
Inci 1216 2.740	39.2935	TOTL 1909 1.545	2.5087	Ne 3 156 0.120	0.0943	Ca2Z 8662 -1.471	0.0024
BA C 0 1.789	4.3964	INWD 1909 1.244	1.2547	Ne 3 361 -1.415	0.0028	CaF1 7291 0.051	0.0804
PA C 0 1.264	1.3142	C 3 1907 0.267	0.1323	Ne 3 3869 1.224	1.1971	CaF2 7324 -0.118	0.0545
H FF 0 1.466	2.0899	C 3 1909 1.521	2.3764	Ne 3 3968 0.710	0.3673	Ca 4 32 -1.198	0.0045
H FB 0 1.570	2.6572	C3 R 1909 -1.469	0.0024	Ne 3 3343 -1.069	0.0061	Fe 2 48 -0.724	0.0135
Cool 1216 2.383	17.3008	Phot 1909 -0.513	0.0220	Ne 3 1815 -0.929	0.0084	Fe 2 7 1.003	0.7210
Crst 960 -0.036	0.0658	C 3 2297 -1.826	0.0011	Ne 4 2424 -0.859	0.0099	Emis 3 1.368	1.6687
Cool 6563 -1.904	0.0009	C 4 1549 0.641	0.3132	Ne 4 4720 -1.336	0.0033	Cool 3 1.368	1.6699
Crst 4861 -2.813	0.0001	INWD 1549 0.484	0.2180	Ne 4 1602 -0.720	0.0136	TOT 0 1.526	2.4034
H2 1 2 -2.214	0.0004	DEST 1549 -2.736	0.0001	Ne 5 3426 -1.709	0.0014	FEIR 0 0.082	0.0865
H-FB 0 -0.225	0.0426	N 1 5200 -1.624	0.0017	Ne 5 3346 -2.141	0.0005	Fe 3 0 0.713	0.3693
H2+ 0 -0.592	0.0183	N 1 1200 -2.401	0.0003	Ne 5 143 -2.806	0.0001	Fe 3 5270 0.033	0.0772
HEH+ 0 -1.548	0.0020	N 2 6584 0.253	0.1282	Mg 1 4571 -2.517	0.0002	Fe 3 4658 0.277	0.1354
HeFF 0 0.663	0.3293	N 2 6548 -0.224	0.0427	Emis 2798 1.684	3.4589	Fe 3 1122 -1.086	0.0059
HeFB 0 0.825	0.4783	N 2 5755 -0.046	0.0643	Cool 2798 1.684	3.4593	Fe 5 3892 0.002	0.0718
MeFB 0 -1.980	0.0007	N 2 5680 -2.428	0.0003	Mg 4 4 -1.009	0.0070	Fe 6 0 -0.943	0.0082
MeFF 0 -1.287	0.0037	N 2 2140 0.011	0.0734	Mg 5 56 -1.959	0.0008	Fe 6 5177 -1.394	0.0029
Toff 0 1.530	2.4230	N 2 1084 -1.213	0.0044	Mg 5 2751 -2.809	0.0001	Fe 7 6087 -2.293	0.0004
HeIC 584 -2.775	0.0001	N 3 1750 0.372	0.1685	Al 3 1860 -0.202	0.0449	Totl 2 -2.388	0.0003
esc 584 0.385	0.1738	N 3 57 -2.597	0.0002	Si 2 35 -0.864	0.0098	AugC 2 -2.388	0.0003

	1	2	3	4	5	6	/	8	9	10	11	12	13	14	15	10	17
**	0 040	1 057						ean Ionis									
Hydrogen Helium		-1.057	-1.867			LOG	gio M	ean ionis	ation	(over 1	radius)						
Carbon				-2.516 -	4 260												
Nitrogen						F 672											
Oxygen				-2.433 -													
Neon				-2.500 -													
Magnesium																	
Aluminum																	
Silicon				-2.020 -			_8 32	4									
								1-10.065-	12.546								
Argon								5 -8.924-		-13.129	5-15.83	3					
				-2.196 -					10.110	10.12.	10.00						
Iron								6 -5.780									
0.5-1.0KE	V:9.02E	+09 1.0	-1.5:5.4	9E+09 1.	5-2.0:3	3.06E+09	9 2.0	-2.5:2.05	E+09 2	.5-3:1	.62E+09	3-5:3.2	1E+09 5-	7.5:1	.88E+09	7.5-1	0:1.11E+09
								rmalised									
	332 0			30 1.216				6 1.129					0.47 1.0		0.51 1.0		0.56 1.033
0.62 1.	022 0	.67 1.0	13 0.7	4 0.925	0.81	0.997	0.8	8 0.992	0.97 (0.992	0.98	0.992	0.99 0.99	92	1.00 0.9	92	
Inward co	ntinua	(nuFnu)	at bear	of Balm	ner Lur	an cor	ioe.	1.04E+02	2 5 91	7+02							
inward co	meinaa	(nur nu)	ut neut	OI DUI	uer, by	adni ser.	163,	1.040.02	2.551	1102							
Outwrd co	ontinua	(nuFnu)	at head	l of Balm	mer, Lyr	nan ser:	ies;	1.04E+02	0.001	E+00							
		. ,															
							rgent	continuu	m - pho	ot/ryd/	/cm2 (r	in)					
	94E+14				1.74-20			.97E+06		1.86E-		1.26E+03	1.81E+0	6	3.24E+05	3.70	E+00
	29E+14				2.72-18			.51E+07		1.68E-		1.88E+03			4.81E+05		
	81E+14				1.39-16			.67E+07		1.50E-		2.79E+03			7.16E+05		
	45E+14				1.86-13			.03E+08		1.34E-		4.14E+03			1.06E+06		
	16E+14				1.30E-9			.68E+08		1.19E-		6.16E+03			1.58E+06	5.37	E-02
	66E+13				1.41E-6			.44E+08		1.05E-		9.15E+03			2.35E+06		
	87E+13				3.31E+0			.06E+08		9.26E-		1.36E+04			3.49E+06		
	46E+13				6.42E-3			.69E+08		8.15E-		2.02E+04			5.19E+06	2.25	E-03
	33E+13				3.17E+0			.85E+08		7.15E-		3.00E+04					
	88E+13				6.34E-1			.80E+08		5.18E-		4.46E+04					
	66E+13				6.05E-0			.60E+08		2.67E-		6.64E+04					
	05E+13				9.95E-0			.45E+08		1.36E+		9.86E+04					
	95E+13		.44-294		8.57E+0			.23E+08		6.96E-		1.47E+05					
0.99 2.	91E+13	3.03 1	.93E-21	15.4	8.65E+0	14 6	9.5 2	.05E+08	849.0	3.55E-	+00	2.18E+05	1.0/E+0	T			

*	
* title map of heating vs cooling	
* hden 0	
* table agn	
<pre>ionization parameter -2.5</pre>	,
* c change plot to punch to generate plot for hazy	
* plot map	
stop zone 1	,
print short	
c map.in	
* c cray	
k –	

Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

546Cell Peak1.78E+00 P(nu>1ryd): -2.2020	Lo 1.00E-05=0.9101cm Average nu:3.038E+00	Hi-Con:7.34E+06 Ryd P(X-ray): -3.0307	E(hi):7.35E+06Ryd P(BalC): -2.6977	E(hi): 100.01 MeV Q(Balmer C): 8.2651
Q(1.0-1.8): 7.6738	Q(1.8-4.0): 7.5661	Q(4.0-20): 7.0287	Q(20): 5.2913	Ion pht flx:9.489E+07
L(gam ray): -3.2922	Q(gam ray): 3.1227	L(Infred): -2.4837	Alf(ox): -1.4120	Total lumin: -1.9367
U(1.0):3.165E-03	U(4.0):3.628E-04	T(En-Den):2.673E+00	T(Comp):1.327E+07	nuJnu(912A):2.006E-03
Occ(FarIR):1.783E-10	Occ(H n=6):6.724E-14	Occ(1Ryd):9.248E-20	Occ(4R):4.741E-22	Occ (Nu-hi):6.607E-50
Tbr(FarIR):2.966E-10	Tbr(H n=6):2.985E-10	Tbr(1Ryd):1.461E-14	Tbr(4R):2.999E-16	Tbr (Nu-hi):7.291E-38

 Tbr(FarIR):2.966E-10
 Tbr(H n=6):2.985E-10
 Tbr(lRyd):1.461E-14
 Tbr(AR):2.995E-16
 Tbr (Nu-h):7.291E-38

 #####
 1 Ter:7.535E+03
 Hden:1.000E+00
 Ne:1.173E+00
 R:1.000E+25
 R=R0:1.362E+18
 R:2.723E+18
 NIR:
 2 Hott8.617E-24
 T912: 4.640E-02###

 -6.05
 6466
 0.15876
 0.02
 1909
 0.04
 15876
 0.02
 1009
 0.04
 16584
 0.03
 5007
 2.055
 30.00
 0.00
 2798
 0.03
 1035
 0.00

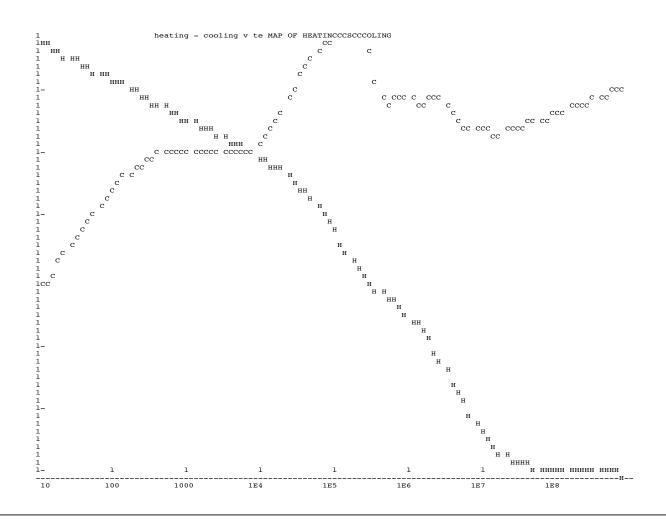
 Hydrogen
 2.707E-03
 9.973E-01
 H+0/Hden:
 1.000E+00
 7.847E-11
 H
 H2
 7.958E-12
 4.252E-11
 H2+
 HeH + 3.629E-11
 H col den
 2.723E+18

 Helium
 8.35E-04
 8.10E-16
 2.155E-22
 2.979E-22
 4.40E-20
 Ter((L); 3.281E+03
 Tercota)
 1.00E+00
 Gam 1/tot 1.00DE+10

 Helium
 8.335E-04
 8.130E-16
 2.155E-22
 2.979E-22
 4.40E-22
 3.6676E-10
 5.10E-21
 1.210E-22
 9.18BE-22
 2.867E-22

 Pressure
 NgasTgas;
 1.636E+04
 P(total):
 2.259E-12
 P(Radtn):
 5.148E-16
 <t

Iron 0.000E+00 2.831E-04 2.203E-02 2.347E-01 3.841E-01 3.181E-01 3.946E-02 1.3341
Calculation stopped because NZONE reached.
Geometry is plane-parallel.
Frequency out of range of free-free gaunt factor routine.
OI negative level populations 3 times.
!Incident radiation field < 10*Habing diffuse ISM field. Is this OK?
C-The Lyman continuum is thin, and I assumed that it was thick. Try another iteration.
C-The HeII continuum is thin and I assumed that it was thick. Try another iteration.



*********************************** CLOUDA 80.08 <*******************************	*****
* title map of heating vs cooling	*
* hden 0	*
* table agn	*
* ionization parameter -2.5	*
* c change plot to punch to generate plot for hazy	*
* plot map	*
* stop zone 1	*
* print short	*
* c map.in	*
* c cray	*
***********************************> LOG(U): -2.50 <*****************************	*****
>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	
>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	

Emission Line Spectrum. Constant Density Model. Open geometry. Iteration 1 of 1. Intensity (erg/s/cm^2)

TOTL 4861 -6.046 1.0000	HeFB 0 -6.458	0.3871	N 2 6548 -7.990	0.0114	PHOT 1895 -8.533	0.0033
TOTL 1216 -4.459 38.5697	MeFF 0 -8.314	0.0054	N 2 122 -8.414	0.0043	Si 6 19 -8.984	0.0012
TotH 0 -4.630 26.0688	Toff 0 -6.196	0.7075	N 2 203 -8.265	0.0060	S 2 6720 -7.184	0.0728
BFH1 0 -4.962 12.1214	esc 584 -6.923	0.1327	N 3 1750 -8.901	0.0014	S 2 4074 -8.707	0.0022
BFHe 0 -4.953 12.3919	He2p 910 -8.012	0.0108	N 3 57 -6.630	0.2604	S 210330 -8.881	0.0015
TotM 0 -5.854 1.5552	He I 504 -6.554	0.3105	TOTL 3727 -7.158	0.0773	S II 6731 -7.575	0.0295
CA B 4861 -6.293 0.5656	He I 4471 -8.228	0.0066	O II 3729 -7.380	0.0463	S II 6716 -7.410	0.0432
CA B 1216 -4.767 19.0184	TOTL 5876 -7.737	0.0204	O II 3726 -7.558	0.0307	S II 4070 -8.830	0.0016
DU B 4861 -6.293 0.5656	Ca B 5876 -7.761	0.0192	O 2 4651 -8.743	0.0020	S 3 18 -6.425	0.4174
Q(H) 4861 -4.346 50.0773	TOTL10830 -7.559	0.0307	0 3 1663 -8.611	0.0027	S 3 34 -6.130	0.8241
Q(H) 1216 -2.8121712.1424	TOTL 3889 -7.924	0.0132	Rec 1663 -7.430	0.0412	S 3 9532 -6.183	0.7293
TOTL 6563 -5.537 3.2289	TOTL 7065 -8.596	0.0028	O 3 5007 -5.622	2.6516	S 3 9069 -6.599	0.2800
TOTL 4861 -6.046 1.0000	He I 2 -8.427	0.0042	0 3 4959 -6.099	0.8839	S 3 6312 -8.167	0.0076
TOTL 4340 -6.392 0.4501	He I 5016 -8.486	0.0036	TOTL 4363 -8.294	0.0057	S 3 3722 -8.396	0.0045
TOTL 4102 -6.657 0.2445	DevB 5016 -8.935	0.0013	Rec 4363 -8.306	0.0055	S 4 105 -6.251	0.6235
TOTL18751 -6.603 0.2769	He I 3965 -8.782	0.0018	0 3 2321 -8.921	0.0013	Ar 2 7 -8.847	0.0016
TOTL12818 -6.923 0.1326	HeII 228 -5.099	8.8416	C EX 4363 -8.746	0.0020	Ar 3 7135 -7.274	0.0592
TOTL10938 -7.181 0.0733	ESC 304 -6.916	0.1347	C EX 5592 -8.675	0.0023	Ar 3 7751 -7.903	0.0139
TOTL40512 -7.334 0.0515	He2C 911 -5.971	1.1873	0 3 880 -5.553	3.1098	Ar 3 22 -8.340	0.0051
TOTL26252 -7.565 0.0303	TOTL 1640 -5.596	2.8134	0 3 520 -5.807	1.7319	Ar 3 9 -7.207	0.0690
TOTL74578 -7.894 0.0142	TOTL 4686 -6.559	0.3068	O 3 3341 -8.688	0.0023	Ar 4 4740 -7.618	0.0267
2 NU 0 -5.055 9.7971	TOTL 1216 -6.001	1.1077	0 4 26 -5.084	9.1662	Ar 5 7007 -8.494	0.0036
TOTL 1216 -4.459 38.5697	Ca B 1640 -5.532	3.2625	CONT 1401 -7.431	0.0412	Ar 5 6435 -8.861	0.0015
TOTL 1026 -7.430 0.0413	DevB 1640 -5.535	3.2444	Ne 2 128 -8.363	0.0048	Ar 5 131 -8.387	0.0046
TOTL 973 -7.444 0.0400	Ca B 4686 -6.328	0.5218	Ne 3 156 -6.108	0.8667	Ar 5 79 -8.473	0.0037
TOTL 950 -7.408 0.0434	DevB 4686 -6.335	0.5132	Ne 3 361 -7.173	0.0745	Ca 2 3933 -7.572	0.0298
TOTL 938 -7.339 0.0509	C 2 158 -6.991	0.1135	Ne 3 3869 -6.842	0.1599	Ca 2 7306 -6.879	0.1469
INWD 1216 -4.459 38.5697	C 2 2326 -8.165	0.0076	Ne 3 3968 -7.355	0.0490	Ca2K 3934 -7.755	0.0195
Dest 1216 -8.919 0.0013	REC 1335 -7.131	0.0822	Ne 4 $2424 = 7.949$	0.0125	Ca2H 3969 -8.036	0.0102
e sc 6563 -8.921 0.0013	C 2 4267 -8.971	0.0012	Ne 5 3426 -8.413	0.0043	CaF1 7291 -7.104	0.0875
e sc 4861 -8.570 0.0030	TOTL 977 -7.309	0.0546	Ne 5 3346 -8.845	0.0016	CaF2 7324 -7.272	0.0595
e sc18751 -6.603 0.2771	C3 R 977 -7.309	0.0546	Ne 5 242 -6.696	0.2238	Ca 4 32 -7.620	0.0266
e sc40512 -7.333 0.0516	TOTL 1909 -7.488	0.0361	Ne 5 143 -6.780	0.1842	Ca 5 4 -8.604	0.0028
nFnu 4860 -5.626 2.6311	C 3 1907 -7.707	0.0218	Emis 2798 -7.645	0.0251	Fe 3 0 -8.273	0.0059
nFnu 1215 -7.802 0.0175	C 3 1909 -7.891	0.0143	Cool 2798 -7.645	0.0251	Fe 3 5270 -8.953	0.0012
Inci 4861 -3.0411011.1165	C3 R 1909 -7.471	0.0376	Mg 4 4 -7.001	0.1108	Fe 3 4658 -8.709	0.0022
Inci 1216 -2.7601929.5989	Phot 1909 -7.595	0.0283	Mg 5 13 -7.863	0.0152	Fe 5 3892 -7.211	0.0683
BA C 0 -5.700 2.2145	C 3 2297 -7.816	0.0170	Mg 5 56 -7.071	0.0944	Fe 6 0 -7.523	0.0333
PA C 0 -6.202 0.6973	C 3 4649 -8.988	0.0011	Al 3 1860 -9.040	0.0010	Fe 6 5177 -7.974	0.0118
H FF 0 -6.320 0.5312	C 4 1549 -8.116	0.0085	Si 2 35 -6.799	0.1765	Fe 7 6087 -8.401	0.0044
H FB 0 -5.984 1.1515	C4 r 1549 - 8.555	0.0031	Si 2 2335 -8.696	0.0022	10 / 000/ -0.401	0.0044
	0.1 1049 -0.555	0.0001	51 2 2555 -0.050	0.0022		

Cooling: O 3 5007:0.103 Heating: BFH1 0:0.465	MAP OF HEATING VS COOLING O 3 880:0.120 O 3 520:0.06 BFHe 0:0.475 TotM 0:0.06(
ENERGY BUDGET: Heat: -4.0 Column density H12:2.723E	96 U(4-): -3.4403 U(sp): -2.56 30 Coolg: -4.633 Error: 0.85 18 H II:2.716E+18 HI:7.372E+15	Compt H: -9.679	WorkF: -4.065 F-F H-11.088 PRADMX:1.8	4E+03
			NeN+dl:3.19E+18 <t(c3)>:7.53E+03 <e(c3)>:1. L THIN:1.00E+30 <t(s2)>:7.53E+03 <e(s2)>:1.</e(s2)></t(s2)></e(c3)></t(c3)>	
T He+:7.53E+03 EHe+:1.17E- <a>:0.00E+00 erdeFe7.8E-	00 T(O+):7.53E+03 EO+:1.17E+00) iter/zn: 3.000	L THIN:1.00E+30 <t(s2)>:7.53E+03 <e(s2)>:1. Te-low:7.53E+03 Te-high:7.53E+03 Hlu/zn:1. <dens>:2.36E-24 <mol>:6.24E-01</mol></dens></e(s2)></t(s2)>	
Mean Jeans l(cm)4.51E-	21 M(sun)5.70E+07 smallest:	len(cm):4.48E+21	M(sun):5.57E+07 Alf(ox-tran): -1.4125	

**************************************	*****
*	*
* title "conventional" BLR model	*
* constant pressure	*
* ionization parameter -2	*
stop column density 23	*
table agn	*
print last iteration	*
iterate	*
hden 9.5	*
c oldblr.in	*
c cray	*
к [—]	*

Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

546Cell Peak1.78E+00	Lo 1.00E-05=0.9101cm	Hi-Con:7.34E+06 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 7.7980	Average nu:3.038E+00	P(X-ray): 6.9693	P(BalC): 7.3023	Q(Balmer C): 18.2651
Q(1.0-1.8): 17.6738	Q(1.8-4.0): 17.5661	Q(4.0-20): 17.0287	Q(20): 15.2913	Ion pht flx:9.489E+17
L(gam ray): 6.7078	Q(gam ray): 13.1227	L(Infred): 7.5163	Alf(ox): -1.4120	Total lumin: 8.0633
U(1.0):1.001E-02	U(4.0):1.147E-03	T(En-Den):8.451E+02	T(Comp):1.327E+07	nuJnu(912A):2.006E+07
Occ(FarIR):1.783E+00	Occ(H n=6):6.724E-04	Occ(1Ryd):9.248E-10	Occ(4R):4.741E-12	Occ (Nu-hi):6.607E-40
Tbr(FarIR):2.966E+00	Tbr(H n=6):2.985E+00	Tbr(1Ryd):1.461E-04	Tbr(4R):2.999E-06	Tbr (Nu-hi):7.291E-28

1 Te:1.628E+04 Hden:3.162E+09 Ne:3.774E+09 R:1.000E+25 R-R0:9.508E+07 dR:1.902E+08 NTR: 1 Htot:6.556E-05 T912: 1.832E-03###
2.45 4686 0.64 5876 0.01 1909 2.21 1549 23.38 6584 0.00 2326 0.03 3727 0.00 6300 0.00 2798 0.18 1035 0.05
Hydrogen 4.841E-04 9.995E-01 H+0/Hden: 1.000E+00 2.949E-14 H- H2 3.760E-13 5.683E-12 H2+ HeH+ 1.050E-12 H col den 6.013E+17
H 2SP 3-6 2.924E-10 3.682E-10 2.653E-11 2.732E-11 3.395E-11 3.633E-11 Texc(La); 7.789E+03 T(contn): 8.450E+02 T(diffs): 4.018E+03
Helium 4.528E-05 7.000E-02 9.300E-01 He I 2S3 2.279E-07 Comp H, C 2.470E-09 3.030E-12 Fill Fact 1.000E+00 Gam 1/tot 9.514E-01
He singlet 4.505E-05 1.870E-11 1.208E-13 1.706E-13 2.524E-13 3.657E-13 He triplt 2.278E-07 7.915E-11 5.879E-13 1.446E-12 3.583E-13
HeII 7.000E-02 1.218E-09 3.301E-12 5.034E-12 8.119E-12 1.265E-11 1.183E-10 1.874E-09 2.380E-07 PRAD/GAS; 1.996E-02
Pressure NgasTgas; 1.177E+14 P(total): 1.657E-02 P(gas): 1.625E-02 P(Radtn): 3.243E-04 Rad accel 1.476E+00 Force Mul 1.136E+03
Carbon 1.698E-06 4.552E-03 2.221E-01 6.379E-01 1.353E-01 2.143E-04 0.000E+00 H2O+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 6.630E-07 2.126E-03 2.095E-01 5.899E-01 1.807E-01 1.784E-02 0.000E+00 0.000E+00 02/Ototl: 0.000E+00 02/Ototl: 0.000E+00
Oxygen 3.923E-07 1.578E-03 1.877E-01 6.264E-01 1.715E-01 1.231E-02 4.154E-04 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.644
Neon 2.833E-07 6.272E-04 1.483E-01 5.411E-01 2.942E-01 1.575E-02 5.592E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 9.135E-06 3.303E-03 2.197E-01 5.249E-01 1.964E-01 5.337E-02 2.286E-03 2.727E-05 3.303E-07 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 1.948E-05 2.377E-02 2.518E-01 5.081E-01 1.700E-01 4.371E-02 2.453E-03 3.020E-05 2.068E-07 1.381E-09 0.000E+00 0.000E+00
Silicon 0 1.686E-06 4.711E-03 2.085E-01 4.915E-01 2.342E-01 5.744E-02 3.485E-03 6.466E-05 5.369E-07 3.461E-09 1.843E-11 0.000E+00
Sulphur 1 6.431E-03 3.833E-01 4.166E-01 1.149E-01 6.978E-02 8.877E-03 1.638E-04 1.740E-06 1.142E-08 6.375E-11 2.705E-13 1.005E-15
Argon 3 4.654E-01 2.905E-01 3.789E-02 9.496E-03 6.604E-04 8.181E-05 5.594E-07 2.698E-09 1.002E-11 2.960E-14 9.430E-17 2.219E-19
Calcium 0 7.216E-05 1.133E-02 1.287E-01 3.767E-01 2.435E-01 1.954E-01 4.114E-02 3.106E-03 1.487E-04 0.000E+00 0.000E+00 0.000E+00
Iron 0 0.000E+00 1.995E-06 8.073E-04 3.162E-02 1.686E-01 5.227E-01 2.458E-01 2.989E-02 5.619E-04 2.197E-05 0.000E+00 0.000E+00
#####193 Te:5.422E+03 Hden:2.216E+10 Ne:1.204E+08 R:1.000E+25 R-R0:5.066E+12 dR:4.638E+11 NTR: 4 Htot:9.555E-08 T912: 6.162E+05###
5.52 4686 0.17 5876 0.20 1909 7.15 1549 18.68 6584 0.00 2326 0.47 3727 0.00 6300 0.06 2798 5.75 1035 0.01
Hydrogen 9.953E-01 4.736E-03 H+0/Hden: 1.000E+00 1.242E-09 H- H2 1.578E-06 3.949E-09 H2+ HeH+ 1.937E-09 H col den 1.001E+23
H 2SP 3-6 1.271E-06 3.812E-06 4.933E-09 8.040E-11 8.671E-12 5.348E-12 Texc(La); 6.251E+03 T(contn): 7.171E+02 T(diffs): 3.848E+02
Helium 9.982E-01 1.767E-03 0.000E+00 He I 2S3 1.123E-08 Comp H, C 7.634E-11 1.684E-14 Fill Fact 1.000E+00 Gam 1/tot 3.072E-02
He singlet 9.982E-01 4.959E-13 2.960E-16 3.811E-16 5.923E-16 8.958E-16 He triplt 1.122E-08 3.031E-12 1.024E-14 3.443E-15 2.880E-14
HeII 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 PRAD/GAS; 1.499E-03
Pressure NgasTgas; 1.330E+14 P(total): 1.838E-02 P(gas): 1.836E-02 P(Radtn): 3.057E-05 Rad accel 6.239E-04 Force Mul 1.999E+02
Carbon 9.397E-05 9.999E-01 6.084E-06 0.000E+00 0.000E+00 0.000E+00 H2O+/Otot 0.000E+00 OH+/Otot1 0.000E+00
Nitrogen 9.014E-01 9.665E-02 1.164E-08 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.2/Ototl: 0.000E+00 02/Ototl: 0.000E+00 0.000E+000E+
Oxygen 9.959E-01 4.131E-03 2.471E-08 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.384

Neon 9.913E-01 7.636E-03 1.099E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Magnesium 0 3.815E-04 9.817E-01 1.789E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Aluminium 0 3.953E-05 9.964E-01 2.860E-03 7.054E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Silicon 0 4,400E-05 1,000E+00 5,422E-06 0,000E+00 0,000E+00 0,000E+00 0,000E+00 0,000E+00 0,000E+00 0,000E+00 0,000E+00
Sulphur 0 2.601E-05 9.974E-01 2.612E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Argon 0 9.745E-01 2.542E-02 4.806E-05 0.000E+00
Calcium 0 2.814E-05 2.819E-02 9.718E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Iron 0 7.983E-04 9.992E-01 3.662E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calculation stopped because column dens reached.
Geometry is plane-parallel.
FeII-MgII photoionization of H N=2 reached 22.5 percent of the total rate out.
Photoionization of He 2Tris reached 58.1 percent of the total rate out.
The largest continuum occupation number was 1.783E+00 at 1.054E-05 Ryd.
Hydrogen self ionization by alpha transitions reached 0.1% of the destruction rate for level 3.
Some fine struc lines are optically thick, largest=2.21E+00
Continuum occupation number reached 1.50E+02 for some fine structure transitions.
Stimulated emission was 6.7% of the total for H transition 7 - 6
Timescale-photoerosion of Fe=2.58E+08yr
Sum of gas+line rad pressure ranged from $1.65E-02$ to $1.87E-02$ in a constant pressure model.
Frequency out of range of free-free gaunt factor routine.
Balmer continuum optical depth is 6.98E-02
Continuum optical depth at low nu (1.054E-05 Ryd) was 2.115E+02
The optical depth to Rayleigh scattering at 1300A is 6.57E-01
Line radiation pressure capped by thermalization length.

CLOUDY 80.08

***************	CLOUDY 80.08	<*****
* title "conventional" BLR model		*
* constant pressure		*
* ionization parameter -2		*
* stop column density 23		*
* table agn		*
<pre>* print last iteration</pre>		*
* iterate		*
* hden 9.5		*
* c oldblr.in		*
* c cray		*
**************************************	OG(U): -2.00	<*************************************

Emission Line Spectrum. Constant Pressure Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2)

						, _, _, _,					
TOTL 4861	5.519	1.0000	HEH+ 0	2.945	0.0027	N 2 2140	4.164	0.0441	PHOT 1895	3.353	0.0068
TOTL 1216	7.203	48.3003		5.175	0.4528	N 2 1084	3.144	0.0042	Si 4 1397	5.893	2.3639
TotH 0	7.346	67.0768	HeFB 0	5.311	0.6187	N 3 1750	5.401	0.7613	Si 6 19	2.649	0.0013
BFH1 0	7.150	42.7253	MeFB 0	3.311	0.0062	N 3 990	3.948	0.0268	S 1R 1807	2.284	0.0006
BFHx 0	5.237	0.5221	MeFF 0	4.010	0.0310	N 4 1486	5.360	0.6926	S 2 6720	2.149	0.0004
BFHe 0	6.750	17.0097	Toff 0	6.083	3.6582	N 4 765	3.504	0.0097	S 2 4074	3.658	0.0138
TotM 0	6.319	6.3014	esc 584	4.823	0.2014	N 4 1718	2.700	0.0015	S 210330	3.458	0.0087
FF H 0		0.0035	He I 504	5.531		N 5 1240	4.568		S II 6731	1.991	0.0003
	3.057				1.0267			0.1118			
ComH 0	3.203	0.0048	He I 4471	4.231	0.0515	O 1 6300	4.265	0.0556	S II 6716	1.634	0.0001
н– н 0	4.825	0.2021	TOTL 5876	4.824	0.2017	O 1 6363	3.788	0.0185	S II 4070	3.577	0.0114
CA B 4861	5.637	1.3105	Ca B 5876	4.664	0.1395	O 1 5577	3.785	0.0184	S II 4078	2.886	0.0023
CA B 1216	7.184	46.2181	TOTL10830	5.675	1.4297	O 1 630	1.687	0.0001	S II10323	3.074	0.0036
DU B 4861	5.637	1.3104	INWD10830	5.575	1.1356	O 1 7774	2.144	0.0004	S II10289	2.945	0.0027
Q(H) 4861	5.654	1.3630	TOTL 3889	4.203	0.0483	6lev 8446	3.949	0.0269	S II10205	2.416	0.0008
Q(H) 1216	7.188	46.6025	TOTL 7065	4.693	0.1493	6lev 1304	5.328	0.6434	S II10339	2.736	0.0016
TOTL 6563	6.293	5.9365	CcHE 0	5.659	1.3799	6lev 11	4.386	0.0735	S II 1256	2.360	0.0007
TOTL 4861	5.519	1.0000	HeI 2	4.062	0.0349	TOTL 7325	2.679	0.0014	S 3 9532	2.457	0.0009
TOTL 4340	5.117	0.3956	DevB 2	3.274	0.0057	O II 2471	2.592	0.0012	S 3 9069	2.041	0.0003
TOTL 4102	4.817	0.1983	He I 5016	4.019	0.0316	O II 7323	2.432	0.0008	S 3 6312	2.793	0.0019
TOTL18751	5.399	0.7582	DevB 5016	3.661	0.0138	O II 7332	2.317	0.0006	S 3 3722	2.564	0.0011
TOTL12818	4.997	0.3005	He I 3965	3.731	0.0163	O II 834	3.119	0.0040	S 3 1198	3.806	0.0194
TOTL10938	4.645	0.1336	DevB 3965	3.160	0.0044		3.380	0.0072	S 3 1729	4.146	0.0423
TOTL40512	4.674	0.1429	He I 3614	3.448	0.0085	O 3 1663	6.023	3.1856	S 4 1406	4.639	0.1316
TOTL26252		0.0836	DevB 3614	3.024	0.0032	Augr 1663	2.958	0.0027	S 5 1198	3.339	0.0066
TOTL74578	4.106	0.0386	He I 3448	3.229	0.0051	Rec 1663	4.133	0.0411	S 5 786	1.784	0.0002
2 NU 0	5.210	0.4899	DevB 3448	2.621	0.0013	O 3 5007	3.786	0.0185	S 6 933	3.002	0.0030
TOTL 1216		48.3003	HeII 228	5.722	1.5947	O 3 4959	3.309	0.0062	Ar 2 7	1.826	0.0002
TOTL 1026		0.1125	ESC 304	5.218	0.4997	LOST 5007	3.495	0.0095		2.473	0.0002
TOTL 973	3.737	0.0165	He2C 911	5.060	0.3474	TOTL 4363	4.140	0.0418	Ar 3 7751	1.843	0.0002
TOTL 950	3.594	0.0119	TOTL 1640	5.714	1.5652	O 3 2321	3.513	0.0099	Ar 4 7335	2.476	0.0009
TOTL 938	3.472	0.0090	TOTL 4686	4.751	0.1703	C EX 5592	2.417	0.0008	Ar 5 7007	1.601	0.0001
LA X 1216	5.219	0.5009	TOTL 1216	5.295	0.5962	O 3 834	4.525	0.1013	Ca 2 3933	3.975	0.0285
Ind2 1216	1.609	0.0001	Ca B 1640	5.527	1.0185	0 3 3341	2.715	0.0016	Ca 2 8579	4.115	0.0394
C13c 6563	4.579	0.1146	DevB 1640	5.526	1.0153	0 4 1402	5.220	0.5023	Ca 2 7306	3.280	0.0058
C14c 4861	3.524	0.0101	Ca B 4686	4.656	0.1371	CONT 1401	4.343	0.0667	Phot 7306	2.400	0.0008
CION 0	5.491	0.9359	DevB 4686	4.651	0.1354	O 4 789	4.254	0.0542	Ca2K 3934	3.715	0.0157
INWD 1216	7.203	48.2772	C 1 1656	1.930	0.0003	O 4 3412	2.735	0.0016	Ca2H 3969	3.629	0.0129
11000 1210											
				4.173			2.661	0.0014			0.0150
INWD 6563	6.274	5.6798	REC 1656	4.173	0.0450	O 5 630	2.661	0.0014	Ca2X 8498	3.695	0.0150
INWD 6563 INWD 4861	6.274 5.513	5.6798 0.9849	REC 1656 C 2 2326	5.187	0.0450 0.4656	O 5 630 TOTL 1218	4.601	0.1208	Ca2X 8498 Ca2Y 8542	3.695 3.609	0.0123
INWD 6563 INWD 4861 INWD18751	6.274 5.513 5.353	5.6798 0.9849 0.6809	REC 1656 C 2 2326 INWD 2326	5.187 5.082	0.0450 0.4656 0.3655	O 5 630 TOTL 1218 O 5 1218	4.601 4.601	0.1208	Ca2X 8498 Ca2Y 8542 Ca2Z 8662	3.695 3.609 3.601	0.0123
INWD 6563 INWD 4861 INWD18751 Strk 1216	6.274 5.513 5.353 3.718	5.6798 0.9849 0.6809 0.0158	REC 1656 C 2 2326 INWD 2326 C 2 1335	5.187 5.082 4.698	0.0450 0.4656 0.3655 0.1507	O 5 630 TOTL 1218 O 5 1218 O 6 1035	4.601 4.601 3.533	0.1208 0.1208 0.0103	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291	3.695 3.609 3.601 3.047	0.0123 0.0121 0.0034
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216	6.274 5.513 5.353 3.718	5.6798 0.9849 0.6809 0.0158	REC 1656 C 2 2326 INWD 2326 C 2 1335	5.187 5.082 4.698	0.0450 0.4656 0.3655 0.1507	O 5 630 TOTL 1218 O 5 1218 O 6 1035	4.601 4.601 3.533	0.1208 0.1208 0.0103	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291	3.695 3.609 3.601 3.047	0.0123 0.0121 0.0034
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563	6.274 5.513 5.353 3.718 4.908	5.6798 0.9849 0.6809 0.0158 0.2445	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335	5.187 5.082 4.698 4.639	0.0450 0.4656 0.3655 0.1507 0.1318	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128	4.601 4.601 3.533 2.096	0.1208 0.1208 0.0103 0.0004	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324	3.695 3.609 3.601 3.047 2.898	0.0123 0.0121 0.0034 0.0024
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861	6.274 5.513 5.353 3.718 4.908 3.851	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267	5.187 5.082 4.698 4.639 2.931	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	O 5 630 TOTL 1218 O 5 1218 O 6 1035 Ne 2 128 Ne 3 156	4.601 4.601 3.533 2.096 1.746	0.1208 0.1208 0.0103 0.0004 0.0002	Ca2X 8498 Ca2X 8542 Ca2Z 8562 CaP1 7291 CaP2 7324 Rec 3933	3.695 3.609 3.601 3.047 2.898 2.316	0.0123 0.0121 0.0034 0.0024 0.0006
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563 Strk 4861 Strk 4861	6.274 5.513 5.353 3.718 4.908 3.851 3.851	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267	5.187 5.082 4.698 4.639 2.931	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869	4.601 4.601 3.533 2.096 1.746	0.1208 0.1208 0.0103 0.0004 0.0002	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933	3.695 3.609 3.601 3.047 2.898 2.316	0.0123 0.0121 0.0034 0.0024 0.0006
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861 Strk18751 Strk18751	6.274 5.513 5.353 3.718 4.908 3.851 3.668 2.749	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977	5.187 5.082 4.698 4.639 2.931 5.557 5.490	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3968	4.601 4.601 3.533 2.096 1.746 3.816 3.303	0.1208 0.1208 0.0103 0.0004 0.0002	Ca2X 8498 Ca2X 8542 Ca2Z 8562 CaF1 7291 CaF2 7324 Rec 3933 Ca 4 32 Ca 5 5311	3.695 3.609 3.601 3.047 2.898 2.316 1.876 1.882	0.0123 0.0121 0.0034 0.0024 0.0006
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861 Strk18751 Strk40512 Dest 1216	6.274 5.513 5.353 3.718 4.908 3.851 3.668 2.749 5.544	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 R 977	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3343	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093	0.1208 0.1208 0.0103 0.0004 0.0002 0.0198 0.0198 0.0061 0.0037	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5311 Ca 5 2414	3.695 3.609 3.601 3.047 2.898 2.316 1.876 1.876 1.82 1.605	0.0123 0.0121 0.0034 0.0024 0.0006
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563 Strk 4861 Strk40512 Dest 1216 Dest 6563	6.274 5.513 5.353 3.718 4.908 3.851 3.668 2.749 5.544 4.121	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 TOTL 1909	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 1.0903 0.9348 0.1555 7.1474	Ne 3 3869 Ne 3 3869 Ne 3 1818 Ne 3 156	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093 3.233	0.1208 0.1208 0.0103 0.0004 0.0002	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5311 Ca 5 2414 Fe 2 48	3.695 3.609 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534	0.0123 0.0121 0.0034 0.0024 0.0006
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861 Strk18751 Strk40512 Dest 1216	6.274 5.513 5.353 3.718 4.908 3.851 3.668 2.749 5.544	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 R 977	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3343	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093	0.1208 0.1208 0.0103 0.0004 0.0002 0.0198 0.0198 0.0061 0.0037	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5311 Ca 5 2414	3.695 3.609 3.601 3.047 2.898 2.316 1.876 1.876 1.82 1.605	0.0123 0.0121 0.0034 0.0024 0.0006
INND 6563 INND 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861	6.274 5.513 5.353 3.718 4.908 3.851 3.668 2.749 5.544 4.121 2.634	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 TOTL 1909 INWD 1909	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3346 Ne 3 3343 Ne 3 3343 Ne 3 1815	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093 3.233 2.497	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002	Ca2X 8498 Ca2Y 8542 Ca2Z 8562 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5414 Fe 2 48 Fe 2 7	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0002 0.0001 1.0348 0.2311
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 nFnu 4860	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.851 3.668 2.749 5.544 4.121 2.634 6.143	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0399 0.0013 4.1985	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 TOTL 1909 INWD 1909 C 3 1907	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073 2.427	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 390 Ne 3 156	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093 3.233 2.497 3.113	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.00198 0.0061 0.0037 0.0052 0.0009 0.0039	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3	3.695 3.601 3.047 2.898 2.316 1.876 1.876 1.882 1.605 5.534 4.883 5.692	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872
INND 6563 INND 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 1216 Dest 4861 nFnu 4860 nFnu 1215	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.634 6.143 5.217	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0017 1.0593 0.0013 4.1985 0.4987	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907	5.187 5.082 4.698 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.374	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 156	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093 3.233 2.497 3.113 2.778	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0018	Ca2X 8498 Ca2X 8542 Ca2Z 8562 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5311 Ca 5 5414 Fe 2 7 Emis 3 Cool 3	3.695 3.601 3.601 3.047 2.316 2.316 1.882 1.605 5.534 4.883 5.692 5.692	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563 Strk 4861 Strk40512 Dest 6263 Dest 6263 Dest 6263 Dest 4861 nFnu 4860 nFnu 1215 Inci 4861	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.8668 2.749 5.544 4.121 2.634 6.143 5.217 6.959	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0013 4.1985 0.4987 27.5214	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 C 2 4267 C 2 4267 C 3 C 977 C 3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1909 C 3 1909	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.374 4.304	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3869 Ne 3 3343 Ne 3 1815 Ne 4 4720 Ne 5 3426 Ne 5 3426	4.601 4.601 3.533 2.096 1.746 3.303 3.093 3.233 2.497 3.113 2.778 2.345	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0003 0.0037 0.0052 0.0009 0.0039 0.0018 0.0007	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.699 5.960	0.0123 0.0121 0.0034 0.0002 0.0006 0.0000 0.0000 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 4861 nFnu 4860 nFnu 4861 Inci 4861 Inci 1216	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.634 6.143 5.217 6.959 7.240	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0017 1.0593 0.0399 0.0013 4.1985 0.4987 27.5214	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1909 C 3 1909 C 3 R 1909 Phot 1909	5.187 5.082 4.698 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.374 4.304	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.9348 0.1555 7.1474 3.5804 0.0008 7.1465 0.0609 0.0424	Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 4 4720 Ne 4 1602 Ne 5 3346 Ne 5 3346 Ne 5 2976	4.601 4.601 3.533 2.096 1.746 3.303 3.093 3.233 2.497 3.113 2.778 2.345 1.717	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0018 0.0052 0.0052 0.0039 0.0018 0.0007	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FET 0	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.534 4.883 5.699 5.699 5.669	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 nFnu 4860 nFnu 1215 Inci 4861 Inci 1216 BA C 0	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.544 4.6143 5.217 6.959 7.240 6.255	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.017 1.0593 0.0013 4.1985 0.04987 27.5214 5.2434	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1909 Phot 1909 C 3 2297	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.074 4.304 4.304 4.147	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 3343 Ne 3 1815 Ne 4 1602 Ne 5 3346 Ne 5 2976 Ne 5 1575	4.601 4.601 3.533 2.096 1.746 3.303 3.093 3.237 2.497 3.113 2.497 3.113 2.778 2.345 1.717 2.193	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0018 0.0018 0.0007 0.0002 0.0002	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FEIR 0 Fe 3 0	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.692 5.960 2.467 3.072	0.0123 0.0121 0.0034 0.0024 0.0006 0.0000 0.0000 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 4861 nFnu 1215 Inci 4861 Inci 1216 BA C 0 PA C 0	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.634 4.121 2.634 6.143 5.217 6.959 7.240 6.255 5.775	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0017 1.0593 0.0399 0.0013 4.1985 0.4987 27.5214 52.5214 5.25214 5.4231 1.8029	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1909 Phot 1909 C 3 2297 C 3 2297	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.374 4.304 4.147 4.147 4.194	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 4 4720 Ne 4 4720 Ne 4 1602 Ne 5 3426 Ne 5 3426 Ne 5 1575 Ne 5 1134	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.033 3.233 2.497 3.113 2.778 2.345 1.717 2.193 3.342	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0037 0.0052 0.0039 0.0039 0.0039 0.0039 0.0032 0.0005 0.0005 0.0005 0.0005	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5311 Ca 5 5214 Fe 2 7 Emis 3 Cool 3 TOT 0 FEIR 0 Fe 3 0 Fe 3 5270	3.695 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.534 4.883 5.532 5.699 5.960 2.467 3.072 2.392	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007
INND 6563 INND 4861 INND18751 Strk 1216 Strk 6563 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 nFnu 4860 nFnu 1215 Inci 4861 Inci 1216 BA C 0	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.544 4.6143 5.217 6.959 7.240 6.255	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.017 1.0593 0.0013 4.1985 0.04987 27.5214 5.2434	TOTL 977 C3 C 977 TOTL 977 C3 C 977 C3 C 977 C3 C 977 TOTL 1909 C 3 1909 C 3 1909 C3 R 1909 C3 R 1909 C 3 2297 C 3 4187 C 3 4649	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 4.304 4.304 4.147 4.194 2.336 3.138	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 3343 Ne 3 1815 Ne 4 1602 Ne 5 3346 Ne 5 2976 Ne 5 1575	4.601 4.601 3.533 2.096 1.746 3.303 3.093 3.237 2.497 3.113 2.497 3.113 2.778 2.345 1.717 2.193	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0009 0.0018 0.0007 0.0002 0.0005 0.0005 0.0005 0.0005 0.0006 0.0001	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FEIR 0 Fe 3 0	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.692 5.960 2.467 3.072	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 4861 nFnu 1215 Inci 4861 Inci 1216 BA C 0 PA C 0	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.634 4.121 2.634 6.143 5.217 6.959 7.240 6.255 5.775	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0017 1.0593 0.0399 0.0013 4.1985 0.4987 27.5214 52.5214 5.25214 5.4231 1.8029	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1909 Phot 1909 C 3 2297 C 3 2297	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.374 4.304 4.147 4.147 4.194	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 4 4720 Ne 4 4720 Ne 4 1602 Ne 5 3426 Ne 5 3426 Ne 5 1575 Ne 5 1134	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.033 3.233 2.497 3.113 2.778 2.345 1.717 2.193 3.342	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0037 0.0052 0.0039 0.0039 0.0039 0.0039 0.0032 0.0005 0.0005 0.0005 0.0005	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 5311 Ca 5 5214 Fe 2 7 Emis 3 Cool 3 TOT 0 FEIR 0 Fe 3 0 Fe 3 5270	3.695 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.534 4.883 5.532 5.699 5.960 2.467 3.072 2.392	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563 Strk 4861 Strk4861 Strk40512 Dest 6563 Dest 6563 Dest 4861 nFnu 4860 nFnu 1215 Inci 1216 BA C 0 PA C 0 H FF 0 H FF 0	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.634 4.121 2.634 4.121 2.634 5.547 6.143 5.217 6.959 7.240 6.255 5.775 6.021 6.091	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0013 4.1985 0.4987 27.5214 52.5214 5.434 1.8029 3.1744 3.7173	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1909 Phot 1909 C 3 2297 C 3 4187 C 3 4649 C 4 549	5.187 5.082 4.698 4.639 2.931 5.557 5.450 4.711 6.374 4.374 5.457 6.374 4.374	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 3 3869 Ne 3 3969 Ne 3 3969 Ne 3 3968 Ne 3 343 Ne 3 1815 Ne 4 1602 Ne 5 3426 Ne 5 3426 Ne 5 3426 Ne 5 1575 Ne 5 1134 Ne 6 1007 Emis 2798	4.601 4.601 1.746 1.746 3.816 3.093 3.093 3.233 2.497 3.113 2.345 1.717 2.342 1.665 2.795	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0018 0.0037 0.0052 0.0039 0.0039 0.0039 0.0039 0.0039 0.0002 0.0005 0.0006 0.0005 0.0006 0.0005	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 2414 Fe 2 48 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FETR 0 FETR 0 Fe 3 5270 Fe 3 5270 Fe 3 4658 Fe 3 1122	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.969 2.467 3.072 2.392 2.392 2.636	0.0123 0.0121 0.0034 0.0002 0.0006 0.0000 0.0000 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092
INND 6563 INND 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 Inci 4861 Inci 4861 Inci 4861 Inci 4216 BA C 0 PA C 0 H FF 0 C C 1216	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.851 3.851 2.749 5.544 4.121 2.634 6.143 5.217 6.959 7.240 6.255 5.775 6.021 6.090 6.323	$\begin{array}{c} 5,6798\\ 0,9849\\ 0,6809\\ 0,0158\\ 0,2445\\ 0,0215\\ \end{array}$	TOTL 977 C3 C 977 C3 C 977 C3 C 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 C 3 1909 C 3 1909 C 3 1909 C 3 1909 C 3 1909 C 3 2297 C 3 4649 C 3 4649 C 4 1549 INWD 1549	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.073 2.427 6.374 4.304 4.147 4.194 2.336 6.3138 6.759	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.9348 0.1555 7.1474 3.5804 0.0008 7.1465 0.0609 0.0424 0.0473 0.0042 18.6806 10.9493	Ne 3 3869 Ne 3 3869 Ne 3 3869 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 4 4720 Ne 4 4720 Ne 4 4720 Ne 5 3426 Ne 5 3426 Ne 5 1575 Ne 5 1575 Ne 5 1134 Ne 6 1007 Emis 2798	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093 3.233 2.497 3.113 2.778 2.345 1.717 2.193 3.342 2.778 2.345 1.717 2.193	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0005 00	Ca2X 8498 Ca2X 8542 Ca2I 8562 CaP1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 CaF2 7324 Ca 5 5311 Ca 5 5414 Fe 2 7 Emis 3 Cool 3 TOT 0 Fe 3 0 Fe 3 5270 Fe 3 4658 Fe 3 1122 Fe 5 3892	3.695 3.609 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.692 5.692 5.692 2.467 3.072 2.396 3.485 2.345	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007
INWD 6563 INWD 4861 INWD18751 Strk 1216 Strk 6563 Strk 4861 Strk40512 Dest 6563 Dest 6563 Dest 6563 Dest 4861 InFnu 4860 nFnu 1215 Inci 4861 Inci 1216 BA C 00 H FF 0 C Col 1216 Heat 1216	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.668 2.749 5.544 4.121 2.634 4.121 2.634 4.915 5.547 6.959 7.240 6.255 5.775 6.021 6.090 6.323 4.976	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0017 1.0593 0.0013 4.1985 0.4987 27.5214 5.2434 1.8029 3.1744 3.7173 6.3662 0.2863	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1909 Phot 1909 C 3 1909 Phot 1909 C 3 2297 C 3 4187 C 3 4649 C 4 1549 INWD 1549 DEST 1549	5.187 5.082 2.931 5.557 5.400 4.711 6.374 6.374 4.304 4.147 4.147 4.194 2.336 3.136 6.791 6.5551	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 2 128 Ne 2 128 Ne 2 128 Ne 3 156 Ne 3 3869 Ne 3 3968 Ne 3 3343 Ne 3 1815 Ne 4 4720 Ne 5 3346 Ne 5 3346 Ne 5 3346 Ne 5 1575 Ne 5 1134 Ne 5 1575 Ne 5 1134 Ne 6 1007 Emis 2798 Ccol 2798	4.601 3.533 2.096 1.746 3.303 3.093 3.233 2.437 3.113 2.345 1.717 2.345 1.717 2.193 3.342 1.6279 6.279 6.293 2.229	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0003 0.0037 0.0052 0.0009 0.0018 0.0007 0.0002 0.0005 0.0005	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca 5 5311 Ca 5 2414 Fe 2 48 Fe 2 77 Emis 3 Cool 3 TOT 0 FEIR 0 FEIR 0 FEIR 0 FEIR 0 FE 3 207 FE 3 4658 Fe 3 1122 Fe 5 3892 Fe 5 0892	3.695 3.601 3.047 2.898 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.699 2.467 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.407 2.408 2.407 2.408 2.407 2.408 2.409 2.407 2.409 2.407 2.409 2.407 2.409 2.407	0.0123 0.0121 0.0034 0.0002 0.0006 0.0000 0.0000 1.0348 0.2311 1.4872 1.5113 2.7582 0.0036 0.0007 0.00036 0.0007 0.0013 0.00092 0.0007
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 4861 nFnu 4860 nFnu 1215 Inci 4861 Inci 1216 BA C 0 PA C 0 PA C 0 H FF 0 H FB 0 Cool 1216 Heat 1216 Crst 960	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.851 3.851 2.634 4.121 2.634 6.143 5.217 7.240 6.255 5.7755 6.0910 6.323 4.976 4.033	$\begin{array}{c} \text{S}, 6798\\ \text{O}, 9849\\ \text{O}, 6809\\ \text{O}, 0158\\ \text{O}, 2445\\ \text{O}, 0215\\ \end{array}$	TOTL 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1909 C 3 1909 C 3 1909 C 3 1909 C 3 1909 C 3 2297 C 3 4187 C 3 4187 C 3 4187 C 3 4187 C 3 4187 C 3 4549 INWD 1549 DEST 1549 DEST 1549	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 4.307 4.714 6.374 4.147 4.147 4.147 4.147 4.147 4.143 6.559 4.311 3.266	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0028 0.	Ne 3 3869 Ne 3 3869 Ne 3 156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 4 4720 Ne 4 4720 Ne 4 4720 Ne 5 3346 Ne 5 1575 Ne 5 1575 Ne 5 1134 Ne 6 1007 Emis 2798 Cool 2798 Mg 4 4 Mg 5 56	4.601 4.601 3.533 2.096 1.746 3.816 3.303 3.093 2.233 2.497 3.113 2.778 2.345 2.345 5.6279 6.293 2.229 1.874	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0018 0.0061 0.0037 0.0052 0.0003 0.0018 0.0007 0.0002 0.0005 0.00066 0.0001 5.7519 5.9340 0.00052	Ca2X 8498 Ca2Z 8542 Ca2Z 8562 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 2414 Fe 2 7 Emis 3 Cool 3 TOT 0 FE3 0 Fe 3 5270 Fe 3 5270 Fe 3 4658 Fe 3 1122 Fe 6 0 Fe 6 5177	3.695 3.609 3.601 3.047 2.898 2.316 1.822 1.605 5.534 4.883 5.692 5.6592 5.692 5.692 2.467 3.072 2.463 3.485 3.027 2.576	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007
INND 6563 INND 4861 INND 4861 Strk 1216 Strk 5563 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 Inci 4861 Inci 4861 Inci 4861 Inci 4861 Inci 4861 Inci 4861 Inci 4861 Inci 4861 Inci 1216 BA C 00 FA C 0 H FF 0 Cool 1216 Heat 1216 Crst 960 Cool 6563	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.851 4.908 3.851 3.851 4.908 3.851 4.908 3.851 4.908 5.544 4.121 2.749 5.544 4.6143 5.217 6.959 7.240 6.255 5.775 6.021 6.090 6.323 4.976 4.033 5.544	$\begin{array}{c} 5.6798\\ 0.9849\\ 0.6809\\ 0.0158\\ 0.2445\\ 0.0215\\ \end{array}$	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1909 Phot 1909 Phot 1909 Phot 1909 C 3 2297 C 3 4187 C 3 4649 C 4 1549 DEST 1549 C 4 4659	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.374 4.147 4.147 4.147 4.147 4.147 4.194 2.336 3.74 4.519 2.555 5.557 5.457 6.4711 4.4711 4.434 4.147 4.457 4.459 2.555 7.557 5.4575 5.4575 5.4575 5.4575 5.4575 5.4575 5.4575 5.45755 5.45755 5.4575557 5.457557 5.457557557 5.4575575575575575575575575575575575575575	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026	Ne 3 3869 Ne 2 1218 Ne 2 128 Ne 2 128 Ne 2 128 Ne 3 156 Ne 3 3869 Ne 3 3343 Ne 3 1815 Ne 4 1602 Ne 5 3426 Ne 5 3426 Ne 5 1575 Ne 5 1134 Ne 6 1007 Emis 2798 Cool 2798 Mg 4 4 Mg 5 5 2751	4.601 3.533 2.096 1.746 3.003 3.093 3.093 3.233 2.497 2.345 1.717 2.193 3.342 1.665 6.279 6.279 6.279 2.229 1.874	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0018 0.0018 0.0001 0.0005 0.0005 0.0001 5.7519 5.9340 0.0005 0.0002 0.0005 0.0002	Ca2X 8498 Ca2Y 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FEIR 0 FEIR 0 FE 3 5270 Fe 3 122 Fe 5 3892 Fe 6 177 Fe 7 6087	3.695 3.601 3.047 2.898 2.316 2.316 1.876 1.882 1.605 5.534 4.883 5.699 5.699 5.699 5.960 2.467 3.072 2.392 2.636 3.485 2.632 3.027 2.578	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0036 0.0007 0.0013 0.0092 0.0001 0.00013 0.0092 0.0001 0.0002
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk 4861 Dest 1216 Dest 1216 Dest 1216 Dest 4861 nFnu 4860 nfru 1215 Inci 4861 Inci 1216 BA C 0 PA C 0 H FF 0 H FF 0 H FF 0 H est 1216 Cool 1216 Heat 1216 Crst 960 Cool 6563 Crst 4861	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.851 3.851 2.634 4.121 2.634 4.121 2.634 4.121 2.634 5.217 6.959 7.240 6.255 5.756 6.021 6.323 4.976 4.033 5.546 4.033	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0017 1.0593 0.0017 1.0593 0.0399 0.0013 4.1985 0.4987 27.5214 52.5214 5.4434 1.8029 3.1744 3.7173 6.3662 0.0327 1.0640 0.1367	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1909 C 3 1909 C 3 1909 C 3 1909 C 3 2297 C 3 4187 C 3 4649 C 4 1549 INWD 1549 DEST 1549 DEST 1549 DC 4 7549 C 4 26584	$\begin{array}{c} 5.187\\ 5.082\\ 4.698\\ 4.639\\ 2.931\\ \end{array}$	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0027 0.00424 0.00424 0.00473 0.00042 0.00424 0.00424 0.00424 0.0007 0.00424 0.00619 0.0056 0.00016	Ne 3 3869 Ne 3 3869 Ne 3 156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 4 4720 Ne 4 4720 Ne 4 4720 Ne 5 3426 Ne 5 3426 Ne 5 3426 Ne 5 1134 Ne 6 1007 Emis 2798 Cool 2798 Mg 4 4 S 556 Mg 5 56 Mg 5 2751 Al 3 1860	4.601 4.601 1.746 1.746 3.816 3.096 1.746 3.093 3.233 2.497 3.113 2.778 2.345 1.717 2.193 3.342 1.665 6.279 6.293 2.229 1.874 2.629	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0003 0.0037 0.0052 0.0003 0.0003 0.0003 0.0005 00	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Tot1 2	3.605 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.659 5.954 4.883 5.699 5.960 2.467 3.072 2.325 2.345 3.027 2.576 2.288 4.349	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007 0.0032 0.0001 0.0005
INND 6563 INND 4861 INND18751 Strk 1216 Strk 5563 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 Inci 4861 Inci 4861 Inci 1216 BA C 00 H FF 0 CC01 1216 Crst 960 Ccol 6563 Crst 4861 CC018751	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.851 3.851 3.851 4.909 5.544 4.121 2.749 5.544 4.121 2.55 5.775 6.959 7.240 6.255 5.775 6.021 6.090 6.323 4.976 4.909 5.546 4.655 4.220	$\begin{array}{c} 5.6798\\ 0.9849\\ 0.6809\\ 0.0158\\ 0.2445\\ 0.0215\\ \end{array}$	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 C 2 4267 C 3 2 4267 C 3 977 C 3 C 977 C 3 C 977 C 3 R 977 TOTL 1909 C 3 2297 C 3 4649 C 4 1549 DEST 1549 C 4 4659 N 2 6548 N 2 6548	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.374 4.147 4.147 4.304 4.147 4.304 4.147 4.338 6.791 6.559 4.511 1.654 1.654 1.941 1.941	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0028 0.1555 7.1474 0.0008 0.0424 0.0473 0.0007 0.0042 18.6806 10.9493 0.0619 0.0056 0.0001 0.0008 0.0005	Ne 3 3869 Ne 3 3869 Ne 3 3869 Ne 3 3156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3343 Ne 4 1602 Ne 5 3426 Ne 5 1575 Ne 5 1275 Ne 5 127	4.601 3.533 2.096 1.746 3.816 3.093 3.233 2.497 3.113 2.778 2.345 1.717 3.342 1.665 6.279 3.229 1.665 6.229 2.229 1.664 4.864 5.126 4.864 5.126 4.864	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0018 0.0007 0.0002 0.0005 0.0001 5.7519 5.9340 0.0001 5.9340 0.0002 0.0002 0.0002 0.0014 0.4013 0.2219	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Tot1 2	3.695 3.601 3.047 2.898 2.316 2.316 1.876 1.882 1.605 5.534 4.883 5.692 5.699 5.960 2.467 3.072 2.392 2.636 3.485 2.485 3.027 2.578	0.0123 0.0121 0.0034 0.0024 0.0006 0.0002 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0036 0.0007 0.0013 0.0092 0.0001 0.00013 0.0092 0.0001 0.0002
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 6563 Strk 4861 Strk 4861 Strk 40512 Dest 1216 Dest 4861 nFnu 1215 Inci 4861 Inci 1216 BA C 0 PA C 0 H FF 0 H FF 0 H FF 0 H FF 0 Ccol 1216 Heat 1216 Crst 960 Ccol 6563 Crst 4861 Ccol18751 Crst 0	6.274 5.513 5.353 3.718 4.908 3.851 3.851 3.851 3.851 2.749 5.544 4.121 2.634 6.255 5.775 6.021 6.959 7.240 6.255 5.775 6.021 6.033 5.546 4.033 5.546 4.033 5.546 4.220 3.373	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0215 0.0017 1.0593 0.0039 0.0013 4.1985 0.4987 27.5214 52.5215 52.5255 52.525555555555	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 TOTL 977 C3 C 977 C3 C 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 2297 C 3 4187 C 3 4187 C 3 4649 DEST 1549 C 4 1549 DEST 1549 C 4 25755	$\begin{array}{c} 5.187\\ 5.082\\ 4.698\\ 4.639\\ 2.931\\ \end{array}$	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.026 0.026 0.026 0.026 0.038 0.9348 0.1555 7.1474 3.5804 0.0008 7.1465 0.0609 0.0424 0.0473 0.0042 0.0473 0.0042 0.00424 0.0007 0.00424 0.0007 0.00424 0.0007 0.00424 0.0005 0.0001 0.0008	Ne 3 3869 Ne 3 3869 Ne 3 156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 4 4720 Ne 4 4720 Ne 4 4720 Ne 4 1602 Ne 5 3426 Ne 5 3426 Ne 5 3426 Ne 5 1134 Ne 6 1007 Ne 6 1007 Ne 6 1007 Ne 5 1134 Ne 6 1007 Si 2 2751 Al 3 1860 Si 2 2335 Si 2 1808	4.601 4.601 1.746 1.746 3.533 2.096 1.746 3.093 3.093 3.023 2.497 3.113 2.778 2.345 1.717 2.342 1.665 6.279 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.2933 2.29355 2.29355 2.29355555555555555555555555555555555555	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0002 0.0004 0.0005 0.0002	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Tot1 2	3.605 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.659 5.954 4.883 5.699 5.960 2.467 3.072 2.325 2.345 3.027 2.576 2.288 4.349	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007 0.0032 0.0001 0.0005
INND 6563 INND 4861 INND18751 Strk 1216 Strk 5563 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 Inci 4861 Inci 4861 Inci 1216 BA C 00 H FF 0 CC01 1216 Crst 960 Ccol 6563 Crst 4861 CC018751	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.851 3.851 3.851 4.908 3.851 4.908 3.851 4.908 5.544 4.6143 5.217 6.959 7.240 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.021 6.095 6.255 5.775 6.025 7.757 6.095 7.757 6.095 7.7577 7.7577 7.75777 7.757777 7.7577777777	$\begin{array}{c} 5.6798\\ 0.9849\\ 0.6809\\ 0.0158\\ 0.2445\\ 0.0215\\ \end{array}$	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 C 2 4267 C 3 2 4267 C 3 977 C 3 C 977 C 3 C 977 C 3 R 977 TOTL 1909 C 3 2297 C 3 4649 C 4 1549 DEST 1549 C 4 4659 N 2 6548 N 2 6548	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.073 2.427 6.374 4.147 4.147 4.304 4.147 4.304 4.147 4.338 6.791 6.559 4.511 1.654 1.654 1.941 1.941	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0028 0.1555 7.1474 0.0008 0.0424 0.0473 0.0007 0.0042 18.6806 10.9493 0.0619 0.0056 0.0001 0.0008 0.0005	Ne 3 3869 Ne 3 3869 Ne 3 3869 Ne 3 3156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3343 Ne 4 1602 Ne 5 3426 Ne 5 1575 Ne 5 1275 Ne 5 127	4.601 3.533 2.096 1.746 3.816 3.093 3.233 2.497 3.113 2.778 2.345 1.717 3.342 1.665 6.279 3.229 1.665 6.229 2.229 1.664 4.864 5.126 4.864 5.126 4.864	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0018 0.0007 0.0002 0.0005 0.0001 5.7519 5.9340 0.0001 5.9340 0.0002 0.0002 0.0002 0.0014 0.4013 0.2219	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Tot1 2	3.605 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.659 5.954 4.883 5.699 5.960 2.467 3.072 2.325 2.345 3.027 2.576 2.288 4.349	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007 0.0032 0.0001 0.0005
INVD 6563 INVD 4861 Strk 1216 Strk 1216 Strk 6563 Strk 4861 Strk 4861 Strk 40512 Dest 1216 Dest 4861 nFnu 1215 Inci 4861 Inci 1216 BA C 0 PA C 0 H FF 0 H FF 0 H FF 0 H FF 0 Ccol 1216 Heat 1216 Crst 960 Ccol 6563 Crst 4861 Ccol18751 Crst 0	6.274 5.513 3.353 3.718 4.908 3.851 3.955 3.975 4.805 3.373 4.805 3	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.0215 0.0017 1.0593 0.0399 0.0013 4.1985 0.4987 27.5214 52.5215 52.5255 52.525555555555	REC 1656 C 2 2326 INWD 2326 C 2 1335 REC 1335 C 2 4267 C 2 4267 C 2 4267 C 3 P77 C 3 C 977 C 3 R 977 TOTL 1909 C 3 2297 C 3 4649 C 4 1549 DEST 1549 DEST 1549 DEST 1548 N 2 6584 N 2 6584 N 2 6584 N 2 6584 N 2 6575 N 2 4239	$\begin{array}{c} 5.187\\ 5.082\\ 4.698\\ 4.639\\ 2.931\\ \end{array}$	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.026 0.026 0.026 0.026 0.038 0.9348 0.1555 7.1474 3.5804 0.0008 7.1465 0.0609 0.0424 0.0473 0.0042 0.0473 0.0042 0.00424 0.0007 0.00424 0.0007 0.00424 0.0007 0.00424 0.0005 0.0001 0.0008	Ne 3 3869 Ne 3 3869 Ne 3 156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 4 4720 Ne 4 4720 Ne 4 4720 Ne 4 1602 Ne 5 3426 Ne 5 3426 Ne 5 3426 Ne 5 1134 Ne 6 1007 Ne 6 1007 Ne 6 1007 Ne 5 1134 Ne 6 1007 Si 2 2751 Al 3 1860 Si 2 2335 Si 2 1808	4.601 4.601 1.746 1.746 3.533 2.096 1.746 3.093 3.093 3.023 2.497 3.113 2.778 2.345 1.717 2.342 1.665 6.279 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.229 1.874 2.6293 2.2933 2.29355 2.29355 2.29355555555555555555555555555555555555	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0009 0.0018 0.0007 0.0005 0.0005 0.0005 0.0005 0.0001 5.7519 5.9340 0.0005 00	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Tot1 2	3.605 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.659 5.954 4.883 5.699 5.960 2.467 3.072 2.325 2.345 3.027 2.576 2.288 4.349	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007 0.0032 0.0001 0.0005
INND 6563 INND 4861 INND 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk40512 Dest 1216 Dest 6563 Dest 4861 nFnu 4860 nFnu 1215 Inci 4861 Inci 1216 BA C 00 H FB 0 Cool 1216 Heat 1216 Crst 960 Cool 6563 Crst 4861 Cool18751 Crst 00 H-FB 0 H-FB 0 H-FB 0 H-FB 0	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.851 3.851 3.851 4.908 3.851 5.544 4.121 2.749 5.544 4.121 2.544 4.121 5.217 6.959 7.240 6.255 5.775 6.021 6.090 6.255 5.775 6.021 6.090 6.253 5.546 4.655 3.544 4.655 3.5748 4.855 4.805 4.455	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.017 1.0593 0.0017 1.0593 0.0013 4.1985 0.04987 27.5214 5.25214 5.25214 5.4434 1.8029 3.1744 3.7173 6.3662 0.0327 1.0640 0.1367 0.0572 0.0071 0.0572 0.0071 0.1928 0.0858	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 1909 Phot 1909 Phot 1909 C 3 2297 C 3 4649 C 4 1549 INWD 1549 DEST 1549 C 4 4659 N 2 6584 N 2 5755 N 2 4239 N 2 5680	$\begin{array}{c} 5.187\\ 5.082\\ 4.698\\ 4.639\\ 2.931\\ \end{array}$	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.1555 7.1474 3.5804 0.0008 0.0424 0.0473 0.0042 18.6806 10.0473 0.0042 18.6806 0.0042 0.0042 0.0042 0.0056 0.0005 0.0005 0.0003 0.0013 0.0004	Ne 3 3869 Ne 3 3869 Ne 3 156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 3 3946 Ne 4 1602 Ne 5 3426 Ne 5 1575 Ne 5 12798 Mg 4 4 Mg 5 56 Mg 5 2751 Al 3 1860 Si 2 2335 Si 2 1808 Si 3 1207	4.601 4.601 3.533 2.096 1.746 1.746 3.816 3.093 3.233 2.497 3.113 2.497 3.113 2.497 3.145 1.7193 3.345 1.7193 3.345 1.7193 3.345 1.2793 2.299 1.874 4.866 5.295 5.096	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0002 0.0004 0.0005 0.0002	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Tot1 2	3.605 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.659 5.954 4.883 5.699 5.960 2.467 3.072 2.325 2.345 3.027 2.576 2.288 4.349	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007 0.0032 0.0001 0.0005
INND 6563 INND 4861 Strk 1216 Strk 1216 Strk 4861 Strk 4861 Strk 4861 Strk 4861 Dest 6563 Dest 4861 nFnu 4860 nFnu 1215 Inci 4861 Inci 1216 BA C 0 PA C 0 H FF 0 Cool 1216 Heat 1216 Crst 960 Cool 6563 Crst 4861 Cool18751 Crst 0 H FF 0	6.274 5.513 3.353 3.718 4.908 3.851 3.851 3.851 3.851 3.851 4.908 3.851 5.544 4.121 2.749 5.544 4.121 2.544 4.121 5.217 6.959 7.240 6.255 5.775 6.021 6.090 6.255 5.775 6.021 6.090 6.253 5.546 4.655 3.544 4.655 3.5748 4.855 4.805 4.455	5.6798 0.9849 0.6809 0.0158 0.2445 0.0215 0.0215 0.0215 0.017 1.0593 0.0017 1.0593 0.0013 4.1985 0.04987 27.5214 5.25214 5.25214 5.4434 1.8029 3.1744 3.7173 6.3662 0.0327 1.0640 0.1367 0.0572 0.0071 0.0572 0.0071 0.1928 0.0858	REC 1656 C 2 2326 INWD 2326 C 2 1335 C 2 1335 C 2 4267 TOTL 977 C3 C 977 C3 R 977 TOTL 1909 INWD 1909 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 1907 C 3 1909 Phot 1909 Phot 1909 C 3 2297 C 3 4649 C 4 1549 INWD 1549 DEST 1549 C 4 4659 N 2 6584 N 2 5755 N 2 4239 N 2 5680	5.187 5.082 4.698 4.639 2.931 5.557 5.490 4.711 6.374 6.374 4.147 4.147 4.147 4.194 2.336 3.1266 1.237 6.3791 6.559 4.311 3.266 1.2659 4.311 3.266 1.2659 2.077 2.585	0.0450 0.4656 0.3655 0.1507 0.1318 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.1555 7.1474 3.5804 0.0008 0.0424 0.0473 0.0042 18.6806 10.0473 0.0042 18.6806 0.0042 0.0042 0.0042 0.0056 0.0005 0.0005 0.0003 0.0013 0.0004	Ne 3 3869 Ne 3 3869 Ne 3 156 Ne 2 128 Ne 3 156 Ne 3 3968 Ne 3 3968 Ne 3 3968 Ne 3 3946 Ne 3 3946 Ne 4 1602 Ne 5 3426 Ne 5 1575 Ne 5 12798 Mg 4 4 Mg 5 56 Mg 5 2751 Al 3 1860 Si 2 2335 Si 2 1808 Si 3 1207	4.601 4.601 3.533 2.096 1.746 1.746 3.816 3.093 3.233 2.497 3.113 2.497 3.113 2.497 3.145 1.7193 3.345 1.7193 3.345 1.7193 3.345 1.2793 2.299 1.874 4.866 5.295 5.096	0.1208 0.1208 0.0103 0.0004 0.0002 0.0002 0.0002 0.0005 0.0009 0.0018 0.0007 0.0005 0.0005 0.0005 0.0005 0.0001 5.7519 5.9340 0.0005 00	Ca2X 8498 Ca2Z 8542 Ca2Z 8662 CaF1 7291 CaF2 7324 Rec 3933 CaF2 7324 Rec 3933 Ca5 5311 Ca 5 5311 Ca 5 5311 Ca 5 5211 Ca 5 2414 Fe 2 48 Fe 2 7 Emis 3 Cool 3 TOT 0 FE 3 0 FE 3 0 FE 3 0 FE 3 0 FE 3 4658 Fe 3 5270 Fe 3 3892 Fe 6 0 Fe 5 3892 Fe 6 5087 Fe 7 6087 Totl 2	3.605 3.609 3.601 3.047 2.898 2.316 1.882 1.605 5.534 4.883 5.659 5.954 4.883 5.699 5.960 2.467 3.072 2.325 2.345 3.027 2.576 2.288	0.0123 0.0121 0.0034 0.0024 0.0006 0.0006 0.0002 0.0001 1.0348 0.2311 1.4872 1.5113 2.7582 0.0009 0.0036 0.0007 0.0013 0.0092 0.0007 0.0032 0.0001 0.0005

Cooling: H FB 0:0.055 Cool 1216:0.095 TOTL 1909:0.107 C 4 1549:0.278 Emis 2798:0.086 Cool 2798:0.088 Heating: BFH1 0:0.637 BFHe 0:0.254 TotM 0:0.094
IONIZE PARMET: U(1-) -1.9996 U(4-): -2.9403 U(sp): -2.85 Q(ion): 14.360 L(ion): 7.036 Q(low): 19.81 P(low) 7.69 ENERGY BUDGET: Heat: 7.346 Coolg: 7.346 Error: 0.0% Compt H: 3.203 WorkF: 9.805 F-F H 3.057 PRADMX:4.67E-01 Column density H12:1.001E+23 H II:2.211E+21 HI:9.791E+22 H-: 1.531E+14 H2: 1.113E+17 H2+:4.485E+14 He H+:2.544E+14 OH: 0.000E+00 Heff:1.066E+23
<pre></pre>
Mean Jeans l(cm)1.87E+16 M(sun)8.89E+01 smallest: len(cm):1.79E+16 M(sun):7.79E+01 Alf(ox-tran): -2.2323
Optical Depths: CONTN; COMT: 1.64E-03 H-: 5.97E-03 R(1300): 6.57E-01 H2+ 3.14E-03 Herri: 3.42E-02 Pfa:1.65E-03 Pa:1.64E-03 Ba:7.33E-03 Hb:6.07E-03 La:1.62E+01 1r:6.162E+05 1.8:1.92E+05 4.2:2.953E+04 21r:3.331E+02 10830: 4.85E+02 3889: 2.12E+01 5876: 2.20E+01 7065: 1.21E+01 1r:6.162E+05 1.8:1.92E+05 4.2:2.953E+04 21r:3.331E+02 1550: 2.05E+04 2800: 6.55E+06 774: 1.00E-20 1240: 2.26E+02 1035: 6.55E+01 1335: 6.34E+06 977: 7.70E+04 1397: 9.88E+03 789: 2.87E+03 1207: 1.85E+04 1085: 7.06E+04 1194: 1.33E+02 1909: 3.07E-02 1895: 4.94E+01 226: 3.17E+01 166: 3.51E-01 1750: 1.16E-03 1205: 9.94E+05 352: 1.40E-03 347: 1.00E-20 1860: 4.14E+03 630: 2.44E+03 834: 1.25E+05 835: 1.70E+04 1808: 5.88E+06 1256: 9.21E+04 -33: 3.20E+05 -48: 2.49E+00 334: 1.14E+04 369: 5.76E+03 8498: 2.11E+01 8452: 1.18E+04 8662: 1.07E+02 353: 1.00E-20 1304: 3.40E+06 1122: 3.09E+02 990: 5.12E+03 1402: 3.83E-02 1214: 1.32E-02 1486: 1.76E-02 235: 1.40E+01
-245: 1.84E-04 765: 1.07E+04 -1198: 3.76E-02 786: 1.12E+02 C157: 2.74E-01 N122: 1.50E-02 N205: 2.02E-02 N57: 5.09E-04 0146: 7.33E-01 063: 2.21E+00 088: 3.94E-03 052: 6.64E-03 026: 1.50E-03 NE13: 4.56E-02 NE36: 3.89E-03 NE16: 1.25E-02 MG4: 5.37E-04 MG14: 8.84E-05 MG6: 5.22E-05 SI35: 1.87E-01 S19: 1.43E-03 S34: 6.88E-04 S11: 3.99E-04 AR7: 4.88E-03 AR9: 2.06E-04 AR22: 6.12E-05 AR13: 7.74E-06 AR8: 1.48E-05 CA3: 1.25E-04 CA12: 3.58E-06 CA4: 1.51E-05 NE14: 1.74E-04 Ne24: 8.67E-05 Si3: 6.35E-12 Si4: 1.28E-10 Fe7: 1.00E-20 Fe61: 1.00E-20 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 2.05E-06 Si6.5: 6.09E-07 C610: 5.97E-06 C370: 4.07E-06
Old hydro optical depths: 1 6.16E+05 2 7.05E-02 3 6.26E-03 4 1.67E-03 5 5.03E-06 6 9.06E-06 7 4.02E-05 Lines: 2-1 7.61E+09 3-2 3.00E+03 4-3 3.86E+01 5-4 2.48E+00 6-5 2.57E-01 7-6 4.72E-02 8-7 5.54E-01 New hydro optical depths: 1 6.16E+05 2 6.98E-02 3 6.38E-03 4 1.17E-03 5 7.27E-06 6 1.07E-05 7 4.49E-05 Lines: 2-1 7.62E+09 3-2 2.98E+03 4-3 3.66E+01 5-4 3.29E+00 6-5 5.11E-01 7-6 7.03E-02 8-7 6.62E-01
Old He Is optical depths: 1 1.92E+05 2 3.10E-02 3-8.41E-11 4-8.99E-10 5-1.87E-09 6-3.07E-09 7-2.10E-08 Lines: 2-1 4.77E+08 3-2 2.80E-02 4-3 1.68E-04 5-4 6.16E-05 6-5-2.54E-04 7-6 1.22E-03 8-7 1.96E-02 New HE Is optical depths: 1 1.92E+05 2 3.08E-02 3-8.62E-11 4-9.70E-10 5-2.01E-09 6-3.31E-09 7-2.24E-08 Lines: 2-1 4.78E+08 3-2 2.95E-02 4-3 1.84E-04 5-4 6.68E-05 6-5-2.81E-04 7-6 1.33E-03 8-7 2.14E-02
Old He II optical depths: 1 2.95E+04 2 6.16E+05 3-2.90E-10 4-8.94E-10 5-1.73E-09 6-2.89E-09 7-2.75E-08 Lines: 2-1 3.63E+06 3-2 1.87E-01 4-3 1.11E-05 5-4-1.93E-06 6-5-4.39E-05 7-6 1.15E-04 8-7 1.79E-03 New HE II optical depths: 1 2.95E+04 2 6.16E+05 3-2.65E-10 4-8.92E-10 5-1.74E-09 6-2.90E-09 7-2.75E-08 Lines: 2-1 3.89E+06 3-2 3.07E-01 4-3 1.43E-05 5-4-1.07E-06 6-5-4.32E-05 7-6 1.15E-04 8-7 1.80E-03
Hydrogen $-0.010 - 1.656$ Log10 Mean Ionisation (over volume)Helium $-0.008 - 1.812 - 2.685$ Carbon $-4.003 - 0.006 - 2.074 - 2.231 - 3.703 - 6.525$ Nitrogen $-0.095 - 0.740 - 2.078 - 2.253 - 3.512 - 4.423$ Oxygen $-0.009 - 2.155 - 1.905 - 2.813 - 3.625 - 4.798 - 6.254$ Neon $-0.025 - 1.454 - 1.733 - 2.809 - 3.252 - 4.558 - 6.994$ Magnesium $-3.396 - 0.033 - 1.155 - 2.753 - 3.373 - 3.955 - 5.209 - 7.205-11.702$ Aluminum $-4.351 - 0.006 - 2.306 - 2.111 - 3.208 - 3.869 - 5.108 - 7.010-11.906-14.081$ Silicon $-4.351 - 0.006 - 2.2306 - 2.130 - 2.822 - 3.633 - 4.873 - 6.611-10.944-13.682-15.956$ Sulphur $-4.607 - 0.009 - 1.882 - 2.249 - 3.172 - 3.501 - 4.473 - 6.617-10.013-12.618-14.872-17.789-20.219$ Argon $-0.029 - 1.295 - 2.125 - 2.185 - 3.220 - 3.633 - 4.633 - 5.536 - 6.6971$ Iron $-3.031 - 0.007 - 2.889 - 1.947 - 3.111 - 2.963 - 3.397 - 4.331 - 6.026 - 7.447$

"CONVENTIONAL" BLR MODEL

4 1 2 3 5 6 7 8 9 10 11 12 13 14 15 16 17 Hydrogen -0.010 -1.656 Log10 Mean Ionisation (over radius) Helium -0.008 -1.812 -2.685 Carbon -4.003 -0.006 -2.074 -2.231 -3.703 -6.525 Nitrogen -0.009 -2.155 -1.905 -2.813 -3.625 -4.798 -6.254 Neon -0.025 -1.454 -1.733 -2.809 -3.252 -4.558 -6.994 Magnesium -3.396 -0.033 -1.155 -2.753 -3.373 -3.955 -5.297 -7.205-11.702 Aluminum -4.325 -0.009 -1.900 -2.111 -3.208 -3.869 -5.108 -7.010-11.906-14.081 Silicon -4.351 -0.006 -2.306 -2.130 -2.822 -3.633 -4.873 -6.611-10.944-13.682-15.956 Sulphur -4.607 -0.009 -1.882 -2.249 -3.172 -3.501 -4.473 -6.178-10.013-12.618-14.872-17.789-20.219 Argon -0.029 -1.295 -2.125 -2.185 -3.220 -3.633 -4.873 -6.6191-10.514-12.829-15.677-18.208-21.247-23.875 Calcium -4.528 -1.644 -0.012 -2.445 -3.318 -3.513 -4.257 -5.360 -6.677 Iron -3.031 -0.007 -2.889 -1.947 -3.111 -2.963 -3.397 -4.331 -6.026 -7.447 0.5-1.0KEV:1.93E+02 1.0-1.5:2.52E+09 1.5-2.0:2.73E+11 2.0-2.5:2.04E+12 2.5-3:5.19E+12 3-5:3.53E+13 5-7.5:4.07E+13 7.5-10:2.54E+13 Normalised continuum 0.25 1.241 0.27 1.207 0.30 1.167 0.33 1.131 0.36 1.102 0.39 1.075 0.43 1.053 0.47 1.051 0.51 1.029 0.56 1.007 0.62 0.966 0.67 0.871 0.74 0.010 0.81 0.774 0.88 0.553 0.97 0.595 0.98 0.605 0.99 0.607 1.00 0.610 Inward continua (nuFnu) at head of Balmer, Lyman series: 3.23E+06 8.02E+06 Outwrd continua (nuFnu) at head of Balmer, Lyman series; 3.08E+06 0.00E+00

 Emergent continuum - phot/ryd/cm2 (r in)

 17.3 3.08-209 75.3 2.74E+03 1.26E+03 5.15E+10

 19.5 1.34-141 81.6 1.43E+05 1.88E+03 2.68E+10

 22.0 1.83-107 88.3 3.42E+06 2.79E+03 1.38E+10

 24.8 7.60E-71 95.7 4.34E+07 4.14E+03 7.04E+09

 27.9 2.69E+45 103.7 1.73E+08 6.16E+03 3.60E+09

 31.5 1.59E-30 112.3 9.97E+08 9.15E+03 1.49E+09

 35.5 1.99E-17 121.6 4.01E+09 1.36E+04 5.19E+08

 40.0 2.44E-27 131.7 1.21E+10 2.02E+04 1.81E+08

 45.0 3.81E-16 142.7 1.87E+10 3.00E+04 6.33E+07

 50.5 1.93E-08 173.9 9.13E+10 4.46E+04 2.21E+07

 54.7 7.05E-07 258.5 2.46E+11 9.86E+04 2.71E+06

 64.2 4.28E-02 571.2 1.52E+11 1.47E+05 9.46E+05

 69.5 1.98E+01 849.0 9.47E+10 2.18E+05 3.30E+05

 0.26 8.70E+18 1.00 0.00E+00 3.9 0.00E+00 3.24E+05 1.15E+05 0.29 6.93E+18 0.33 5.55E+18 0.37 4.48E+18 4.0 0.00E+00 4.2 0.00E+00 4.7 0.00E+00 5.3 0.00E+00 4.81E+05 4.01E+04 7.16E+05 1.40E+04 1.06E+06 4.86E+03 1.58E+06 1.69E+03 1.01 0.00E+00 1.02 0.00E+00 1.10 0.00E+00 0.42 3.63E+18 1.24 0.00E+00 5.3 0.00E+00 5.9 0.00E+00 6.7 0.00E+00 8.5 0.00E+00 9.5 0.00E+00 10.7 0.00E+00 12.1 0.00E+00 13.6 0.00E+00 15.4 0.00E+00 0.47 3.00E+18 0.53 2.44E+18 0.60 1.95E+18 0.67 1.45E+18 1.40 0.00E+00 1.57 3.37E+11 1.78 0.00E+00 2.00 6.58E+09 2.35E+06 5.87E+02 3.49E+06 2.04E+02 5.19E+06 7.08E+01 0.76 1.78E+15 0.86 1.02E+18 2.25 2.37E+12 2.54 0.00E+00 0.97 5.88E+17 2.86 0.00E+00 0.99 5.79E+17 3.22 0.00E+00 0.99 5.76E+17 3.63 0.00E+00

OPTIMIZATION DRIVER CLOUDY 80.08

title test of optimization driver optimize literations 30 ; increase limit to number of iterations optimize luminostiy -1 ;want H-bet flux of .1 erg cm^-2 s^-1 optimize column density ;read in sets of desired column densities * optimize column density ;read in sets of desired column densities * hydrogen 2 21.3 * end of column dens * optimize lines ; read in sets of desired relative line intensities * o 3 5007 3.1415 * end of lines VARY>>> * hden 3 vary ;vary the density, ionization parameter, and bb temp * optimze increment 1 VARY>>> * black 5 vary * optimze increment .5 * optimize increment .5 * ionizat -2 vary VARY>>> optimize increment .5 * c optim.in * c cray Up to 30 iterations will be performed, and the final version of the input file will be written on Fortran I/O unit 7 3 parameters will be varied. The first lines, and the increments are: HDEN= 3.00000 Initial increment is 1.000, the limits are -1.00E+37 to 1.00E+37 BLACKbody= 5.00000 Initial increment is 0.500, the limits are -1.00E+37 to 1.00E+37 IONIZATION PARAMETER= -2.00000 HDEN= 3.00000 BLACKbody= 5.00000 IONIZATION PARAMETER= -2.00000 IONIZATION PARAMETER= -2.00000 ID Model Observed error 0 3 5007 13.93833 3.14150 0.055000 HYDR 2 8.8892E+20 1.9553E+21 0.055000 1 TOTL 4861 -0.87555 -1.00000 0.055000 Iteration 1 Chieg= 4.87E+03 Iteration 1 chieg= 4.87E+03 chi**2 Type 4.72E+03 Relative intensity 122.98053 Column density 2.48E+01 Line intensity chi**2 error Type 9.12E+03 Relative intensity 112.29203 Column density 3.41E+02 Line intensity 0.05000 0.05000 HDEN= 3,00000

BLACKbody= 5.50000 BLACKDOGY= 5.50000 ID NIZATION PARAMETER= -2.00000 ID Model Observed error 0 3 5007 19.40824 3.14150 0.05000 HYDR 2 1.5823E+21 1.9953E+21 0.05000 TOTL 4861 -0.84828 -1.00000 0.05000 Iteration 3 Chisq= 1.08E+04 chi**2 Type 1.07E+04 Relative intensity 17.13797 Column density 3.48E+01 Line intensity IONIZATION PARAMETER= -1.50000 ID Model Observed error 0 3 5007 15.80766 3.14150 0.05000 HYDR 2 2.8449E+21 1.953B+21 0.05000 TOTL 4861 -0.37613 -1.00000 0.05000 Iteration 4 Chisq= 6.81E+03 chi**2 Type 6.50E+03 Relative intensity 72.53675 Column density 2.32E+02 Line intensity HDEN= 3.66667 BLACKbody= 4.50000 IONIZATION PARAMETER= -1.66667 chi**2 Type 6.55E+03 Relative intensity 13.31223 Column density 3.43E+02 Line intensity HDEN= 2.44444 BLACKbody= 4.66667 IONIZATION PARAMETER= -1.44444chi**2 Type 1.20E+02 Relative intensity 22.89984 Column density 4.35E+01 Line intensity HDEN= 1.66667 BLACKbody= 4.50000 IONIZATION PARAMETER= -1.16667
 IONIZATION PARAMETER= -1.16667

 ID
 Model
 Observed
 error

 0 3 5007
 0.00180
 3.14150
 0.05000
 3

 HYDR
 2 6.4053E+17
 1.953B+21
 0.05000
 3

 TOTL
 4861
 -4.67149
 -1.00000
 0.05000
 4

 Iteration
 7 Chisq=
 1.00E+10
 0.05000
 4
 chi**2 Type 1.22E+09 Relative intensity 399.74322 Column density 8.81E+09 Line intensity HDEN= 1.96296 chi**2 Type 6.63E+03 Relative intensity 27.93300 Column density 3.12E+03 Line intensity BLACKbody= 4.69444 IONIZATION PARAMETER= -1.65741 ID Model O 3 5007 4.82630 Observed 3.14150 chi**2 Type 1.15E+02 Relative intensity error 0.05000 1.9953E+21 HYDR HYDR 2 1.6666E+21 TOTL 4861 -0.26470 0.05000 10.85559 Column density 2.66E+02 Line intensity -0.26470 -1.00000 0.05000

Iteration 9 Chisq= 3.92E+02 HDEN= 2.79012 BLACKbody= 4.57407 IONIZATION PARAMETER= -1.90123
 IONIZATION PARAMETERS
 -1.90123

 ID
 Model
 Observed

 0 3 5007
 0.95346
 3.14150

 HYDR
 2 9.3401E+20
 1.9953E+21

 TOTL
 4861
 -0.94653
 -1.00000

 Iteration
 10 Chisq=
 2.23E+03
 chi**2 Type 2.11E+03 Relative intensity 113.16092 Column density 5.37E+00 Line intensity error 0.05000 0.05000 HDEN= 2.65021 BLACKbody= 4.29012 IONIZATION PARAMETER= -1.33539
 IONIZATION PARAMETER
 -1.35339

 ID
 Model
 Observed
 error

 0
 3
 5007
 0.00097
 3.14150
 0.05000
 4

 HYDR
 2
 2.9591E+21
 1.953B+21
 0.05000
 5

 TOTL
 4861
 -0.53810
 -1.00000
 0.05000
 5

 Iteration
 11 Chiege
 4.23E+09
 chi**2 Type 4.23E+09 Relative intensity 93.34197 Column density 1.71E+02 Line intensity HDEN= 2.91255 HDEN= 2.91255 BLACKbody= 4.82253 IONIZATION PARAMETER= -1.83385 ID MCARTION PARAMETER= -1.83385 ID Model Observed error 0 3 5007 7.36194 3.14150 0.05000 7 HYDR 2 1.1983E+21 1.9953E+21 0.05000 6 TOTL 4861 -0.76589 -1.00000 0.05000 6 Iteration 12 Chisq= 8.55E+02 chi**2 Type 7.22E+02 Relative intensity 63.81360 Column density 6.95E+01 Line intensity HDEN= 2.94170 chi**2 Type 2.55E+03 Relative intensity 196.29044 Column density 2.52E+02 Line intensity error 0.05000 0.05000 0.05000 3 BLACKbody= 4.65098 IONIZATION PARAMETER= -1.77323 IONIZATION PARAMETER= -1.77323 ID Model Observed error 0 3 5007 2.35474 3.14150 0.05000 4 HYDR 2 1.2192E+21 1.955B+21 0.05000 6 TOTL 4861 -0.78182 -1.00000 0.05000 6 Iteration 14 Chisq= 1.68E+02 chi**2 Type 4.47E+01 Relative intensity 60.52031 Column density 6.24E+01 Line intensity HDEN= 2.76292 BLACKbody= 4.51886 IONIZATION PARAMETER= -1.41621 IONIZATION PARAMETER= -1.41621 ID Model Observed error 0 3 5007 0.36990 3.14150 0.05000 HYDR 2 2.7488E+21 0.953E+21 0.05000 TOTL 4861 -0.50413 -1.00000 0.05000 Iteration 15 Chisq= 2.27E+04 ****** chi**2 Type 2.25E+04 Relative intensity 57.05494 Column density 1.85E+02 Line intensity HDEN= 2.87514 BLACKbody= 4.74661 IONIZATION PARAMETER= -1.72944 Model Observed error chi**2 Type ТD

O 3 5007 4.98990 3.14150 0.05000 HYDR 2 1.4313E+21 1.9953E+21 0.05000 TOTI 4861 -0.69381 -1.00000 0.05000 Iteration 16 Chisq= 2.73E+02 1.38E+02 Relative intensity 31.96007 Column density 1.02E+02 Line intensity HDEN= 2.19100 BLACKbody= 4.68173 IONIZATION PARAMETER= -1.64067 ID Model Observed error 0 3 5007 1.72537 3.14150 0.05000 2 HYDR 2 1.5279E+21 1.9953E+21 0.05000 2 TOTL 4861 -1.27547 -1.00000 0.05000 2 Iteration 17 Chisq= 6.05E+02 HDEN= 2.19100 BLACKbody= 4.68173 chi**2 Type 2.69E+02 Relative intensity 21.94485 Column density 3.14E+02 Line intensity HDEN= 2.97830 BLACKbody= 4.69127 IONIZATION PARAMETER= -1.65322 IONIZATION PARAMETER= -1.65322 ID Model Observed error 0 3 5007 3.90665 3.14150 0.05000 1 HYDR 2 1.6384E+21 1.9953E+21 0.05000 TOTL 4861 -0.51797 -1.00000 0.05000 Iteration 18 Chisq= 2.16E+02 chi**2 Type 2.37E+01 Relative intensity 12.79641 Column density 1.80E+02 Line intensity HDEN= 2.62537 BLACKbody= 4.59266 IONIZATION PARAMETER= -1.51783 IONIZATION PARAMETER= -1.51783 ID Model Observed error 0 3 5007 0.98777 3.14150 0.05000 1 HYDR 2 2.1413E+21 0.05000 TOTL 4861 -0.72513 -1.00000 0.05000 8 Iteration 19 Chisq= 1.99E+03 chi**2 Type 1.90E+03 Relative intensity 2.14345 Column density 8.80E+01 Line intensity HDEN= 2.81270 BLACKbody= 4.70812 IONIZATION PARAMETER= -1.67654 chi**2 Type 1.66E+01 Relative intensity 20.80618 Column density 9.72E+01 Line intensity HDEN= 2.41180 BLACKbody= 4.65925 IONIZATION PARAMETER= -1.60959
 IONIZATION PARAMETER= -1.00959

 ID
 Model
 Observed
 error

 0 3 5007
 1.71173
 3.14150
 0.05000
 1

 HYDR
 2 1.69558+21
 0.95538+21
 0.05000
 1

 Tort
 4861
 -1.02186
 -1.00000
 0.05000
 1

 Iteration
 21 Chisq= 2.89E+02
 -1.00000
 0.05000
 1
 1
 chi**2 Type 2.79E+02 Relative intensity 9.00657 Column density 1.07E+00 Line intensity HDEN= 2.83668 BLACKbody= 4.68326 IONIZATION PARAMETER= DIACADOQY= 4.08320 IONIZATION PARAMETER= -1.64231 ID Model Observed error 0 3 5007 3.28331 3.14150 0.05000 HYDR 2 1.6476E+21 1.9953E+21 0.05000 TOTL 4861 -0.64540 -1.00000 0.05000 Iteration 22 Chisq= 1.38E+02 ****** chi**2 Type 8.15E-01 Relative intensity 12.14774 Column density 1.25E+02 Line intensity HDEN= 3,20715

BLACKbody= 4.69491 BLACKDOGY 4.69491 IONIZATION PARAMETER= -1.95028 ID Model Observed error O 3 5007 4.24748 3.14150 0.05000 HYDR 2 8.6052E+20 1.9953E+21 0.05000 1 TOTL 4861 -0.58697 -1.00000 0.05000 Iteration 23 Chisq= 3.30E+02 chi**2 Type 4.96E+01 Relative intensity 129.37612 Column density 1.51E+02 Line intensity HDEN= 2.63512 BLACKbody= 4.67373 IONIZATION PARAMETER= -1.57090 IONIZATION PARAMETER= -1.57090 ID Model Observed error 0 3 5007 2.51548 3.14150 0.05000 HYDR 2 1.9106±21 1.9553±21 0.05000 TOTL 4861 -0.76372 -1.00000 0.05000 Iteration 24 Chisq= 9.59±01 chi**2 Type 2.48E+01 Relative intensity 0.72024 Column density 7.04E+01 Line intensity HDEN= 2.69498 BLACKbody= 4.72576 IONIZATION PARAMETER= -1.48660 chi**2 Type 3.96E+01 Relative intensity 17.92258 Column density 1.33E+02 Line intensity HDEN= 2.79476 BLACKbody= 4.66967 IONIZATION PARAMETER= -1.70158 chi**2 Type 9.41E+00 Relative intensity 34.07983 Column density 7.78E+01 Line intensity HDEN= 2.65837 BLACKbody= 4.68442 IONIZATION PARAMETER= -1.65703 IONIZATION PARAMETER= -1.65703 ID Model Observed error 0 3 5007 2.75824 3.14150 0.05000 7 HYDR 2 1.55242+21 1.9558+21 0.05000 7 TOTL 4861 -0.83596 -1.00000 0.05000 7 Iteration 27 Chisq= 6.69E+01 chi**2 Type 7.72E+00 Relative intensity 19.54576 Column density 3.96E+01 Line intensity chi**2 Type 2.47E+01 Relative intensity 23.87486 Column density 8.54E+00 Line intensity
 ID
 MARAPIER
 -1.014/1

 ID
 Model
 Observed

 0 3 5007
 1.62071
 3.14150

 HYDR
 2 1.6940E+21
 1.9953E+21

 TOTL
 4861
 -0.92144
 -1.00000
 chi**2 Type 3.52E+02 Relative intensity 9.11687 Column density 1.10E+01 Line intensity error 0.05000 0.05000 0.05000

Iteration 29 Chisq= 3.72E+02 HDEN= 2.73953 BLACKbody= 4.69213 IONIZATION PARAMETER= -1.66108 chi**2 Type 8.67E-02 Relative intensity 18.59250 Column density 7.18E+01 Line intensity HDEN= 2.50116 BLACKbody= 4.69757 IONIZATION PARAMETER= -1.56267
 ION FARMETER
 -1.30207

 ID
 Model
 Observed
 error

 0
 3
 5007
 2.72126
 3.14150
 0.05000

 HYDR
 2
 1.9427E+21
 1.953B+21
 0.05000
 1.955B+21
 0.05000

 TOTL
 4861
 -0.88813
 -1.00000
 0.05000
 1

 Iteration
 31 Chisq=
 3.04E+01
 1
 1
 1
 chi**2 Type 9.54E+00 Relative intensity 0.27746 Column density 2.06E+01 Line intensity HDEN= 2.35436 HDEN= 2.35436 BLACKbody= 4.71151 IONIZATION PARAMETER= -1.49322 ID Model Observed error 0 3 5007 2.78743 3.14150 0.05000 HYDR 2 2.2585E+21 1.9953E+21 0.05000 TOTL 4861 -0.96615 -1.00000 0.05000 Iteration 32 Chisg= 1.57E+01 chi**2 Type 6.45E+00 Relative intensity 6.96386 Column density 2.25E+00 Line intensity HDEN= 2.47362 4.71871 BLACKbody= chi**2 Type 2.10E-01 Relative intensity 13.21916 Column density 3.04E-03 Line intensity IONIZATION PARAMETER= -1.67688 ID Model Observed error 0 3 5007 3.38859 3.14150 0.05000 : HYDR 2 1.5358E+21 1.953B+21 0.05000 TOTL 4861 -1.11195 -1.00000 0.05000 : Iteration 34 Chisq= 5.83E+01 ****** chi**2 Type 2.47E+00 Relative intensity 21.21164 Column density 3.46E+01 Line intensity IONIZATION PARAMETER= -1.53836 ID Model Observed error 0 3 5007 2.52734 3.14150 0.05000 HYDR 2 2.0157E+21 1.9953E+21 0.05000 TOTL 4861 -1.16974 -1.00000 0.05000 Iteration 35 Chisq= 1.15E+02 chi**2 Type 2.36E+01 Relative intensity 0.04186 Column density 9.15E+01 Line intensity HDEN= 2.60263 BLACKbody= 4.69860 IONIZATION PARAMETER= -1.63040 chi**2 Model Observed error Type ТD

O 3 5007 2.96916 3.14150 0.05000 HYDR 2 1.6613E+21 1.9953E+21 0.05000 TOTI 4861 -0.86339 -1.00000 0.05000 Iteration 36 Chisq= 4.17E+01 1.35E+00 Relative intensity 11.20731 Column density 2.91E+01 Line intensity HDEN= 2.38452 HDEN= 2.38452 BLACKbody= 4.73421 IONIZATION PARAMETER= -1.51239 ID Model Observed error 0 3 5007 3.39501 3.14150 0.05000 HYDR 2 2.2239E+21 1.9953E+21 0.05000 TOTL 4861 -0.95575 -1.00000 0.05000 Iteration 37 Chisg= 1.16E+01 chi**2 Type 2.60E+00 Relative intensity 5.25276 Column density 3.75E+00 Line intensity HDEN= 2.29217 ody= 4.75881 HDEN= 2.29217 BLACKbody= 4.75881 IONIZATION PARAMETER= -1.43639 ID Model Observed error 0 3 5007 3.90052 3.14150 0.05000 2 HYDR 2 2.6860E+21 1.9953E+21 0.05000 2 TOTL 4861 -0.97296 -1.00000 0.05000 2 Iteration 38 Chisg= 7.27E+01 chi**2 Type 2.34E+01 Relative intensity 47.93817 Column density 1.46E+00 Line intensity HDEN= 2.20570 BLACKbody= 4.74435 IONIZATION PARAMETER= -1.46771 IONIZATION PARAMETER= -1.46771 ID Model Observed error 0 3 5007 3.29647 3.14150 0.05000 9 HYDR 2 2.459E+21 0.05000 1 TOTL 4861 -1.08645 -1.00000 0.05000 1 Iteration 39 Chisq= 4.16E+01 chi**2 Type 9.73E-01 Relative intensity 21.22705 Column density 1.94E+01 Line intensity HDEN= 2.30493 BLACKbody= 4.73291 IONIZATION PARAMETER= -1.50838 chi**2 Type 1.34E-02 Relative intensity 3.97098 Column density 2.62E+00 Line intensity HDEN= 2.42102 BLACKbody= 4.74570 IONIZATION PARAMETER= -1.61500
 IONIZATION PARAMETER= -1.61500

 ID
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 Observed
 error

 0 3 5007
 3.66977
 3.14150
 0.055000

 HYDR 2 1.7661E+21
 1.9953E+21
 0.055000

 Tort 4861
 -1.02695
 -1.00000
 0.055000

 Iteration 41 Chisq=
 1.82E+01
 1
 chi**2 Type 1.13E+01 Relative intensity 5.27461 Column density 1.64E+00 Line intensity chi**2 error Type 7.52E-01 Relative intensity 1.70288 Column density 7.05E-01 Line intensity 0.05000 0.05000 HDEN= 2,23336

BLACKbody= 4.73942 BLACKDOGY= 4.73942 IONIZATION PARAMETER= -1.38807 ID Model Observed error 0 3 5007 3.30335 3.14150 0.05000 HYDR 2 2.9335E+21 1.9953E+21 0.05000 T TOTL 4861 -0.98045 -1.00000 0.05000 Iteration 43 Chisq= 9.03E+01 chi**2 Type 1.06E+00 Relative intensity 88.44898 Column density 7.75E-01 Line intensity chi**2 IONIZATION PARAMETER= -1.57818 ID Model Observed error 0 3 5007 3.14357 3.14150 0.05000 HYDR 2 1.8904E+21 1.9953E+21 0.05000 TOTL 4861 -0.99433 -1.00000 0.05000 Iteration 44 Chisq= 1.17E+00 ****** chi**2 Type 1.73E-04 Relative intensity 1.10506 Column density 6.74E-02 Line intensity HDEN= 2.34182 BLACKbody= 4.71703 IONIZATION PARAMETER= -1.56109 chi**2 Type 5.92E+00 Relative intensity 0.18913 Column density 4.40E+00 Line intensity HDEN= 2.35250 BLACKbody= 4.72132 IONIZATION PARAMETER= -1.54892
 IONIZATION PARAMETER
 -1.34892

 ID
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 Observed
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 0
 3
 5007
 2.95900
 3.14150
 0.05000
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 HYDR
 2
 2.0050E+21
 1.953B+21
 0.05000
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 -1.02444
 -1.00000
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 chi**2 Type 1.52E+00 Relative intensity 0.00957 Column density 1.34E+00 Line intensity HDEN= 2.45312 HDEN= 2.45312 BLACKbody= 4.71060 IONIZATION PARAMETER= -1.59213
 LUNIZATION PARAMETER= -1.59213

 ID
 Model
 Observed
 error

 0 3 5007
 2.87724
 3.14150
 0.05000
 1

 HYDR
 2 1.8115421
 1.9953B+21
 0.05000
 1

 TOTL
 4861
 -0.96875
 -1.00000
 0.05000

 Iteration
 47 Chisq=
 8.69E+00
 1
 1
 chi**2 Type 3.37E+00 Relative intensity 3.39280 Column density 1.93E+00 Line intensity HDEN= 2.34198 chi**2 Type 3.07E-01 Relative intensity 0.61152 Column density 9.69E-01 Line intensity BLACKbody= 4.72830 IONIZATION PARAMETER= -1.58061
 ID
 MARAPIER
 -1.38001

 ID
 Model
 Observed

 0 3 5007
 3.13919
 3.14150

 HYDR 2
 1.8785E+21
 1.9953E+21

 TOTL 4861
 -1.04215
 -1.00000
 chi**2 Type 2.17E-04 Relative intensity error 0.05000 0.05000 1.36883 Column density 4.15E+00 Line intensity 0.05000

Iteration 49 Chisq= 5.52E+00 HDEN= 2.37018 BLACKbody= 4.72212 IONIZATION PARAMETER= -1.53790 chi**2 Type 4.19E-01 Relative intensity 0.42951 Column density 2.42E-02 Line intensity HDEN= 2.39798 BLACKbody= 4.72757 IONIZATION PARAMETER= -1.54802
 ID
 MARABLER
 -1.94802

 ID
 Model
 Observed
 error

 0
 3
 5007
 3.18737
 3.14150
 0.055000

 HYDR
 2
 2.0246E+21
 1.9953E+21
 0.055000
 8

 Tearting
 1
 -0.97949
 -1.00000
 0.055000
 8

 Tearting
 51
 Chisge
 1.02E+00
 1.02E+00
 1.02E+00
 chi**2 Type 8.53E-02 Relative intensity 0.08669 Column density 8.51E-01 Line intensity HDEN= 2.44584 BLACKbody= 4.72171 HDEN= 2.44584 BLACKbody= 4.72171 IONIZATION PARAMETER= -1.58008 ID Model Observed error 0 3 5007 3.14899 3.14150 0.05000 2 HYDR 2 1.8896E+21 1.9953E+21 0.05000 TOTL 4861 -0.96290 -1.00000 0.05000 2 Iteration 52 Chisq= 3.81E+00 chi**2 Type 2.28E-03 Relative intensity 1.12210 Column density 2.68E+00 Line intensity HDEN= 2.36794 BLACKbody= 4.72593 chi**2 Type 1.56E-02 Relative intensity 0.33019 Column density 9.69E-03 Line intensity error 0.05000 0.05000 0.05000 IONIZATION PARAMETER= -1.50710 ID Model Observed error 0 3 5007 3.07674 3.14150 0.05000 1 HYDR 2 2.2182+21 1.9953E+21 0.05000 TOTL 4861 -0.98995 -1.00000 0.05000 2 Iteration 54 Chisq= 5.38E+00 chi**2 Type 1.77E-01 Relative intensity 4.99726 Column density 2.09E-01 Line intensity HDEN= 2.39613 BLACKbody= 4.72454 IONIZATION PARAMETER= -1.56041 IONIZATION PARAMETER= -1.56041 ID Model Observed error 0 3 5007 3.14055 3.14150 0.05000 HYDR 2 1.9657E+21 1.9953E+21 0.055000 TOTL 4861 -0.99403 -1.00000 0.05000 Iteration 55 Chisq= 1.62E-01 chi**2 Type 3.67E-05 Relative intensity 0.08789 Column density 7.45E-02 Line intensity HDEN= 2.35819 BLACKbody= 4.72083 IONIZATION PARAMETER= -1.54553 Model Observed error chi**2 Type ТD

O 3 5007 2.96393 3.14150 0.05000 3 HYDR 2 2.0205E+21 1.9953E+21 0.05000 TOTI 4861 -1.01553 -1.00000 0.05000 3 Iteration 56 Chisq= 2.03E+00 1.44E+00 Relative intensity 0.06396 Column density 5.30E-01 Line intensity HDEN= 2.38803 BLACKbody= 4.72588 IONIZATION PARAMETER= -1.54740 ID Model Observed error 0 3 5007 3.16515 3.14150 0.05000 2 HYDR 2 2.0289E+21 1.9953E+21 0.05000 TOTL 4861 -0.98841 -1.00000 0.05000 2 Iteration 57 Chisq= 4.14E-01 HDEN= 2.38803 BLACKbody= 4.72588 chi**2 Type 2.27E-02 Relative intensity 0.11349 Column density 2.78E-01 Line intensity HDEN= 2.39789 BLACKbody= 4.72878 BLACKbody= 4.72878 IONIZATION PARAMETER= -1.56198 ID Model Observed error 0 3 5007 3.20199 3.14150 0.05000 HYDR 2 1.9637E+21 1.9953E+21 0.05000 TOTL 4861 -0.99348 -1.00000 0.05000 Iteration 58 Chisq= 3.37E-01 chi**2 Type 1.48E-01 Relative intensity 0.10020 Column density 8.87E-02 Line intensity HDEN= 2.38661 BLACKbody= 4.72696 IONIZATION PARAMETER= -1.56220 IONIZATION PARAMETER= -1.56220 ID Model Observed error 0 3 5007 3.17330 3.14150 0.05000 HYDR 2 1.9605E+21 1.9953E+21 0.05000 TOTL 4861 -1.00519 -1.00000 0.05000 Iteration 59 Chisq= 2.20E-01 Amoeba exceeding maximum iterations. chi**2 Type 4.10E-02 Relative intensity 0.12131 Column density 5.79E-02 Line intensity Cloudy was called 59 times. Optimal command: HDEN= 2.39613 Optimal command: HDEN= 2.39613 Smallest value: 1.67E+00 Largest value: 4.00E+00 Allowed range -1.00E+37 to 1.00E+37 Optimal command: BLACKbody= 4.72454 Smallest value: 4.29E+00 Largest value: 5.50E+00 Allowed range -1.00E+37 to 1.00E+37 Optimal command: IONIZATION PARAMETER= -1.56041 Smallest value: -2.00E+00 Largest value: -1.17E+00 Allowed range -1.00E+37 to 1.00E+37 HDEN= 2.39613 BLACKbody= 4.72454 IONIZATION PARAMETER= -1.56041

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title test of optimization driver	
optimize iterations 30 ; increase limit to number of iterations	
optimize luminostiy -1 ;want H-bet flux of .1 erg cm^-2 s^-1	
optimize column density ; read in sets of desired column densities	
optimize lines ; read in sets of desired relative line intensities	
HDEN= 2.39613	
optimze increment 1	
BLACKbody= 4.72454	
optimize increment .5	
IONIZATION PARAMETER= -1.56041	
optimize increment .5	
c optim.in	
c cray	

Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

335Cell Peak1.31E+00	Lo 1.00E-05=0.9105cm	Hi-Con:1.23E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 0.8355	Average nu:1.529E+00	P(X-ray): 0.0000	P(BalC): 0.6195	O(Balmer C): 11.4912
Q(1.0-1.8): 11.2051	Q(1.8-4.0): 10.6528	O(4.0-20): 8.4244	O(20): 0.0000	Ion pht flx:2.056E+11
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): -0.7514	Alf(ox): 0.0000	Total lumin: 1.0488
U(1.0):2.754E-02	U(4.0):3.560E-05	T(En-Den):1.490E+01	T(Comp):5.077E+04	nuJnu(912A):7.263E+00
Occ(FarIR):1.988E-10	Occ(H n=6):7.154E-14	Occ(1Ryd):3.349E-16	Occ(4R):4.123E-20	Occ (Nu-hi):1.414E-30
Tbr(FarIR):3.306E-10	Tbr(H n=6):3.177E-10	Tbr(1Ryd):5.291E-11	Tbr(4R):2.608E-14	Tbr (Nu-hi):2.699E-24
				tot:3.212E-19 T912: 1.567E-03###
-4.09 4686 0.13 5876 0.08 19				
				H+ 2.101E-12 H col den 9.039E+17
): 1.490E+01 T(diffs): 2.683E+02
				ct 1.000E+00 Gam 1/tot 1.000E+00
				18 1.086E-19 8.707E-19 3.118E-19
	1.305E-19 2.018E-19 3.2			
				el 1.131E-07 Force Mul 9.524E+02
	8.579E-01 1.248E-01 2.6			
				1: 0.000E+00 02+/Otot: 0.000E+00
				00 Hex(tot): 0.000E+00 A:-12.245
	9.534E-01 1.835E-02 0.0			
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				tot:8.465E-21 T912: 1.005E+02###
-0.99 4686 0.00 5876 0.16 19				
P(LINES): 0.032 0.000 0.000 0.0				
	H+0/Hden: 1.000E+00 2.5			H+ 1.153E-07 H col den 1.982E+21
): 1.176E+01 T(diffs): 3.004E+02
				ct 1.000E+00 Gam 1/tot 1.000E+00
He singlet 7.744E-01 2.268E-14	6.203E-21 8.317E-21 1.2	288E-20 1.916E-20 He tr	iplt 1.769E-08 2.688E-	16 1.010E-20 2.082E-19 9.607E-21
HeII 0.000E+00 0.000E+00	0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000	0.000E+00 0.000E+00 0.000E+	00 PRAD/GAS; 7.049E-02

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Pressure						1.637E-10						4.270E+02
Carbon	3.293E-05	9.937E-01	6.221E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen	9.459E-01	5.408E-02	2.277E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/Ototl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9 5028-01	4 982E-02	4 0528-06	0 0008+00	0 000 -	0.000E+00	0 000E+00	0 000E+00	0 000 =+00	Hex(tot).	0 0000+00	A 12 244
						0.000E+00						A12.244
Neon												
Magnesium 0	1.607E-04	9.906E-01	9.216E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Aluminium 0	2.721E-05	9.952E-01	4.799E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Silicon 0	2.674E-05	1.000E+00	7.116E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
	8.821E-06											
	7.406E-01											
Calcium 0	5.533E-06	1.067E-02	9.893E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Iron 0	4.953E-04	9.994E-01	1.133E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
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C-This is t	he last ite	eration and	d the fine	structure	optical de	epths chand	ed. Try a	another ite	eration.			
Frequency	out of rai	nge of free	-free gau	nt factor	routine.		· •					
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						-1.56	; <	****	*******	*******	****	****	
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En	nission Lin	e Spectru	ım.	Constant	Density	Model.		One	en deome	try. Itera	tion	1 of 1.	
200	TODION DIN	e opeoere			ensity (er				geome	<i> </i>	01011		
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-0.994	1.0000	He2p	910	-2.392	0.0400	N	2	6548	-2.412	0.0382	s	2 6720 -	2.198
0.366	22.9100	He I	504	-1.118	0.7523	REC	:	6584	-3.797	0.0016	s	2 4074 -	3.565
0.349	22.0437	He I	4471	-2.306	0.0488	N	2	5755	-3.998	0.0010	S	210330 -	3.738
0.296	19.4907	TOTL	5876	-1.801	0.1561				-3.261			II 6731 -	2.537
-0.666	2.1277	Ca B	5876	-1.821	0.1488	N	2	203	-3.950	0.0011	S	II 6716 -	2.464
-1.365	0.4252	TOTL1	0830	-1.552	0.2767	N	2	4239	-4.419	0.0004	S	II 4070 -	
-0.989	1.0118	TOTL	3889	-2.372	0.0419	N	2	5680	-3.838	0.0014	S	II 4078 -	4.169
0.527	33.2202	TOTL	7065	-2.307	0.0487	N	2	2140	-4.057	0.0009	S	II10323 -	4.192
-0.989	1.0118	CcHE	0	-2.372	0.0418	N	3	1750	-3.978	0.0010	S	II10289 -	4.321
-1.010	0.9632	He T	2	-2.511	0.0304	N	3	57	-1.301	0.4929	S	TT10373 -	4.640

incensity (erg/s/cm 2)																
TOTL	4861	-0.994	1.0000	He2p	910	-2.392	0.0400	N	26	5548	-2.412	0.0382	s	2 6720	-2.198	0.0625
TOTL	1216	0.366	22.9100	He I	504	-1.118	0.7523	REC	: 6	5584	-3.797	0.0016	s	2 4074	-3.565	0.0027
TotH	0 1	0.349	22.0437	He I	4471	-2.306	0.0488	N	2 5	5755	-3.998	0.0010	s	210330	-3.738	0.0018
BFH1	0	0.296	19.4907	TOTL	5876	-1.801	0.1561	N	2	122	-3.261	0.0054	s	II 6731	-2.537	0.0286
BFHe	. 0	-0.666	2.1277	Ca B	5876	-1.821	0.1488	N	2	203	-3.950	0.0011	s	II 6716	-2.464	0.0339
TotM	ι O ·	-1.365	0.4252	TOTL1	0830	-1.552	0.2767	N	2 4	1239	-4.419	0.0004	s	II 4070	-3.689	0.0020
CA B	4861	-0.989	1.0118	TOTL	3889	-2.372	0.0419	N	2 5	5680	-3.838	0.0014	s	II 4078	-4.169	0.0007
CA B	1216	0.527	33.2202	TOTL	7065	-2.307	0.0487	N	2 2	2140	-4.057	0.0009	s	II10323	-4.192	0.0006
DU B	4861	-0.989	1.0118	CcHE	0	-2.372	0.0418	N	3 1	1750	-3.978	0.0010	s	II10289	-4.321	0.0005
Q(H)	4861 -	-1.010	0.9632	He I	2	-2.511	0.0304	N	3	57	-1.301	0.4929	s	II10373	-4.640	0.0002
Q(H)	1216	0.524	32.9317	DevB	2	-2.763	0.0170	0	1 6	5300	-3.278	0.0052	s	II10339	-4.319	0.0005
TOTL	6563	-0.570	2.6574	He I	5016	-2.576	0.0262	0	1 6	5363	-3.755	0.0017	s	3 18	-1.106	0.7725
TOTL	4861	-0.994	1.0000	DevB	5016	-2.665	0.0213	0	1	630	-3.827	0.0015	s	3 34	-0.961	1.0790
TOTL	4340	-1.281	0.5165	He I	3965	-2.875	0.0132	0	1 1	1470	-4.876	0.0001	s		-1.065	0.8496
TOTL	4102 -	-1.501	0.3109	DevB	3965	-3.066	0.0085	0	1 7	7774	-4.707	0.0002	s	3 9069	-1.481	0.3262
TOTL	18751 -	-1.551	0.2772	He I	3614	-3.158	0.0068	TOT	L 3	3727	-1.421	0.3738	s	3 6312	-3.214	0.0060
TOTL	12818	-1.812	0.1522	DevB	3614	-3.259	0.0054	TOT	L 7	7325	-3.291	0.0051	s	3 3722	-3.443	0.0036
TOTL	10938 -	-2.024	0.0932	He I	3448	-3.377	0.0041	ION	IZ 3	3727	-3.748	0.0018	s	3 1729	-4.986	0.0001
TOTL	40512 -	-2.223	0.0591	DevB	3448	-3.548	0.0028	ION	z 7	7325	-4.348	0.0004	s	4 105	-1.013	0.9562
TOTL	26252	-2.409	0.0385	HeII	228	-2.785	0.0162	0 I	I 3	3729	-1.703	0.1954	Ar	2 7	-3.571	0.0026
TOTL	74578	-2.738	0.0180	ESC	304	-4.097	0.0008	ΟΙ	I 3	3726	-1.747	0.1766	Ar	3 7135	-2.061	0.0857
2 NU	0	0.016	10.2312	He2C	911	-3.267	0.0053	0 I	I 2	2471	-3.391	0.0040	Ar	3 7751	-2.691	0.0201
	1216		22.9100				0.0147				-3.548	0.0028	Ar		-2.949	0.0111
TOTL	1026 -	-3.333	0.0046	TOTL	4686	-3.785	0.0016	ΟΙ	I 7	7332	-3.640	0.0023	Ar	3 9	-1.806	0.1543
	973		0.0041				0.0058				-3.270			4 4740		0.0074
	950		0.0039				0.0171				-3.759	0.0017		2 3933		0.0004
TOTL		-3.405	0.0039				0.0171				-4.902	0.0001		2 8579		0.0050
	1216		22.9100				0.0030				-0.497	3.1405		2 7306		0.0660
	1216		0.3037				0.0029				-0.974	1.0468		2K 3934		0.0002
	18751 -		0.2773				0.0002				-3.377	0.0041		2H 3969		0.0002
	40512		0.0242				0.0074				-4.004	0.0010		2X 8498		0.0003
	4860		2.4052								-0.579	2.5983		2Y 8542		0.0030
	1215 -		0.0007						3		-0.326	4.6509		2Z 8662		0.0017
Inci	4861 -	-0.650	2.2070	REC	1335	-1.669	0.2113	0	4	26	-2.511	0.0304	Ca	F1 7291	-2.400	0.0393

Inci	1216 0.711	50.7209	C 2 4267 -3.527	0.0029	Ne 2 128 -2.240	0.0568	CaF2 7324 -2.567	0.0267
BA C	0 -0.424	3.7191	TOTL 977 -2.771	0.0167	Ne 3 156 -0.674	2.0912	Ca 4 32 -3.630	0.0023
PA C	0 -0.919	1.1893	C3 R 977 -2.771	0.0167	Ne 3 361 -1.748	0.1763	Fe 2 48 -4.457	0.0003
H FF	0 -1.136	0.7213	TOTL 1909 -2.566	0.0268	Ne 3 3869 -1.758	0.1723	Fe 2 7 -2.612	0.0241
H FB	0 -0.881	1.2987	C 3 1907 -2.786	0.0161	Ne 3 3968 -2.271	0.0529	Emis 3 -2.495	0.0316
Cool	1216 -3.054	0.0087	C 3 1909 -2.967	0.0106	Emis 2798 -2.124	0.0741	Cool 3 -2.495	0.0316
H-FB	0 -4.946	0.0001	C3 R 1909 -2.933	0.0115	Cool 2798 -2.124	0.0741	TOT 0 -2.246	0.0560
HeFF	0 -2.142	0.0712	Phot 1909 -2.522		Al 3 1860 -4.188	0.0006	FEIR 0 -2.913	0.0121
HeFB	0 -1.916	0.1196	C 3 2297 -3.273	8 0.0053	Si 2 35 -1.926	0.1169	Fe 3 0 -2.455	0.0346
MeFB	0 -4.861	0.0001	C 3 4649 -4.483	3 0.0003	Si 2 2335 -3.402	0.0039	Fe 3 5270 -3.135	0.0072
MeFF	0 -3.320	0.0047	C 4 1549 -4.931	0.0001	Si 2 1808 -4.656	0.0002	Fe 3 4658 -2.891	0.0127
Toff	0 -1.092	0.7972	N 1 5200 -4.346	0.0004	Si 3 1895 -3.048	0.0088		
esc	584 -1.929	0.1161	N 2 6584 -1.935	0.1145	PHOT 1895 -3.351	0.0044		

TEST OF OPTIMIZATION DRIVER Cooling: H FB 0:0.059 O 3 5007:0.142 O 3 880:0.118 O 3 520:0.210 Ne 3 156:0.095	
Heating: BFH1 0:0.884 BFHe 0:0.097 IONIZE PARMET: U(1-) -1.5600 U(4-): -4.4486 U(sp): -1.56 Q(ion): 6.175 L(ion): -3.950 Q(low): 11.56 P(low) 0.64 ENERGY BUDGET: Heat: 0.349 Coolg: 0.350 Error: 0.3% Compt H: -6.477 WorkF: 0.824 F-F H -5.717 PRADMX:1.13E+01 Column density H12:1.982E+21 H II:1.966E+21 H1:1.597E+19 H-: 1.223E+11 H2: 9.929E+10 H2+17.875E+10 He H+:1.856E+12	
OH: 0.000E+00 Heff:0.000E+00 <nh>:2.490E+02 <td>:6.26E+03 <to3>:6.16E+03 Ne:2.739E+02 ti(snd):9.11E+12 NeN+d1:5.37E+23 <t(c3)>:6.23E+03 <e(c3)>:2.74E+02 He/Ha:1.15E-01 = 1.18*true N/oap:4.47E-02 = 0.34true T(O3R):6.682E+03 L THIN:1.00E+30 <t(s2)>:7.50E+03 <e(s2)>:2.21E+02 T He+:6.26E+03 EHE+:2.73E+02 T(O+):7.26E+03 EO+:2.66E+02 iter/zn: 3.082 Te-low:3.64E+03 Te-high:8.90E+03 H1u/zn:3.88E+00</e(s2)></t(s2)></e(c3)></t(c3)></to3></td></nh>	:6.26E+03 <to3>:6.16E+03 Ne:2.739E+02 ti(snd):9.11E+12 NeN+d1:5.37E+23 <t(c3)>:6.23E+03 <e(c3)>:2.74E+02 He/Ha:1.15E-01 = 1.18*true N/oap:4.47E-02 = 0.34true T(O3R):6.682E+03 L THIN:1.00E+30 <t(s2)>:7.50E+03 <e(s2)>:2.21E+02 T He+:6.26E+03 EHE+:2.73E+02 T(O+):7.26E+03 EO+:2.66E+02 iter/zn: 3.082 Te-low:3.64E+03 Te-high:8.90E+03 H1u/zn:3.88E+00</e(s2)></t(s2)></e(c3)></t(c3)></to3>
<pre><a>:0.00E+00 erdeFe0.0E+00 Tcompt9.45E+09 Tthr1.79E+09 <tden>: 6.26E+03 <dens>:5.87E-22 <mol>:6.48E-01 Mean Jeans l(cm)1.87E+20 M(sun)1.01E+06 smallest: len(cm):1.43E+20 M(sun):4.48E+05 Alf(ox-tran): 0.0000</mol></dens></tden></pre>	
Optical Depths: CONTN; COMP: 1.44E-03 H-: 4.77E-06 R(1300): 1.07E-04 H2+ 5.51E-07 HeTri:2.09E-03 Pfa:1.44E-03 Pa:1.44E-03 Ba:1.44E-03 Hb:1.44E-03 La:4.25E-03 1r:1.005E+02 1.8:2.75E+01 4.:5.799E+01 21R:1.000E-20 10830: 2.05E+02 3889: 8.75E+00 5876: 1.26E-06 7065: 6.96E-07	
10530: 2.054702 3637: 6.754700 3676: 1.264-06 705: 6.962-07 1335: 1.00E-20 1335: 6.54E+03 977: 2.50E+05 1397: 1.51E+04 1550: 5.18E+04 1207: 6.42E+04 1085: 3.74E+02 1240: 1.89E-02 1035: 1.00E-20 1335: 6.54E+03 977: 2.50E+05 1397: 1.51E+04 789: 4.84E+01 1207: 6.42E+04 1085: 3.74E+02 1194: 1.88E+02 1909: 9.96E-02 1895: 1.72E+00 2326: 3.27E-03 1666: 7.88E-01 1750: 3.75E-03 1025: 1.32E+02 352: 1.00E-20 347: 1.00E-20 1806: 4.34E+03 630: 3.05E-02 834: 2.92E+04 835: 3.83E+04 1808: 6.96E+03 1256: 4.87E+01 -3: 9.48E+01 -48: 6.59E-08 334: 4.92E+02 3969: 2.48E+02 8496: 6.61E-05 8542: 5.88E-04 8662: 3.36E-04 353: 1.00E-20 1304: 4.51E+02 1122: 6.31E+02 990: 1.65E+04 1402: 6.46E-04 1214: 1.65E-07 1486: 6.68E-03 235: 1.66E-02 1406: 2.01E-01 1656: 1.22E+00 9830: 2.03E-10 877: 9.76E-11 6300: 1.20E-06 5577: 1.40E-10 7.324: 3.29E-05 7324: 2.28E-05 1039: 6.41E+01 -8466: 1.83E+13 -4368: 7.12E-16 -132: 3.62E-15 -13: 5.79E-15 -29: 2.78E-16 -46: 1.	
-245: 1.00E-20 765: 4.06E+03 -1198: 3.85E-03 786: 1.15E+01 C157: 3.05E-03 NE12: 2.81E-03 N205: 2.64E-03 N57: 2.14E-01 0146:-1.67E-04 063: 1.35E-02 088: 2.13E+00 052: 9.80E-01 026: 1.98E-03 NE13: 1.46E-02 NE36: -9.92E-04 NE16: 3.06E-01 MG4: 2.56E-06 MG14: 1.00E-20 MG6: 1.00E-20 SI35: 6.45E-03 S19: 1.00E-02 S34: 1.24E-01 S11: 1.59E-02 AR7: 3.34E-04 AR9: 1.01E-02 AR22:-1.15E-05 AR13: 1.24E-06 AR8: 7.71E-10 CA3: 1.31E-04 CA12:-1.06E-12 CA4: 1.93E-08 NE14: 1.00E-20 NE24: 1.00E-20 S13: 1.00E-20 S14: 1.00E-20 Fe7: 1.00E-20 Fe61: 1.00E-20 Fe23: 1.00E-20 Fe13: 1.00E-20 S12.5: 1.00E-20 S16.5: 1.00E-20 C610: 4.33E-07 C370: 1.90E-05	
Old hydro optical depths: 1 9.99E+07 2 1.00E-20 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 1.00E-20	
Lines: 2-1 9.96E+09 3-2 1.59E-03 4-3 1.59E-05 5-4 7.93E-07 6-5 1.22E-07 7-6 1.22E-08 8-7 1.22E-09 New hydro optical depths: 1 1.01E+02 2 2.52E-06 3 4.77E-06 4 1.35E-06 5 5.57E-13 6 1.44E-12 7 5.14E-12 Lines: 2-1 1.12E+06 3-2 4.87E-03 4-3 8.90E-10 5-4 3.40E-10 6-5-1.69E-09 7-6 1.14E-08 8-7 1.55E-07	
Old He Is optical depths: 1 8.30E+05 2 0.00E+00 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 1.00E-20 Lines: 2-1 9.96E+09 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 0.00E+00	
New HE Is optical depths: 1 2.75E+01 2 6.47E-04 3-2.80E-16 4-8.32E-16 5-1.65E-15 6-2.87E-15 7-3.15E-14 Lines: 2-1 4.87E+04 3-2 3.19E-04 4-3 5.86E-11 5-4 1.77E-11 6-5-6.13E-11 7-6 5.09E-10 8-7 6.89E-09	
Old He II optical depths: 1 8.30E+05 2 8.30E+05 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 1.00E-20 Lines: 2-1 9.96E+09 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 0.00E+00	
New HE II optical depths: 1 5.80E+01 2 1.01E+02 3-4.59E-18 4-1.13E-17 5-2.20E-17 6-3.83E-17 7-4.13E-16 Lines: 2-1 1.33E+06 3-2 2.17E-07 4-3 2.87E-14 5-4-3.33E-14 6-5-2.59E-13 7-6 6.14E-13 8-7 9.10E-12	
Hydrogen -2.094 -0.004 Log10 Mean Ionisation (over volume)	
Helium -2.262 -0.003 -2.712 Carbon -4.888 -1.245 -0.047 -1.337 -5.721	
Nitrogen -2.445 -1.262 -0.057 -1.185 -6.131 Oxygen -2.138 -1.058 -0.044 -3.125 -7.075	
Neon -2.783 -1.151 -0.033 -3.833 Magnesium -4.388 -1.270 -0.024 -4.490	
Aluminum -5.281 -1.149 -0.253 -0.431 Silicon -5.730 -1.167 -0.248 -0.446 -2.044	
Sulphur -6.553 -1.530 -0.124 -0.663 -2.679 Argon -2.539 -1.385 -0.105 -0.770 -4.651	
Calcium -3.907 -1.339 -0.031 -1.657 -5.679 Iron -4.269 -1.765 -1.010 -0.053 -3.059 -5.583	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	
Hydrogen -2.094 -0.004 Log10 Mean Ionisation (over radius)	
Helium -2.262 -0.003 -2.712 Carbon -4.888 -1.245 -0.047 -1.337 -5.721	
Nitrogen -2.445 -1.262 -0.057 -1.185 -6.131 Oxygen -2.138 -1.058 -0.044 -3.125 -7.075	
Neon -2.783 -1.151 -0.033 -3.833 Magnesium -4.388 -1.270 -0.024 -4.490	

Helium -2.262 -0.003 -2.712 Carbon -4.888 -1.245 -0.047 -1.337 -5.721 Nitrogen -2.445 -1.262 -0.047 -1.337 -5.721 Nitrogen -2.138 -1.058 -0.044 -3.125 -7.075 Neon -2.783 -1.151 -0.033 -3.833 Magnesium -4.388 -1.270 -0.024 -4.400 Aluminum -5.281 -1.149 -0.253 -0.431 Silicon -5.730 -1.167 -0.248 -0.446 -2.044 Sulphur -6.553 -1.530 -0.124 -0.663 -2.679 Argon -2.539 -1.385 -0.105 -0.770 -4.651 Calcium -3.907 -1.339 -0.031 -1.657 -5.679 Iron -4.269 -1.765 -1.010 -0.053 -3.059 -5.583 Normalised continum 0.25 3.502 0.27 2.394 0.30 1.782 0.33 1.488 0.36 1.371 0.39 1.297 0.43 1.262 0.47 1.242 0.51 1.229 0.56 1.212 0.62 1.189 0.67 1.142 0.74 1.032 0.81 0.999 0.88 0.999 0.97 0.999 0.98 0.999 0.99 0.999 1.00 0.999 Inward continua (nuFnu) at head of Balmer, Lyman series; 1.10E+00 4.75E+00 Outwrd continua (nuFnu) at head of Balmer, Lyman series; 1.10E+00 2.17E-06 Emergent continuum - phot/ryd/cm2 (r in) 0.26 1.12E+12 0.53 5.57E+11 1.0 3.38E+11 1.2 8.37E+01 2.5 8.87E+04 4.18E+00 2.37E-11 8.45E+00 4.05E+00 0.29 7.43E+11 0.67 5.02E+11 1.0 3.35E+11 1.4 1.66E+00 2.9 3.76E+05 4.66E+00 2.37E-11 8.45E+00 4.05E+00 0.33 6.03E+11 0.67 5.02E+11 1.0 2.70E+05 1.6 6.25E+03 3.2 1.61E+06 5.25E+00 2.27E-05 1.07E+05 1.21E+01 1.43E-02 0.42 5.60E+11 0.76 4.16E+11 1.0 2.04E+05 1.8 6.48E+01 3.6 1.04E+06 5.95E+00 1.21E+01 1.21E+01 1.43E-02

0.42 5.60E+11 0.86 3.86E+11 1.0 1.54E+05 2.0 1.03E+03 3.9 1.41E+06 6.66E+00 5.01E-01 0.47 5.60E+11 0.97 3.46E+11 1.1 8.09E+03 2.3 7.59E+03 4.0 2.41E-10 7.51E+00 2.93E+00 ID Model Observed error chi**2 Type 0 3 5007 3.14055 3.14150 0.05000 3.67E-05 Relative intensity HYDR 2 1.9657E+21 1.9953E+21 0.05000 0.08780 Column density TOTL 4861 -0.99403 -1.00000 0.05000 7.45E-02 Line intensity Iteration 60 Chisge 1.62E-01	0.3	7 5.691	E+11 0.	76	4.16E+11	1.0	2.04E+05	1	.8 6.8	84E+01	3.6 1.04E+06	5.91E+00	1.47E-02	1.21E+(
ID Model Observed error chi**2 Type 0 3 5007 3.14055 3.14150 0.05000 3.67E-05 Relative intensity HYDR 2 1.9657E+21 1.9953E+21 0.05000 0.08789 Column density TOTL 4861 -0.99403 -1.00000 0.05000 7.45E-02 Line intensity	0.42	2 5.601	E+11 0.	86	3.86E+11	1.0	1.54E+05	2	.0 1.0	03E+03	3.9 1.41E+06	6.66E+00	5.01E-01	
0 3 5007 3.14055 3.14150 0.05000 3.67E-05 Relative intensity HYDR 2 1.9657E+21 1.9953E+21 0.05000 0.08789 Column density TOTI 4861 -0.99403 -1.00000 0.05000 7.45E-02 Line intensity	0.4	7 5.601	E+11 0.	97	3.46E+11	1.1	8.09E+03	2	.3 7.5	59E+03	4.0 2.41E-10	7.51E+00	2.93E+00	
HYDR 2 1.9657E+21 1.9953E+21 0.05000 0.08789 Column density TOTL 4861 -0.99403 -1.00000 0.05000 7.45E-02 Line intensity	ID		Mc	del	Observed		error	c	hi**2	Type				
TOTL 4861 -0.99403 -1.00000 0.05000 7.45E-02 Line intensity	O 3	5007	3.14	055	3.14150		0.05000	3.6	7E-05	Relative	intensity			
	HYDR	2	1.9657E	+21	1.9953E+21		0.05000	Ο.	08789	Column de	ensity			
Iteration 60 Chisg= 1.62E-01	TOTL	4861	-0.99	403	-1.00000		0.05000	7.4	5E-02	Line inte	ensity			
	Itera	ion (60 Chisq	[=	1.62E-01									

e de la constante d	
* title conditions similar to Orion nebula blister	
* sphere	
table star kurucz 39,700K	
* phi(h) 13.0	
turbulence 8 km/sec	
* hden 4	
* abundances hii region	
* constant pressure	
* iterate	
* print last iteration	
c orion.in	
c cray	
e Transformer de la construcción de	

Chemical composition He:.095 C:3.00E-04 N:7.00E-05 O:4.00E-04 Ne:1.10E-04 Mg:3.00E-05 Al:2.0E-07 Si:3.00E-06 S:1.00E-05 A:3.0E-06 Ca:2.0E-08 Fe:3.00E-06

P(nu>lryd): 2.4800 Average nu Q(1.0-1.8): 12.9496 Q(1.8-4.0) L(gam ray): 0.0000 Q(gam ray) U(1.0):3.338E-02 U(4.0) Occ(FarIR):2.609E-08 Occ(H n=6) Tbr(FarIR):4.375E-08 Tbr(H n=6)	05=0.9025cm Hi-Con:3.99E+00 Ry u:1.385E+00 P(X-ray): 0.000): 12.0419 Q(4.0-20): 0.000): 0.0000 L(Infred): 1.499):0.000E+00 T(En-Den):4.57LE+():1.204E-11 Occ(1Ryd):2.456E-1):5.348E-08 Tbr(1Ryd):3.67PE-():1.960E-22 Grain Mg2:3.617E-2	00 P(Ba1C): 2.8173 00 Q(20): 0.0000 6 Alf(cox): 0.0000 11 T(Comp): 3.542E+04 .4 Occ(4R): 0.000E+00 9 Tbr(4R): 0.000E+00	E(hi): 100.01 MeV Q(Balmer C): 13.6996 Ion pht flx:1.001E+13 Total lumin: 2.9957 nuJnu(912A):5.336E+02 Occ (Nu-hi):6.473E-22 Tbr (Nu-hi):4.050E-16 Grain(HeII):3.532E-22
##### 1 Te:8.609E+03 Hden:1.000E+04 Ne:1.0	097E+04 B:1.000E+25 B-B0:2.573E+	15 dB 5, 145E+15 NTR: 3 H	Lot:2.969E=16 T912: 4.824E+01###
	49 0.00 6584 0.01 5007 1.59 3		
Hydrogen 1.249E-04 9.999E-01 H+0/Hden: 1	1.000E+00 2.403E-12 H- H2 4.	772E-15 6.261E-13 H2+ He	H+ 1.025E-12 H col den 5.145E+19
H 2SP 3-6 2.408E-10 3.462E-14 1.732E-16 1	1.582E-16 1.850E-16 2.178E-16 Te	exc(La); 5.120E+03 T(contn): 4.515E+01 T(diffs): 4.101E+01
			ct 1.000E+00 Gam 1/tot 1.000E+00
			15 8.030E-18 6.301E-17 1.022E-17
	0.000E+00 0.000E+00 0.000E+00 0.		
			g: 2.559E-17 Frac(tot) 8.619E-02
			g: 3.160E-17 Frac(tot) 1.064E-01
	2.476E-08 P(gas): 2.449E-08 P(2.949E-04 0.000E+00 0.000E+00 0.		el 1.229E-05 Force Mul 1.182E+03
			1: 0.000E+00 O2+/Otot: 0.000E+00
			00 Hex(tot): 0.000E+00 A:-12.430
	0.000E+00 0.000E+00 0.000E+00 0.		
Magnesium 0 4.660E-06 8.217E-03 9.918E-01 0			
Aluminium 0 1.007E-06 1.779E-02 5.674E-01 4	4.148E-01 0.000E+00 0.000E+00 0.	000E+00 0.000E+00 0.000E+	00 0.000E+00 0.000E+00 0.000E+00
Silicon 0 1.241E-07 6.151E-03 7.650E-01 2	2.288E-01 6.719E-05 0.000E+00 0.	000E+00 0.000E+00 0.000E+	00 0.000E+00 0.000E+00 0.000E+00
Sulphur 0 0.000E+00 6.597E-03 9.101E-01 8	8.333E-02 0.000E+00 0.000E+00 0.	000E+00 0.000E+00 0.000E+	00 0.000E+00 0.000E+00 0.000E+00
Argon 0 9.205E-07 2.267E-02 9.699E-01 7			
Calcium 0 9.758E-05 1.372E-02 9.861E-01 5			
Iron 0 0.000E+00 1.545E-04 7.461E-02 9			
##### 98 Te:3.877E+03 Hden:8.261E+04 Ne:1.4			
0.49 4686 0.00 5876 0.13 1909 0.70 154			
Hydrogen 9.833E-01 1.673E-02 H+0/Hden: 1 H 2SP 3-6 2.658E-10 2.145E-13 1.002E-16 1			H+ 6.165E-11 H col den 1.528E+21): 3.408E+01 T(diffs): 4.136E+01
			t 1.000E+00 Gam 1/tot 1.000E+00
He singlet 0.000E+00 0.000E+00 0.000E+00 0			
	0.0001.00 0.0001.00 0.0001.00 He	. SITETS STORE (0.000 E)	55 5.5551.55 5.5501.00 0.0001.00

HeII	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	PRAD/GAS;	2.425E-03	
Gra-Ori	Dust temp	1.259E+02	Pot(Volt)	2.210E+00	Nelectron	4.605E+02	drft cm/s	1.566E+04	Heating:	1.261E-17	Frac(tot)	2.607E-01
Sil-Ori	Dust temp	1.024E+02	Pot(Volt)	2.263E+00	Nelectron	4.714E+02	drft cm/s	1.328E+04	Heating:	1.456E-17	Frac(tot)	3.009E-01
Pressure	NgasTgas;	3.921E+08	P(total):	5.433E-08	P(gas):	5.413E-08	P(Radtn):	2.033E-10	Rad accel	3.330E-06	Force Mul	6.637E+04
Carbon	4.039E-05	9.998E-01	2.079E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen	9.656E-01	3.436E-02	7.416E-16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/Ototl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9.857E-01	1.432E-02	5.933E-16	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.216
Neon	9.520E-01	4.801E-02	2.156E-11	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Magnesium O	1.821E-04	9.993E-01	4.728E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Aluminium 0	2.664E-05	9.993E-01	6.348E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Silicon 0	2.901E-05	1.000E+00	2.268E-06	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Sulphur 0	1.058E-05	9.946E-01	5.421E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Argon 0	9.199E-01	8.012E-02	3.351E-14	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Calcium 0	7.468E-06	1.345E-02	9.865E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Iron 0	5.286E-04	9.995E-01	1.587E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Calculati	on stopped	because 1	owest Te re	eached.								
	is plane-pa											
FeII-MgII	photoionia	zation of 1	H N=2 reach	ned 3.3 p	percent of	the total	rate out.					
	zation of H											
	s+line rad							pressure mo	odel.			
	in-gas phot						1.					
	in photoele											
	in-gas cool					otal.						
	Frequency out of range of free-free gaunt factor routine.											
Balmer continuum optical depth is 1.04E+00												
	Balmer continuum stimulated emission correction to optical depths reached 0.14											
Paschen c	ont optical	L depth=	4.80E-01									

**************************************	*****
* title conditions similar to Orion nebula blister	*
* sphere	*
* table star kurucz 39,700K	*
* phi(h) 13.0	*
* turbulence 8 km/sec	*
* hden 4	*
* abundances hii region	*
* constant pressure	*
* iterate	*
* print last iteration	*
* c orion.in	*
* c cray	*
**************************************	*****

Emission Line Spectrum. Constant Pressure Model. Closed geometry. Iteration 2 of 2. Intensity (erg/s/cm^2)

TOTL 4861 0.487	1.0000	BA C 0 1.081	3.9313	C 3 1909 0.021	0.3425	Si 2 1808 -3.233	0.0002
TOTL 1216 1.248	5.7728	PA C 0 0.570	1.2124	Phot 1909 -1.495	0.0104	Si 3 1207 -2.609	0.0008
TotH 0 1.775	19.4001	Grai 0 2.493	101.5280	N 2 6584 0.217	0.5372	Si 3 1895 -0.982	0.0340
BFH1 0 1.689	15.9133	Grai 1216 1.992	32.0084	N 2 6548 -0.260	0.1791	PHOT 1895 -3.015	0.0003
BFHe 0 0.598	1.2914	H FF 0 0.583	1.2491	REC 6584 -2.609	0.0008	Si 4 1397 -3.067	0.0003
TotM 0 -0.442	0.1178	н ғв 0 0.802	2.0684	N 2 5755 -1.406	0.0128	S 2 6720 -0.850	0.0460
н- н 0 -3.337	0.0001	Cool 1216 -0.587	0.0843	N 2 122 -2.928	0.0004	S 2 4074 -1.009	0.0319
GraH 0 0.804	2.0774	Crst 960 -3.252	0.0002	N 2 4239 -3.156	0.0002	S 210330 -1.183	0.0214
GraC 0 0.485	0.9948	H-FB 0 -3.262	0.0002	N 2 5680 -2.609	0.0008	S II 6731 -1.018	0.0313
CA B 4861 0.463	0.9474	HeFF 0 -0.463	0.1122	N 2 2140 -1.326	0.0154	S II 6716 -1.344	0.0148
CA B 1216 1.995	32.2256	HeFB 0 -0.318	0.1565	N 2 1084 -3.144	0.0002	S II 4070 -1.132	0.0240
DU B 4861 0.456	0.9304	MeFB 0 -2.712	0.0006	N 3 1750 -1.113	0.0252	S II 4078 -1.617	0.0079
O(H) 4861 0.677	1.5492	MeFF 0 -1.991	0.0033	N 3 57 -1.074	0.0275	S II10323 -1.635	0.0075
Q(H) 1216 2.211	52.9687	TOFF 0 0.622	1.3647	0 1 6300 -1.756	0.0057	S II10289 -1.764	0.0056
TOTL 6563 0.934	2.7990	He I 4471 -0.890	0.0419	0 1 6363 -2.233	0.0019	s II10205 -11704 s II10373 -2.087	0.0027
TOTL 4861 0.487	1.0000	TOTL 5876 -0.400	0.1297	0 1 630 -2.786	0.0005	S II10373 -2:087 S II10339 -1.767	0.0027
TOTL 4340 0.186	0.5001	Ca B 5876 -0.443	0.1174	0 1 7774 -2.711	0.0005	S 3 18 0.031	0.3503
TOTL 4102 -0.047	0.2927	TOTL10830 0.213	0.5327	TOTL 3727 0.661	1.4940	S 3 34 -0.736	0.0599
TOTL18751 -0.064	0.2927	INWD10830 -0.078	0.2727	TOTL 7325 0.006	0.3301	S 3 9532 0.695	1.6152
TOTL12818 -0.343	0.1480	TOTL 3889 -1.072	0.2727	IONZ 3727 -2.459	0.0011	S 3 9069 0.279	0.6201
	0.0879	TOTL 7065 -0.628	0.0278	IONZ 7325 -2.648	0.00011	S 3 6312 -0.966	0.0352
TOTL10938 -0.569 TOTL40512 -0.754	0.0879		1.0060		0.0007	S 3 6312 -0.966 S 3 3722 -1.195	0.0352
	0.0363		0.0266		1.1156		0.0208
TOTL26252 -0.953							
TOTL74578 -1.283	0.0170	DevB 2 -1.408	0.0127	O II 2471 -0.096	0.2613	S 3 1729 -2.049	0.0029
2 NU 0 1.244	5.7231	He I 5016 -1.141	0.0235	O II 7323 -0.252	0.1823	S 4 105 -0.708	0.0639
TOTL 1216 1.248	5.7728	DevB 5016 -1.259	0.0179	O II 7332 -0.343	0.1479	Ar 2 7 -1.530	0.0096
TOTL 1026 -1.621	0.0078	He I 3965 -1.434	0.0120	0 2 4651 -2.389	0.0013	Ar 3 7135 -0.131	0.2412
TOTL 973 -1.704	0.0064	DevB 3965 -1.672	0.0069	0 3 1663 -1.289	0.0167	Ar 3 7751 -0.761	0.0566
TOTL 950 -1.691	0.0066	He I 3614 -1.718	0.0062	O 3 5007 1.043	3.5994	Ar 3 22 -1.543	0.0093
TOTL 938 -1.652	0.0073	DevB 3614 -1.852	0.0046	O 3 4959 0.566	1.1998	Ar 3 9 -0.316	0.1576
C13c 6563 -2.638	0.0008	He I 3448 -1.937	0.0038	TOTL 4363 -1.235	0.0190	Ar 4 4740 -2.924	0.0004
CION 0 -2.592	0.0008	DevB 3448 -2.159	0.0023	0 3 2321 -1.862	0.0045	Ca 2 3933 -2.780	0.0005
INWD 1216 1.243	5.7059	REC 1656 -2.851	0.0005	O 3 880 -1.167	0.0222	Ca 2 7306 -2.324	0.0015
INWD 6563 0.633	1.3988	C I 9850 -3.275	0.0002	O 3 520 -0.256	0.1806	Ca2K 3934 -2.962	0.0004
INWD 4861 0.186	0.4996	C 2 158 -3.032	0.0003	Ne 2 128 0.365	0.7561	Ca2H 3969 -3.243	0.0002
INWD18751 -0.366	0.1405	C 2 2326 -0.363	0.1413	Ne 3 156 -0.093	0.2633	CaF1 7291 -2.549	0.0009
Dest 1216 1.973	30.6246	INWD 2326 -0.664	0.0706	Ne 3 361 -1.286	0.0169	CaF2 7324 -2.718	0.0006
Dest 6563 -0.834	0.0477	C 2 1335 -1.622	0.0078	Ne 3 3869 -0.410	0.1268	Fe 2 7 -1.795	0.0052
Dest 4861 -2.615	0.0008	REC 1335 -0.329	0.1527	Ne 3 3968 -0.923	0.0389	Emis 3 -1.518	0.0099
e sc18751 -1.466	0.0112	C 2 4267 -2.135	0.0024	Ne 3 1815 -3.380	0.0001	Cool 3 -1.477	0.0109
e sc40512 -2.698	0.0007	TOTL 977 -2.018	0.0031	Emis 2798 -0.194	0.2083	TOT 0 -1.328	0.0153

nFnu 4860 0.881 2.4768	C3 C 977 -2.021	0.0031	Cool 2798 0.165 (0.4770 FEIR 0 -2.631	0.0008
nFnu 1215 -1.268 0.0176	TOTL 1909 0.333	0.7009	Al 3 1860 -2.277 (0.0017 Fe 3 0 -1.085	0.0268
Inci 4861 1.608 13.2183	INWD 1909 0.030	0.3490	Si 2 35 -2.647 (D.0007 Fe 3 5270 -1.765	0.0056
Inci 1216 2.919 270.6663	C 3 1907 0.041	0.3585	Si 2 2335 -2.157 (D.0023 Fe 3 4658 -1.521	0.0098

CONDITIONS SIMILAR TO ORION NEBULA BLISTER 0:0.051 H FF 0:0.064 H FB 0:0.106 CCHE 0:0 0:0.820 BFHe 0:0.067 GraH 0:0.107 Cooling: GraC Heating: BFH1 0:0.052 TOTL 3727:0.077 O 3 5007:0.185 S 3 9532:0.083 U(1-) -1.4765 U(4-):-37.0000 U(sp): -2.39 Q(ion): 7.012 L(ion): -3.411 Q(low): 13.47 Heat: 1.775 Coolg: 1.775 Error: 0.1% Compt H: -4.819 WorkF: 2.292 F-F H -9.396 H12:1.528E+21 H II:1.52E+21 HI:7.533E+18 H-: 1.532E+11 H2: 2.631E+11 H2+:6.702E+10 OH: 0.000E+00 Heff:0.000E+00 TONTZE PARMET: P(low) 2.49 PRADMX:2.55E=02 ENERGY BUDGET : He H+:5.312E+10 Column density <NH>:1.317E+04 <TO3>:9.07E+03 Ne:1.350E+04 ti(snd):1.05E+11 NeN+dl:2.24E+25 <T(C3)>:9.39E+03 <E(C3)>:1.45E+04 <Tp>:9.46E+03 He/Ha:9.59E-02 T He+:9.42E+03 <a>:0.00E+00
 101*true
 N/Oap:1.05E-01
 =
 0.60true
 T(O3R):9.269E+03

 EHe+1.46E+04
 T(O+):9.84E+03
 EO+11.60E+04
 iter/zn:
 2.900

 erdeF0.0E+00
 Tcompt1.99E+06
 Thr1.37E+08
 <Tden>: 9.45E+03

 l(cm)1.25E+19
 M(sun)9.71E+04
 smallest:
 len(cm):7.98E+18

 L THIN:1.00F+30 <T(S2)>:9.83E+03 <E(S2)>:1.59E+04

 Te-low:3.88E+03 Te-high:1.06E+04 Hlu/zn:3.86E+00

 <dens>:3.05E-20 <Mol>:6.39E-01

 M(sun):2.55E+04 Alf(ox-tran):
 0.0000
 = 1.01*true EHe+:1.46E+04 Mean Jeans L(dust): 2.493E+00 L(dust): 2.493E+00 Gra-ISM Sil-ISM Gra-Ori Sil-Ori Sil-0.01 Sil-0.1 SilicatP <Tdust>: 0.000E+00 0.000E+00 1.572E+02 1.227E+02 0.000E+00 0.000E+00 0.000E+00 <Vel D>: 0.000E+00 0.000E+00 5.985E+04 4.910E+04 0.000E+00 0.000E+00 0.000E+00 <Pot D>: 0.000E+00 0.000E+00 1.527E+00 1.615E+00 0.000E+00 0.000E+00 SilicatPN CONTN; COMP: 5.52E-04 H-: 2.99E-06 R(1300): 5.05E-05 H2+ 4.69E-07 HeTri:1.17E+00 Pa:1.12E-01 Ba:5.67E-01 Hb:7.55E-01 La:1.24E+00 1r:4.847E+01 1.8:6.21E+01 4. 3889: 2.18E+01 5876: 5.70E-05 7065: 3.14E-05 2800: 1.24E+03 774: 1.00E-20 1240: 1.00E-20 1035: 1.00E-20 1335: 2.71E+03 977 1207: 1.42E+03 1085: 1.85E+02 1194: 2.38E+01 1909: 2.11E-02 1895: 3.80E-02 2326 1025: 1.02E+01 352: 1.00E-20 347: 1.00E-20 1860: 6.45E+01 630: 1.00E-20 1256: 7.59E+00 -3: 8.36E-01 100 Optical Depths: CONTN; COMP: 5.52E-04 Pfa:2.39E-02 10830: 5.12E+02 1550: 1.80E+00 4.:1.000E-20 21R:1.000E-20 977: 5.29E+04 1397: 6.40E+01

 1035:
 1.00E-20
 1335:
 2.71E+03
 9/7:
 5.29E+04

 1909:
 2.11E-02
 1895:
 3.80E-02
 2326:
 1.36E-03

 1860:
 6.45E+01
 630:
 1.00E-20
 834:
 1.90E+04

 3934:
 5.93E-01
 3969:
 2.99E-01
 8498:
 9.53E-06

 990:
 2.37E+03
 1402:
 1.00E-20
 1214:
 1.00E-20

 8727:
 2.52E-09
 6300:
 9.22E-08
 5577:
 1.61E-09

 789: 1.00E-20 1666: 4.62E-02 1750: 5.37E-04 835: 2.25E+03 -3: 8.36E-01 1304: 3.48E+01 1656: 5.44E-01 1808: 1.07E+02 1256: 7.59E+00 -48: 8.43E-08 8542: 8.54E-05 1122: 9830: 1.61E+01 9.07E-11 8662: 4.84E-05 2335: 2.55E-04 353: 1.00E-20 1406: 3.20E-03 1486: 1.20E-06 7291: 3.97E-08 1039: 4.94E+00 -8446: 3.08E-13 -4368: 765: 7.32E-01 -1198: 1.00E-20 786: 7324: 2.75E-08 1.90E-15 -132: 1.59E-13 -113: 2.52E-13 -29: 7.45E-15 -46: 5.95E-13 -245: 1.00E-20 786: N57: NE16: 1.00E-20 -245: 1.00E-20 765: 7.32E-01 -1198: 1.00E-20 786: 1.00E-20 C157: 8.63E-05 N122: 6.12E-05 N205: 2.63E-05 N57: 3.00E-03 0146:-6.13E-05 063: 4.17E-04 088: 1.82E-03 026: 1.00E-20 NE13: 3.23E-02 NE36:-6.69E-04 NE16: 7.98E-03 MG4: 1.00E-20 MG14: 1.00E-20 MG6: 1.00E-20 S19: 2.26E-03 S34: 6.81E-04 S11: 1.59E-04 AR7: 1.37E-04 AR9: 1.37E-03 AR22:-5.39E-05 AR13: 1.00E-20 CA3: 9.99E-11 CA12: 1.00E-20 CA4: 1.00E-20 Ne14: 1.00E-20 Ne14: 1.00E-20 S3: 1.00E-20 S14: 1.00E-20 S14: 1.00E-20 Fe61: 1.00E-20 Fe23: 1.00E-20 Fe13: 1.00E-20 S12.5: 1.00E-20 S16.5: 1.00E-20 C610: 8.45E-07 C370: 3.91E-06 052: 1.25E-02 SI35: 7.33E-06 AR8: 1.00E-20 Fe7: 1.00E-20 01d hydro optical depths: 1 4.82E+01 Lines: 2-1 4.06E+05 New hydro optical depths: 1 4.82E+01 Lines: 2-1 2.04E+05 2 5.29E-01 3-2 5.54E-02 3 2.44E-01 4 1.20E-01 4-3 2.78E-08 5-4 2.08E-08 5 5.84E-02 6-5 3.32E-09 6 3.10E-02 7-6 2.16E-07 7 1.00E-02 8-7 2.84E-06 2 5.20E-01 3-2 2.78E-02 3 2.40E-01 4 1.18E-01 4-3 1.53E-08 5-4 1.14E-08 5 5.74E-02 6-5 2.58E-09 6 3.05E-02 7 9.87E-03 7-6 1.09E-07 8-7 1.44E-06

 Old He Is optical depths:
 1 3.07E+01
 2 2.93E-01
 3-1.95E-15
 4-6.96E-15
 5-1.41E-14
 6-2.48E-14
 7-2.78E-13

 Lines:
 2-1
 1.58E+05
 3-2
 1.07E-02
 4-3
 8.24E-10
 5-4
 3.93E-10
 6-5-5.33E-11
 7-6
 6.14E-09
 8-7
 8.08E-08

 New HE Is optical depths:
 1 3.13E+01
 2 2.82E-01
 3-1.97E-15
 4-7.02E-15
 5-1.42E-14
 6-2.50E-14
 7-2.80E-13

 Lines:
 2-1
 1.62E+05
 3-2
 1.07E-02
 4-3
 8.30E-10
 5-4
 3.97E-10
 6-5-9.78E-11
 7-6
 6.17E-09
 8-7
 8.13E-08

 Old He II optical depths:
 1
 9.43E+01
 2
 2.41E+01
 3
 5.00E-21
 4
 5.00E-21

 Lines:
 2-1
 1.00E+00
 3-2
 1.00E-20
 3-4
 1.00E-20
 5-4
 1.00E-20

 New HE II optical depths:
 1
 8.71E+01
 2
 2.41E+01
 3
 5.00E-21
 4
 5.00E-21

 Lines:
 2-1
 1.00E-20
 3-2
 1.00E-20
 4-3
 1.00E-20
 5-4
 1.00E-21
 5 5.00E-21 6 5.00E-21 7 5.00E-21 6-5 1.00E-20 7-6 1.00E-20 8-7 1.00E-20 5 5.00E-21 6 5.00E-21 7 5.00E-21 6-5 1.00E-20 7-6 1.00E-20 8-7 1.00E-20 Hydrogen -2.307 -0.002 Helium -1.306 -0.022-30.000 Log10 Mean Ionisation (over volume)

Helium -1.306 -0.022-30.000 Carbon -4.603 -0.982 -0.048 -4.109 Nitrogen -2.899 -0.785 -0.078 -4.092 Oxygen -2.314 -0.304 -0.302 Neon -2.297 -0.075 -0.816 Magnesium -3.648 -1.212 -0.028 Aluminum -4.482 -0.871 -0.175 -0.707

-5.235 -1.201 -0.079 -0.984 -4.809

Silicon

Sulphur Argon Calcium Iron 5 7 1 2 3 Λ 6 8 9 10 11 12 13 14 15 16 17 Hydrogen -2.307 -0.002 Helium -1.306 -0.022-30.000 Carbon -4.603 -0.982 -0.048 -4.109 Nitrogen -2.899 -0.785 -0.078 -4.092 Oxygen -2.314 -0.304 -0.302 Log10 Mean Ionisation (over radius) Oxygen Neon -2.297 -0.075 -0.816 Magnesium -3.648 -1.212 -0.028 Aluminum -4.482 -0.871 -0.175 -0.707 Silicon -5.235 -1.201 -0.079 -0.984 -4.809 -5.895 -1.384 -0.034 -1.460 -2.604 -0.906 -0.060 -2.662 -2.840 -1.385 -0.019 -4.876 -3.989 -1.783 -0.541 -0.158 Sulphur Argon Calcium Iron Normalised continuum 0.36 0.657 0.39 0.622 0.43 0.590 0.88 0.401 0.96 0.414 0.98 0.416 0.25 1.100 0.27 0.915 0.30 0.784 0.33 0.707 0.62 0.420 0.67 0.404 0.74 0.381 0.81 0.387 0.47 0.551 0.51 0.497 0.56 0.448 0.99 0.417 1.00 0.417 Emergent continuum - phot/ryd/cm2 (r in) 0.9 2.30E+13 1.0 1.97E+13 2.86E+00 2.29E-02 3.22E+00 1.39E-01 0.47 4.24E+13 0.53 3.65E+13 0.26 6.49E+13 0.29 5.39E+13 1.6 4.68E+06 1.8 9.80E+07 1.0 3.52E+07 1.0 2.71E+07 2.0 9.93E+00 2.3 6.67E-01 2.5 2.64E-02 0.33 4.93E+13 0.60 3.24E+13 0.67 2.92E+13 1.0 1.23E+13 1.0 1.06E+13 1.1 2.00E+06 3.63E+00 3.04E-01 0.37 4.72E+13 1.2 5.56E+04 3.89E+00 8.14E-01 0.42 4.49E+13 0.76 2.55E+13 1.0 4.57E+07 1.4 3.34E+04

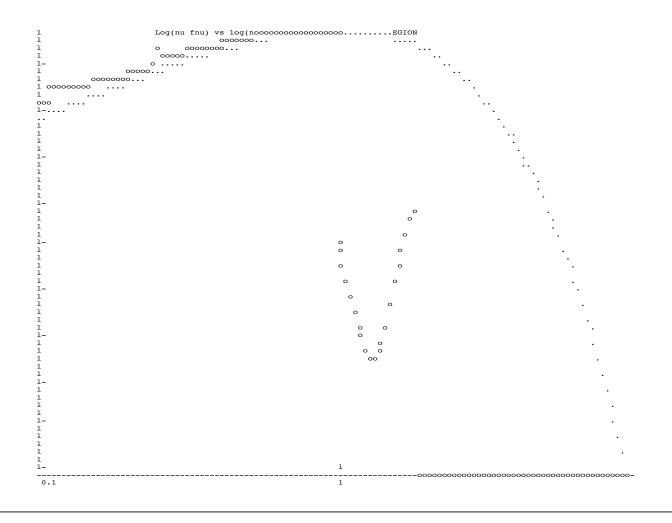
*	
* title "New" Paris meeting HII region	
* c "standard" HII region model of the Pequignot Meudon Conferance	
* sphere	
* black body, T=40,000K radius = 12.113943	
* hden = 2	
* radius = 18.477121	
* abund -1 C-3.6576 N-4.39794 O-3.481146 ne-4.30103 mg-8 al=-8	
* continue si-8 s-5.04576 ar-8 ca=-8 fe-8	
* plot continuum .1	
* iterate ; must iterate since fine structure lines are opticall thick	
* print last	
* c parishii.in	
* c cray	
*	

Chemical composition He:.100 C:2.20E-04 N:4.00E-05 O:3.30E-04 Ne:5.00E-05 Mg:1.00E-08 Al:1.0E-08 S:9.00E-06 A:1.0E-08 Ca:1.0E-08 Fe:1.00E-08

He:.100 C:2.20E-04 N:4.00E-05 O:3.30E-04 Ne:5.00E-05 Mg:1.00E-08 A1:1.0E-08 S1:1.00E-08 S:9.00E-06 A:1.0E-08 Ca:1.0E-08 Fe:1.00E-08
326Cell Peak9.65E-01 Lo 1.00E-05=0.9105cm Hi-Con:9.38E+00 Ryd E(hi):7.35E+06Ryd E(hi): 100.01 MeV
P(nu>1ryd): 39.1048 Average nu:1.370E+00 P(X-ray): 0.0000 P(BalC): 39.2323 Q(Balmer C): 50.1283
Q(1.0-1.8): 49.5803 Q(1.8-4.0): 48.6622 Q(4.0-20): 45.5292 Q(20): 0.0000 Ion pht flx:3.770E+11
L(gam ray): 0.0000 Q(gam ray): 0.0000 L(Infred): 38.0134 Alf(ox): 0.0000 Total lumin: 39.4890
L/Lsolar: 5.9062 Abs bol mg: -10.0455 Abs V mag: -6.3924 Bol cor: -3.6531 nuFnu(Bbet): 38.1136
U(1.0):1.258E-01 U(4.0):9.976E-06 T(En-Den):1.862E+01 T(Comp):3.830E+04 nuJnu(912A):2.006E+01
Occ(FarIR):1.129E-09 Occ(H n=6):4.006E-13 Occ(1Ryd):9.248E-16 Occ(4R):6.369E-21 Occ (Nu-hi):6.544E-30
Tbr(FarIR):1.877E-09 Tbr(H n=6):1.779E-09 Tbr(1Ryd):1.461E-10 Tbr(4R):4.029E-15 Tbr (Nu-hi):9.547E-24
1 Te:6.512E+03 Hden:1.000E+02 Ne:1.115E+02 R:3.004E+18 R-R0:3.795E+15 dR:7.591E+15 NTR: 3 Htot:2.611E-20 T912: 4.023E+01###
-4,68,4686 0.08,5876 0.10 1909 0.01 1549 0.00 6584 0.00 5007 1.14 3727 0.01 6300 0.00 2798 0.00 1035 0.00
Hydrogen 2.968E-05 1.000E+00 H+0/Hden: 1.000E+00 2.747E-15 H- H2 9.992E-17 5.027E-14 H2+ HeH+ 5.753E-14 H col den 7.591E+17
H 2SP 3-6 2.090E-12 2.632E-18 6.672E-19 7.923E-19 1.089E-18 1.503E-18 Texc(La); 3.797E+03 T(contn): 1.854E+01 T(diffs): 2.626E+02
Helium 1.703E-04 8.650E-01 1.349E-01 He I 2S3 2.421E-07 Comp H, C 5.224E-26 8.883E-27 Fill Fact 1.000E+00 Gam 1/tot 1.000E+00
He singlet 1.701E-04 5.103E-13 1.399E-19 1.813E-19 2.526E-19 3.457E-19 He triplt 2.421E-07 4.584E-18 4.872E-20 4.317E-19 1.165E-19
HeII 8.650E-01 8.047E-14 2.180E-20 3.347E-20 5.389E-20 8.337E-20 7.416E-19 8.133E-18 1.687E-15 PRAD/GAS; 1.088E-02
Pressure NgasTgas; 1.358E+06 P(total): 1.895E-10 P(gas): 1.875E-10 P(Radtn): 2.040E-12 Rad accel 3.261E-08 Force Mul 1.133E+02
Carbon 0.000E+00 5.129E-03 9.118E-01 8.304E-02 2.792E-05 0.000E+00 0.000E+00 H20+/Otot 0.000E+00 OH+/Ototl 0.000E+00
Nitrogen 2.156E-07 5.877E-03 8.882E-01 1.059E-01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 2.760E-07 2.011E-02 9.379E-01 4.196E-02 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Hex(tot): 0.000E+00 A:-12.437
Neon 4.023E-06 3.303E-02 9.630E-01 4.001E-03 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 Macnesium 0 4.532E-07 2.222E-03 9.976E-01 1.311E-04 0.000E+00
Magnesium 0 4.532E-0/ 2.222E-03 9.9/0E-01 1.311E-04 0.000E+00
Alumining 0.000E+00 1.961E-05 5.066E-01 5.912E-01 0.000E+00 000E+00 0.000E+00 000E+00 000E+00 000E+00 000E+00 000E+00 000E+00 000E+00 000E+00 000E+00 00E+000E+000E+000E+000E+00
Sulphur 0.0000F400 1.292E-03 6.660E-01 3.878E-01 4.902E-03 0.000E+00 000E+00 0.000E+00 0.000E+000E+
Argon 0 0.000E+00 6.215E-03 7.313E-01 2.619E-01 6.110E-04 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Calcium 0 1.102E-05 4.082E-03 9.517E-01 4.14E-02 1.955E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
Iron 0 0.000E+00 1.286E-05 2.084E-02 9.308E-01 4.834E-02 1.723E-05 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
#####110 Te:3.810E+03 Hden:1.000E+02 Ne:5.469E+00 R:1.463E+19 R-R0:1.163E+19 dR:6.607E+14 NTR: 4 Htot:3.095E-22 T912: 8.044E+01###
-0.74 4686 0.00 5876 0.12 1909 0.11 1549 0.00 6584 0.60 5007 1.62 3727 2.43 6300 0.01 2798 0.00 1035 0.00
Hydrogen 9.456E-01 5.444E-02 H+0/Hden: 1.000E+00 7.555E-09 H- H2 3.703E-08 2.186E-09 H2+ HeH+ 7.418E-11 H col den 1.163E+21
H 2SP 3-6 3.118E-13 2.143E-16 9.240E-20 1.498E-19 2.589E-19 4.333E-19 Texc(La); 2.955E+03 T(contn): 7.380E+00 T(diffs): 3.255E+02
Helium 1.000E+00 0.000E+00 0.000E+00 He I 2S3 0.000E+00 Comp H, C 4.610E-29 7.081E-30 Fill Fact 1.000E+00 Gam 1/tot 1.000E+00
He singlet 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 He triplt 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
HeII 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 PRAD/GAS; 2.186E-02

Pressure	Nasamasa.	4 0592+05	D(total).	7 0928 11	D(cac).	6 9/58 11	D(Badtn).	2 2768 12	Rad accol	2.035E-10	Force Mul	5 920 2 + 02
												J.039E+02
Carbon										OH+/Ototl		
Nitrogen	9.711E-01	2.887E-02	2.597E-15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/0totl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9.532E-01	4.682E-02	7.083E-15	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.215
Neon	8.562E-01	1.438E-01	1.116E-10	0.000E+00								
Magnesium O	2.988E-04	9.974E-01	2.328E-03	0.000E+00								
Aluminium O	4.590E-05	9.978E-01	2.159E-03	0.000E+00								
Silicon 0	4.808E-05	9.999E-01	6.979E-06	0.000E+00								
Sulphur 0	1.800E-05	9.826E-01	1.737E-02	0.000E+00								
Argon 0	7.679E-01	2.321E-01	6.940E-13	0.000E+00								
Calcium 0	2.146E-05	2.294E-02	9.770E-01	0.000E+00								
Iron 0	8.460E-04	9.991E-01	5.424E-05	0.000E+00								
Calculation stopped because lowest Te reached.												
Geometry	Geometry is spherical.											
Photoioni	Photoionization of He 2TriS reached 2.9 percent of the total rate out.											

Photoionization of He 2Tris reached 2.9 percent of the total rate out Some fine struc lines are optically thick, largest=7.02E-01 Frequency out of range of free-free gaunt factor routine.



		Luminosity (erg/s)	emitted by	shell with full co	verage.		
TOTL 4861 37.310	1.0000	PA C 0 37.407	1.2508	C 2 1335 34.916	0.0040	0 3 5007 37.518	1.6163
TOTL 1216 38.679	23.4002	H FF 0 37.334	1.0577	REC 1335 36.324	0.1032	0 3 4959 37.041	0.5388
Toth 0 38.499	15.4491	H FB 0 37.507	1.5756	C 2 4267 34.490	0.0015	TOTL 4363 34.921	0.0041
BFH1 0 38.460	14.1209	Cool 1216 36.286	0.0946	TOTL 977 34.292	0.0010	0 3 2321 34.294	0.0010
BFHe 0 37.405	1.2447	Crst 960 33.560	0.0002	C3 R 977 34.273	0.0009	0 3 880 37.383	1.1839
TotM 0 36.230	0.0833	H-FB 0 33.758	0.0003	TOTL 1909 36.344	0.1081	0 3 520 37.346	1.0880
н- н 0 33.535	0.0002	H2+ 0 33.478	0.0001	INWD 1909 36.035	0.0532	0 4 26 34.166	0.0007
CA B 4861 37.313	1.0067	HeFF 0 36.205	0.0786	C 3 1907 36.125	0.0653	Ne 2 128 36.672	0.2301
CA B 1216 38.839	33.8374	HeFB 0 36.387	0.1194	C 3 1909 35.941	0.0428	Ne 3 156 36.963	0.4500
DU B 4861 37.313	1.0067	MeFB 0 33.963	0.0005	C3 R 1909 34.111	0.0006	Ne 3 361 35.896	0.0385
O(H) 4861 37.307	0.9926	MeFF 0 34.577	0.0019	Phot 1909 35.135	0.0067	Ne 3 3869 36.261	0.0894
Q(H) 1216 38.840	33.9366	TOFF 0 37.366	1.1381	C 3 2297 33.767	0.0003	Ne 3 3968 35.748	0.0274
TOTL 6563 37.739	2.6838	He I 4471 35.900	0.0390	C 4 1549 33.333	0.0001	Emis 2798 33.534	0.0002
TOTL 4861 37.310	1.0000	TOTL 5876 36.375	0.1163	N 1 5200 34.463	0.0014	Cool 2798 33.534	0.0002
TOTL 4340 37.018	0.5110	Ca B 5876 36.364	0.1133	REC 5200 33.455	0.0001	si 2 35 33.350	0.0001
TOTL 4102 36.793	0.3045	TOTL10830 36.631	0.2094	N 2 6584 37.089	0.6014	s 2 6720 36.774	0.2910
TOTL18751 36.752	0.2769	INWD10830 36.111	0.0633	N 2 6548 36.612	0.2005	S 2 4074 35.441	0.0135
TOTL12818 36.487	0.1506	TOTL 3889 36.130	0.0662	REC 6584 33.922	0.0004	s 210330 35.268	0.0091
TOTL10938 36.270	0.0913	TOTL 7065 35.676	0.0232	N 2 5755 35.178	0.0074	S II 6731 36.407	0.1250
TOTL40512 36.076	0.0584	CcHE 0 35.765	0.0285	N 2 122 35.814	0.0319	S II 6716 36.530	0.1661
TOTL26252 35.886	0.0377	He I 2 35.700	0.0245	N 2 203 35.347	0.0109	S II 4070 35.318	0.0102
TOTL74578 35.556	0.0176	DevB 2 35.620	0.0204	N 2 5680 33.862	0.0004	S II 4078 34.835	0.0034
2 NU 0 38.335	10.5888	He I 5016 35.641	0.0214	N 2 2140 35.223	0.0082	S II10323 34.815	0.0032
TOTL 1216 38.679	23.4002	DevB 5016 35.614	0.0202	N 3 1750 34.513	0.0016	S II10289 34.686	0.0024
TOTL 1026 35.176	0.0074	He I 3965 35.345	0.0109	N 3 57 36.516	0.1608	S II10205 34.000	0.0011
TOTL 973 35.116	0.0064	DevB 3965 35.277	0.0093	0 1 6300 35.216	0.0081	S II10373 34.305	0.0024
TOTL 950 35.102	0.0062	He I 3614 35.062	0.0057	0 1 6363 34.739	0.0027	S 3 18 37.041	0.5381
TOTL 938 35.096	0.0061	DevB 3614 35.034	0.0053	0 1 630 34.467	0.0014	s 3 34 37.273	0.9192
C13c 6563 34.187	0.0001	He I 3448 34.843	0.0034	0 1 1470 33.438	0.0001	s 3 9532 37.327	1.0417
CION 0 34.184	0.0007	DevB 3448 34.792	0.0030	0 1 7774 34.024	0.0005	S 3 9069 36.912	0.3999
INWD 1216 38.640	21.3947	TOTL 1640 34.337	0.0011	6lev 1304 33.367	0.0001	s 3 6312 35.474	0.0146
INWD 6563 37.437	1.3410	TOTL 4686 33.376	0.0001	TOTL 3727 37.695	2.4298	s 3 3722 35.245	0.0086
INWD 4861 37.009	0.5000	TOTL 1216 33.933	0.0004	TOTL 7325 35.876	0.0368	s 3 1729 34.141	0.0007
INWD18751 36.451	0.1385	Ca B 1640 34.401	0.0012	IONZ 3727 34.748	0.0027	s 4 105 36.343	0.1079
Dest 1216 35.519	0.0162	DevB 1640 34.401	0.0012	IONZ 7325 34.079	0.0006	Ar 3 7135 33.895	0.0004
e sc18751 36.753	0.2772	Ca B 4686 33.621	0.0002	0 II 3729 37.450	1.3805	Ar 3 9 33.924	0.0004
e sc40512 36.077	0.0585	DevB 4686 33.619	0.0002	O II 3726 37.330	1.0466	Ca 2 3933 33.870	0.0004
nFnu 4860 37.777	2.9328	REC 1656 34.207	0.0008	0 II 2471 35.774	0.0291	Ca 2 7306 34.431	0.0013
nFnu 1215 35.066	0.0057	C I 9850 34.379	0.0012	O II 7323 35.618	0.0203	Ca2K 3934 33.684	0.0002
Inci 4861 38.114	6.3672	C 2 158 36.152	0.0695	0 II 7332 35.527	0.0165	Ca2H 3969 33.411	0.0001
Inci 1216 39.299	97.5993	C 2 2326 36.529	0.1656	0 2 4651 34.375	0.00105	CaF1 7291 34.207	0.0001
	- / • 0 / / 0						

"NEW" PARIS MEETING HII REGION Cooling: H FF 0:0.068 H FB 0:0.102 TOTL 3727:0.157 O 3 5007:0.105 O 3 880:0.077 O 3 520:0.070 S 3 9532:0.067 Heating: BFH1 0:0.914 BFHe 0:0.081
IONIZE PARMET: U(1-) -0.9004 U(4-): -5.0011 U(sp): -2.27 Q(ion): 44.552 L(ion): 34.128 Q(low): 50.22 P(low) 39.26 ENERGY BUDGET: Heat: 38.499 Coolg: 38.499 Error: 0.1% Compt H: 31.699 WorkF: 39.074 F-F H 32.553 PRADMX:1.97E-01 Column density H12:1.163E+21 H II:1.157E+21 HI:6.387E+18 H-: 1.571E+11 H2: 2.938E+11 H2+:6.519E+10 He H+:2.089E+10 OH: 0.000E+00 Heff:0.000E+00
<pre><nds:1.000e+02 <tp="">:7.64E+03 <to3>:7.22E+03 Ne:1.101E+02 ti(snd):1.1EE+13 NeN+d1:1.26E+23 <t(c3)>:7.45E+03 <e(c3)>:1.10E+02 He/Ha:8.60E-02 = 0.86*true N/Oap:4.96E-02 = 0.41true T(O3R):7.686E+03 L THIN:1.00E+30 <t(s2)>:8.82E+03 <e(s2)>:9.82E+01 T He+:7.42E+03 EHe+1.10E+02 T(O+):8.46E+03 EO+:1.06E+02 iter/zn: 2.296 Te-low:3.81E+03 Te-high:1.01E+04 H1u/zn:2.94E+00 <a>:0.00E+00 erdeFe0.0E+00 Tcompt7.38E+09 Thtrl.11E+10 <tden>: 7.65E+03 <dens>:2.34E-22 <mol>:6.46E-01 [cm]3.25E+20 M(sun)2.1E+06 = 0]; 0.000</mol></dens></tden></e(s2)></t(s2)></e(c3)></t(c3)></to3></nds:1.000e+02></pre>
Optical Depths: CONTN; COMP: 4.19E-04 H-: 3.06E-06 R(1300): 4.29E-05 H2+ 4.56E-07 HeTri:9.77E-04 Pfa:8.38E-04 Pa:8.38E-04 Ba:8.43E-04 Hb:8.42E-04 La:1.94E-03 lr:4.022E+01 1.8:1.16E+02 4.:4.314E+01 21R:1.000E-20 10830: 4.01E+01 3889: 1.71E+00 5876: 2.04E-08 7065: 1.12E-08
1550: 4.09E+02 2800: 1.23E+00 774: 1.00E-20 1240: 1.00E-20 1035: 1.00E-20 1335: 5.92E+03 977: 7.50E+04 1397: 1.05E+00 789: 4.45E+00 1207: 1.29E+01 1085: 3.14E+02 1194: 6.29E+01 1909: 2.99E-02 1895: 3.45E-04 2326: 2.90E-03 1666: 1.20E-01 1750: 6.15E-04 1025: 2.10E+01 352: 1.00E-20 347: 1.00E-20 1860: 9.21E+00 630: 1.00E-20 834: 2.37E+04 835: 5.82E+03
1808: 1.22E+00 1256: 3.08E+01 -3: 1.58E+02 -48: 7.26E+12 3934: 1.55E+00 3969: 7.82E-01 8498: 1.25E-07 8542: 1.12E-06 8662: 6.36E-07 353: 1.00E-20 1304: 7.20E+01 1122: 2.42E-01 990: 2.71E+03 1402: 5.93E-05 1214: 1.00E-20 1486: 2.70E-04 2335: 2.91E-06 1406: 2.47E-02 1656: 2.58E+00 9830: 4.31E-10 8727: 1.24E-10 6300: 1.91E-07 5577: 1.60E-11 7291: 1.04E-07
7324: 7.18E-08 1039: 1.02E+01 -8446: 1.24E-14 -4368: 5.49E-17 -132: 1.69E-15 -113: 2.68E-15 -29: 8.23E-17 -46: 6.33E-15 -245: 1.00E-20 765: 1.64E+02 -1198: 1.95E-04 786: 5.82E-01
C157: 5.52E-03 N122: 3.52E-03 N205: 7.74E-03 N57: 4.22E-02 0146:-1.26E-05 063: 2.17E-03 088: 7.02E-01 052: 8.88E-02 026: 1.93E-04 NE13: 1.75E-02 NE36:-5.75E-05 NE16: 4.41E-02 MG4: 2.44E-11 MG14: 1.00E-20 MG6: 1.00E-20 S135: 1.39E-06 S19: 1.54E-03 S34: 4.89E-02 S11: 1.97E-03 AR7: 2.38E-06 AR9: 1.43E-05 AR22:-6.51E-09 AR13: 4.40E-10 AR8: 1.05E-13
CA3: 5.58E-08 CA12:-3.94E-17 CA4: 1.66E-12 Ne14: 1.00E-20 Ne24: 1.00E-20 Si3: 1.00E-20 Si4: 1.00E-20 Fe7: 1.00E-20 Fe61: 1.00E-20 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 1.00E-20 Si6.5: 1.00E-20 C610: 2.78E-07 C370: 4.39E-05
Old hydro optical depths: 1 4.02E+01 2 2.96E-06 3 5.82E-06 4 1.64E-06 5 1.10E-13 6 2.74E-13 7 1.01E-12 Lines: 2-1 4.17E+05 3-2 8.89E-04 4-3 1.59E-10 5-4 8.30E-11 6-5-2.16E-10 7-6 2.00E-09 8-7 2.69E-08
New hydro optical depths: 1 4.02E+01 2 3.04E-06 3 5.98E-06 4 1.69E-06 5 1.10E-13 6 2.73E-13 7 1.01E-12 Lines: 2-1 2.08E+05 3-2 4.44E-04 4-3 7.95E-11 5-4 4.18E-11 6-5-1.07E-10 7-6 9.98E-10 8-7 1.34E-08
Old He Is optical depths: 1 5.74E+01 2 6.94E-05 3-2.03E-17 4-6.34E-17 5-1.26E-16 6-2.20E-16 7-2.43E-15 Lines: 2-1 5.46E+05 3-2 4.74E-05 4-3 9.80E-12 5-4 3.58E-12 6-5-8.42E-12 7-6 8.48E-11 8-7 1.14E-09
New HE IS optical depths: 1 5.90E+01 2 7.00E-05 3-2.02E-17 4-6.30E-17 5-1.26E-16 6-2.19E-16 7-2.42E-15 Lines: 2-1 5.63E+05 3-2 4.73E-05 4-3 9.77E-12 5-4 3.60E-12 6-5-8.32E-12 7-6 8.44E-11 8-7 1.13E-09
Old He II optical depths: 1 2.15E+01 2 2.01E+01 3-2.27E-19 4-5.71E-19 5-1.11E-18 6-1.94E-18 7-2.10E-17 Lines: 2-1 3.88E+05 3-2 2.39E-08 4-3 3.31E-15 5-4-2.91E-15 6-5-2.55E-14 7-6 6.62E-14 8-7 9.70E-13
New HE II optical depths: 1 2.16E+01 2 2.01E+01 3-2.27E-19 4-5.69E-19 5-1.11E-18 6-1.93E-18 7-2.09E-17 Lines: 2-1 3.73E+05 3-2 2.37E-08 4-3 3.28E-15 5-4-2.84E-15 6-5-2.51E-14 7-6 6.56E-14 8-7 9.60E-13
Hydrogen -1.900 -0.006 Log10 Mean Ionisation (over volume)
Helium -0.569 -0.137 -3.901 Carbon -3.767 -0.539 -0.151 -2.412 -7.706
Nitrogen -2.041 -0.367 -0.255 -2.336 Oxygen -1.889 -0.267 -0.351 -4.444
Neon -1.860 -0.231 -0.399 -5.340 Magnesium -3.306 -0.869 -0.063 -6.601
Aluminum -4.150 -0.587 -0.185 -1.054 Silicon -4.831 -0.815 -0.109 -1.161 -3.426
Sulphur -5.528 -0.931 -0.071 -1.467 -4.127
Argon -2.220 -0.434 -0.215 -1.775 -6.237 Calcium -2.441 -0.987 -0.050 -2.864 -8.095
Iron -3.220 -1.273 -0.292 -0.362 -4.376 -8.462

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
Hydrogen	-2.260	-0.002				L	og10 Me	ean Ioni:	sation	(over r	adius)					
Helium	-0.903	-0.059	-2.933														
Carbon	-4.070	-0.796	-0.082 -	1.951 -	-6.727												
Nitrogen	-2.410	-0.626	-0.127 -	1.861													
Oxygen	-2.260	-0.470	-0.183 -	3.475													
Neon	-2.208	-0.409	-0.219 -	4.380													
Magnesium	-3.654	-1.152	-0.032 -	5.656													
Aluminum	-4.475	-0.850	-0.184 -	0.689													
Silicon	-5.177	-1.110	-0.120 -	0.788 -	-2.788												
Sulphur	-5.886	-1.205	-0.072 -	1.050 -	-3.448												
Argon	-2.595	-0.694	-0.126 -	1.326 -	-5.267												
Calcium	-2.752	-1.194	-0.031 -	2.399 -	-7.109												
Iron	-3.590	-1.610	-0.486 -	0.188 -	-3.409	-7.471											
							Noi	rmalised	contir	uum							
0.25 2.	551 0	.27 1.99	2 0.30	1.632	0.33	1.427	0.36	6 1.325	0.39	1.260	0.43	1.227	0.47	L.210	0.51 1.2	01	0.56 1.192
0.62 1.	177 0	.67 1.14	0 0.74	1.035	0.81	1.000	0.88	B 1.000	0.97	1.000	0.98	1.000	0.99 1	L.000	1.00 1.0	00	
						Eme	ergent	continu	um – ph	ot/ryd/	'cm2 (1	r in)					
0.26 4.	16E+12	0.53 2.	22E+12	1.0	9.46E+	11	1.2 4	.74E+04	2.5	2.92E-	-03	4.18E+0	0 8.321	E-10	8.45E+00	1.48	BE-02
0.29 3.	18E+12	0.60 2.	06E+12	1.0	9.31E+	11	1.4 3	.88E+04	2.9	4.61E-	-05	4.66E+0	0 6.511	S-07			
0.33 2.	71E+12	0.67 1.	82E+12	1.0	1.60E+	07	1.6 2	.13E+06	3.2	3.46E-	-07	5.25E+0	0 1.061	E-04			
0.37 2.	51E+12	0.76 1.	42E+12	1.0	1.24E+	07	1.8 2	.67E+07	3.6	1.99E-	-06	5.91E+0	0 4.361	E-03			
0.42 2.	40E+12	0.86 1.	21E+12	1.0	9.68E+	06	2.0 1	.75E+00	3.9	5.02E-	-05	6.66E+0	0 2.771	E-02			
0.47 2.	32E+12	0.97 9.	86E+11	1.1	8.69E+	05	2.3 9	.45E-02	4.0	3.07E-	-11	7.50E+0	0 3.921	E-02			

*	**************************************	*
*		*
*	title paris meeting NLR model	*
*	r iterate	*
*	print last iteration	*
*	interpolate (0 -10) (0.073 -10) (0.074 1) (7352 -4)	*
*	CONTINUE (7400 -15) (7,353,000 -20)	*
*	stop lyman continuum optical depth 4	*
*	rhden 3	*
*	abund -1 C-3.5229 N-4. O-3.22185 ne-3.82391 mg-4.5229 al=-8	*
*	continue si-4.5229 s-4.82391 ar-8 ca=-8 fe-7	*
*	<pre>vionization parameter -2</pre>	*
*	c parisnlr.in	*
*	c cray	*
*		*
*	*************************	*

Chemical composition He:.100 C:3.00E-04 N:1.00E-04 O:6.00E-04 Ne:1.50E-04 Mg:3.00E-05 A:1.0E-08 Si:3.00E-05 S:1.50E-05 A:1.0E-08 Ca:1.0E-08 Fe:1.00E-07

478Cell Peak1.57E+02	Lo 1.00E-05=0.9120cm		E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 1.7642	Average nu:8.888E+00	P(X-ray): 1.5829	P(BalC): 0.9577	Q(Balmer C): 11.9548
Q(1.0-1.8): 11.1278	Q(1.8-4.0): 10.9587	Q(4.0-20): 10.7803	Q(20): 10.1653	Ion pht flx:3.001E+11
L(gam ray): -0.9305	Q(gam ray): 5.8744	L(Infred): 0.9013	Alf(ox): -1.0006	Total lumin: 1.8759
U(1.0):1.001E-02	U(4.0):2.499E-03	T(En-Den):2.399E+01	T(Comp):1.914E+07	nuJnu(912A):6.540E+00
Occ(FarIR):3.514E-11	Occ(H n=6):1.838E-21	Occ(1Ryd):3.015E-16	Occ(4R):1.171E-18	Occ (Nu-hi):5.951E-43
Tbr(FarIR):5.835E-11	Tbr(H n=6):8.161E-18	Tbr(1Ryd):4.763E-11	Tbr(4R):7.408E-13	Tbr (Nu-hi):7.784E-34

1 Te:1.581E+04 Hden:1.000E+03 Ne:1.199E+03 R:1.000E+25 R-R0:6.851E+15 dR:1.370E+16 NTR: 2 Htot:9.534E-18 T912: 4.541E-02###
-2.55 4686 0.35 5876 0.00 1909 2.06 1549 9.82 6584 0.01 5007 2.43 3727 0.02 6300 0.00 2798 0.00 1035 0.27
Hydrogen 5.265E-04 9.995E-01 H+0/Hden: 1.000E+00 6.113E-12 H- H2 4.303E-13 6.269E-12 H2+ HeH+ 8.723E-13 H col den 1.370E+19
H 2SP 3-6 1.577E-11 2.540E-15 5.930E-18 5.981E-18 7.434E-18 9.454E-18 Texc(La); 4.356E+03 T(contn): 2.394E+01 T(diffs): 2.548E+02
Helium 4.202E-05 4.978E-02 9.502E-01 He I 2S3 5.410E-08 Comp H, C 7.242E-22 5.980E-25 Fill Fact 1.000E+00 Gam 1/tot 9.715E-01
He singlet 4.197E-05 3.206E-13 2.514E-20 3.406E-20 4.883E-20 6.715E-20 He triplt 5.410E-08 6.583E-18 3.616E-20 2.134E-19 3.172E-20
HeII 4.978E-02 2.932E-12 7.846E-19 1.168E-18 1.819E-18 2.723E-18 2.298E-17 2.278E-16 4.159E-14 PRAD/GAS; 7.285E-03
Pressure NgasTgas; 3.551E+07 P(total): 4.938E-09 P(gas): 4.902E-09 P(Radtn): 3.571E-11 Rad accel 4.636E-07 Force Mul 5.468E+02
Carbon 1.868E-06 4.103E-03 1.929E-01 5.223E-01 2.531E-01 2.710E-02 4.342E-04 H2O+/Otot 0.000E+00 OH+/Ototl 0.000E+00
Nitrogen 3.210E-07 9.353E-04 1.073E-01 3.647E-01 3.026E-01 2.176E-01 6.784E-03 4.097E-05 02/Ototl: 0.000E+00 02+/Otot: 0.000E+00
Oxygen 1.408E-07 5.399E-04 8.715E-02 4.006E-01 3.087E-01 1.569E-01 4.597E-02 1.612E-04 0.000E+00 Hex(tot): 0.000E+00 A:-12.624
Neon 0.000E+00 6.212E-05 2.628E-02 1.977E-01 5.383E-01 2.291E-01 7.055E-03 1.513E-03 9.476E-05 0.000E+00 0.000E+00
Magnesium 0 2.470E-07 5.261E-05 5.304E-03 4.293E-02 1.008E-01 3.868E-01 3.677E-01 8.839E-02 7.611E-03 4.013E-04 1.247E-05 0.000E+00
Aluminium 0 7.793E-07 1.009E-03 5.493E-03 2.914E-02 7.210E-02 3.115E-01 4.179E-01 1.491E-01 1.317E-02 5.210E-04 1.335E-05 0.000E+00
Silicon 0 0.000E+00 2.186E-04 8.186E-03 2.927E-02 4.741E-02 2.293E-01 3.869E-01 2.450E-01 5.015E-02 3.378E-03 1.086E-04 0.000E+00
Sulphur 0 0.000E+00 5.210E-04 2.650E-02 5.876E-02 5.632E-02 2.276E-01 3.111E-01 2.290E-01 7.905E-02 1.058E-02 5.914E-04 1.763E-05
Argon 1 1.344E-04 8.416E-03 3.735E-02 6.014E-02 1.516E-01 2.522E-01 2.351E-01 2.154E-01 3.606E-02 3.428E-03 1.249E-04 2.281E-06
Calcium 0 0.000E+00 1.967E-04 2.679E-03 1.493E-02 2.811E-02 1.542E-01 3.260E-01 3.007E-01 1.273E-01 3.650E-02 8.888E-03 4.422E-04
Iron 1 0.000E+00 2.775E-05 1.345E-03 1.107E-02 1.214E-01 3.421E-01 4.040E-01 8.556E-02 2.937E-02 4.622E-03 4.981E-04 4.084E-05
#####100 Te:9.406E+03 Hden:1.000E+03 Ne:1.649E+02 R:1.000E+25 R-R0:3.164E+18 dR:1.502E+17 NTR: 5 Htot:8.789E-19 T912: 1.001E+04###
-0.86 4686 0.24 5876 0.10 1909 6.14 1549 9.64 6584 2.31 5007 25.00 3727 3.08 6300 1.07 2798 2.67 1035 0.12
Hydrogen 8.515E-01 1.485E-01 H+0/Hden: 1.000E+00 3.245E-09 H- H2 1.171E-07 6.778E-09 H2+ HeH+ 4.926E-08 H col den 3.239E+21
H 2SP 3-6 6.738E-12 2.789E-13 5.526E-19 6.638E-19 9.901E-19 1.436E-18 Texc(La); 3.726E+03 T(contn): 2.140E+01 T(diffs): 2.468E+02
Helium 8.480E-01 1.485E-01 3.569E-03 He I 2S3 4.549E-08 Comp H, C 1.017E-22 3.104E-26 Fill Fact 1.000E+00 Gam 1/tot 6.553E-02
He singlet 8.480E-01 8.513E-14 1.598E-20 2.093E-20 3.135E-20 4.521E-20 He triplt 4.549E-08 3.558E-16 2.375E-20 4.254E-19 1.935E-20
HeII 1.485E-01 2.235E-15 5.963E-22 9.018E-22 1.423E-21 2.155E-21 1.861E-20 1.935E-19 4.488E-17 PRAD/GAS; 2.180E-02
Pressure NgasTgas; 1.218E+07 P(total): 1.739E-09 P(gas): 1.681E-09 P(Radtn): 5.772E-11 Rad accel 1.677E-08 Force Mul 2.266E+02
Carbon 1.748E-04 8.811E-01 1.185E-01 1.114E-04 7.142E-05 0.000E+00 0.000E+00 H2O+/Otot 0.000E+00 OH+/Ototl 0.000E+00

Nitrogen	3.065E-01	6.927E-01	6.522E-04	1.389E-04	1.400E-07	2.274E-05	0.000E+00	0.000E+00	02/0totl:	0.000E+00	02+/0tot:	0.000E+00	
Oxygen	8.649E-01	1.345E-01	6.662E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.565	
Neon	2.720E-02	2.589E-01	7.137E-01	1.514E-04	3.816E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00		
Magnesium (0 1.910E-03	6.500E-01	3.479E-01	1.347E-04	9.646E-06	1.231E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Aluminium (0 7.034E-05	6.335E-01	1.727E-01	1.065E-01	4.042E-02	3.298E-02	1.168E-02	2.017E-03	1.662E-04	0.000E+00	0.000E+00	0.000E+00	
Silicon (0 6.545E-05	9.969E-01	2.076E-03	8.597E-04	8.358E-07	6.355E-05	3.752E-05	1.240E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Sulphur (0 2.099E-05	6.073E-01	3.921E-01	3.338E-04	4.732E-05	1.400E-04	4.422E-05	3.191E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	
Argon (0 8.037E-02	7.427E-01	1.760E-01	2.431E-04	4.941E-05	1.895E-04	1.360E-04	1.331E-04	1.033E-04	3.022E-05	0.000E+00	0.000E+00	
Calcium (0 1.769E-03	5.795E-02	9.069E-01	1.053E-02	3.932E-04	9.923E-03	5.176E-03	4.690E-03	1.754E-03	7.442E-04	2.066E-04	0.000E+00	
Iron (0 6.536E-03	9.651E-01	1.506E-02	4.929E-04	4.803E-03	3.689E-03	2.616E-03	1.196E-03	3.574E-04	1.340E-04	0.000E+00	0.000E+00	
Calculati	ion stopped	because of	otical dept	ch reached									
Geometry is plane-parallel.													
FeII-MgII photoionization of H N=2 reached 10.8 percent of the total rate out.													

Photoionization of He 2TriS reached 14.5 percent of the total rate out.

title paris meeting NLR model iterate print last iteration

C-Continuum not defined at gamma-ray energies - pair production and Compton scattering OK? Some fine struc lines are optically thick, largest=8.54E-01 Frequency out of range of free-free gaunt factor routine. The optical depth to Rayleigh scattering at 1300A is 1.07E-02

print last iteration interpolate (0 -10) (0.073 -10) (0.074 1) (7352 -4) stop lyman continuum optical depth 4 hden 3 abund -1 C-3.5229 N-4. O-3.22185 ne-3.82391 mg-4.5229 al=-8 ionization parameter -2 tant Density Model. Open geometry. Iteration 2 of 2. Intensity (erg/s/cm^2) Emission Line Spectrum. Constant Density Model. Mg 7 2629 -1.831 Mg 8 3 -2.158 Al 3 1860 -4.609 Si 2 35 -0.833 Si 2 2335 -1.520 Si 2 1808 -2.548 Si 3 1207 -2.318 Si 3 1895 -1.206 PHOT 1895 -3.350 Si 4 1397 -1.525 Si 6 19 -1.676 Si 7 2148 -2.420 0 1 6363 -1.308 0 1 5577 -2.701 0 1 630 -1.323 0 1 1470 -2.447 0 1 7774 -4.429 T OI 0 -2.875 He I 2 -2.514 DevB 2 -3.289 He I 5016 -2.560 DevB 5016 -2.913 He I 3965 -2.849 DevB 3965 -3.412 TOTL 4861 -0.860 TOTL 1216 0.683 1.0000 34.9131 0.0221 0.3559 0.1067 0.0037 1.235 124.3059 0.679 34.6054 0.901 57.6624 0.645 32.0009 0.0144 0.3440 0.0259 0.0003 0.0097 0.0002 1.0627 0.2186 0.0205 TotH 0 0.0199 0.0199 0.0089 0.0103 0.0028 BFH1 õ BFHe TotM T OI 0 -2.875 61ev 1304 -2.880 TOTL 3727 -0.372 TOTL 7325 -1.810 IONZ 3727 -3.257 IONZ 7325 -3.817 DevB 3965 -3.412 He I 3614 -3.132 DevB 3614 -3.548 He I 3448 -3.351 DevB 3448 -3.948 HeII 228 -0.532 ComH 0 -2.946 0.0082 0.0053 0.0095 0.0348 0 -2.565 н- н 0.0197 0.0020 3.0760 0.4505 H- H 0 -2.565 CA B 4861 -0.866 CA B 1216 0.680 DU B 4861 -0.866 0.9856 34.6504 0.9856 0.0032 0.1122 0.0040 0.0011 0.0032 0.2160 2.1282 IONZ 7325 -3.817 O II 3729 -0.695 O II 3729 -0.652 O II 2471 -1.909 O II 7323 -2.066 O II 7332 -2.160 O II 7332 -2.160 O II 834 -4.010 O 2 4651 -3.404 O 3 1663 -0.859 Phot 1663 -3.814 Augr 1663 -2.719 Rec 1663 -2.291 Q(H) 4861 -0.846 Q(H) 1216 0.846 TOTL 6563 -0.397 TOTL 4861 -0.860 TOTL 4340 -1.163 TOTL 4102 -1.398 ESC 304 -0.891 He2C 911 -1.251 TOTL 1640 -0.499 TOTL 4686 -1.473 1.0319 0.9315 1.4597 0.0275 1.6123 0.0892 0.0621 35,2817 0.4064 0.2149 2.9032 2.2947 0.0122 TOTL 1216 -0.915 Ca B 1640 -0.445 0.4972 0.8797 0.0501 0.0027 0.2897 2.5996 0.0007 0.0070 Ca B 1640 -0.445 DevB 1640 -0.447 Ca B 4686 -1.310 DevB 4686 -1.316 C 1 1656 -4.753 REC 1656 -3.649 C I 9850 -3.524 C 1 8727 -4.593 C 2 158 -2.048 C 2 2326 -0.913 TOTL18751 -1.416 TOTL12818 -1.694 TOTL10938 -1.921 TOTL40512 -2.105 2.5870 0.3545 0.3497 0.0005 0.0021 1.4603 0.1003 0.2775 0.0029 1.0020 0.0869 0.0001 0.0138 S 2 4074 -1.858 S 210330 -2.031 S II 6731 -1.025 S II 6716 -0.969 S II 4070 -1.982 S II 4078 -2.463 S II10323 -2.485 S II10229 -2.613 S II10373 -2.933 S II10373 -2.933 S II10375 -4.537 Rec 1663 -2.291 O 3 5007 0.538 O 3 4959 0.061 TOTL 4363 -1.228 TOTL26252 -2.305 TOTL74578 -2.635 0.0359 0.0016 0.0371 0.0674 0.0168 0.0022 24.9979 0.6835 2 NU 0 TOTL 1216 0.349 16.1707 0.00022 8.3326 0.7768 TOTL 4363 -1.228 Rec 4363 -3.344 O 3 2321 -1.855 C EX 4363 -3.872 C EX 5592 -3.801 O 3 880 -0.896 TOTL 1026 -3.614 0.0018 0.8840 0.0033 0.0249 INWD 2326 -1.208 C 2 1335 -2.135 REC 1335 -1.888 C 2 4267 -3.630 TOTL 973 -3.557 TOTL 950 -3.525 0.0020 0.4481 0.1010 0.0237 TOTL 973 -3.537 TOTL 950 -3.525 TOTL 938 -3.471 LA X 1216 -0.756 0.0022 0.0531 0.0176 0.0022 0.0936 0.0011 0.0084 3 3 3 C 2 4267 -3.630 TOTL 977 -1.169 C3 C 977 -1.251 C3 R 977 -1.930 TOTL 1909 -0.071 INWD 1909 -0.365 C 3 1907 -0.294 C 3 1909 -0.468 0 3 520 -0.483 0 3 834 -2.416 0 3 3341 -3.704 0 4 26 -0.114 0 4 1402 -1.276 CONT 1401 -1.787 S III 1256 -4.537 S 3 18 -1.122 S 3 34 -1.053 S 39532 -0.636 S 39069 -1.052 S 3 6312 -2.135 C13c 6563 -1.697 0.1456 0.4909 2.3803 0.0002 C14c 4861 -2.765 0.0124 0.4057 0.0278 0.5467 CION 0 -1.553 INWD 1216 0.646 INWD 6563 -0.695 0.0852 0.0014 0.6402 0.2027 32.0066 1.4628 3.1217 0.3839 0.6428 4861 -1.160 INWD 0.5005 3.6768 0.1183 0.0531 O 4 789 -2.309 O 4 3412 -3.233 O 5 630 -3.536 TOTL 1218 -1.455 s 3 3722 -2.364 s 3 1198 -3.526 s 3 1729 -2.760 s 4 105 -0.942 INWD18751 -1.718 0.1387 2.4670 0.0356 0.0313 C 3 1909 -0.400 C3 R 1909 -2.091 Phot 1909 -2.196 C 3 2297 -2.449 Dest 1216 -1.626 Dest 6563 -4.214 e sc18751 -1.526 0.0022 0.0126 0.8282 0.1714 0.0587 0.0042 Phot 1909 -2.196 C 3 2297 -2.449 C 3 4187 -4.306 C 3 4649 -3.509 0.0004 0.0461 0.0258 0.0021 s 4 1406 -2.560 s 5 1198 -3.117 e sc40512 -2.673 nFnu 4860 -0.126 0.0154 0.0004 O 5 1218 -1.868 O 5 1214 -1.667 0.0981 0.0199 5,4180 0.0022 0.1558 0.0055

PARIS MEETING NLR MODEL
Cooling: Cool 1216:0.112 C 4 1549:0.077 O 3 5007:0.200 O 3 4959:0.067
Heating: BFH1 0:0.278 BFHe 0:0.464 TotM 0:0.257
IONIZE PARMET: U(1-) -1.9996 U(4-): -2.6021 U(sp): -2.00 Q(ion): 9.713 L(ion): 1.486 Q(low): 12.57 P(low) 1.23
ENERGY BUDGET: Heat: 1.235 Coolg: 1.236 Error: 0.3% Compt H: -2.946 WorkF: 1.212 F-F H -5.860 PRADMX:3.43E-01
Column density H12:3.239E+21 H II:1.648E+21 HI:1.591E+21 H-: 8.267E+12 H2: 1.220E+14 H2+:6.642E+12 He H+:1.155E+14 OH: 0.000E+00 Heff:2.290E+21 He H:1.155E+14 OH: 0.000E+00 Heff:2.290E+21 OH: 0.000E+00 Heff:2.290E+21 OH:0.000E+00 Heff:2.290E+00 Heff:2.290E+000 Heff:290E+000E+00 Heff:290E+00 Heff:290E+00 H
<pre><nh>:1.000E+03 <tp>:1.33E+04 <to3>:1.39E+04 Ne:1.117E+03 ti(snd):3.15E+12 NeN+dl:1.50E+24 <t(c3)>:1.24E+04 <e(c3)>:7.71E+02</e(c3)></t(c3)></to3></tp></nh></pre>
He/Ha:9.22E-02 = 0.92*true N/Oap:3.98E-01 = 2.39true T(O3R):1.392E+04 L THIN:1.00E+30 <t(s2)>9.95E+03 <e(s2)>:2.53E+02 T He+1.23E+04 EHe+:7.84E+02 T(O+):1.04E+04 EO+:3.69E+02 iter/zn: 2.092 Te-low:9.41E+03 Te-hin1:1.6EE+04 Hu/zn:2.60E+00</e(s2)></t(s2)>
T He+:1.23E+04 EHe+:7.84E+02 T(O+):1.04E+04 EO+:3.69E+02 iter/zn: 2.092 Te-low:9.41E+03 Te-high:1.66E+04 Hlu/zn:2.60E+00 <abr></abr> <abr></abr> cab:0.00E+00 erdeFe0.0E+00 Tcompt3.09E+08 Thr8.09E+08 <tdenb: 1.16e+04="" <abr="" <denbs:2.36e-21=""></tdenb:> MO1>:8.92E-01
Mean Jeans l(cm)1.32E+20 M(sun)1.43E+06 smallest: len(cm):1.19E+20 M(sun):1.04E+06 Alf(ox-tran): -1.0450
Optical Depths: CONTN; COMP: 1.25E-03 H-: 3.22E-04 R(1300): 1.07E-02 H2+ 4.65E-05 HeTri:1.95E-03
Pfail.25E-03 Pail.25E-03 Bail.54E-03 Bbil.48E-03 Lai2.65E-01 1r:1.001E+04 1.8:3.06E+03 4.:6.628E+02 21R:7.467E+00
10830: 1.23E+02 3889: 5.25E+00 5876: 9.73E-07 7065: 5.37E-07
1550: 1.26E+04 2800: 4.91E+04 774: 4.26E+00 1240: 8.62E+02 1035: 1.27E+03 1335: 6.57E+04 977: 8.79E+04 1397: 2.20E+03 789: 3.11E+03 1207: 5.57E+03 1085: 4.38E+03 1194: 1.15E+02 1909: 3.50E-02 1895: 1.49E-01 2326: 3.28E-02 1666: 1.60E-01
1750: 7.24E-04 1025: 8.84E+03 352: 1.05E-02 347: 1.00E-20 1860: 4.97E+00 630: 7.71E+03 834: 4.45E+04 835: 7.76E+03
1808: 7.92E+04 1256: 6.59E+02 -3: 1.01E+01 -48: 1.68E-08 3934: 3.14E+00 3969: 1.58E+00 8498: 1.60E-06 8542: 1.44E-05
8662: 8.13E-06 353: 1.40E-03 1304: 3.03E+04 1122: 7.27E-01 990: 3.20E+03 1402: 4.15E-02 1214: 4.16E-02 1486: 1.10E-02 2353: 1.89E-01 1406: 4.58E-02 1656: 1.55E+01 9830: 2.63E-09 8727: 3.21E-09 6300: 8.02E-05 5577: 3.59E-08 7291: 2.10E-07
7324: 1.45E-07 1039: 4.30E+03 -8446: 9.08E-09 -4368: 3.44E-11 -132:-5.69E-14 -113: 1.73E-13 -29: 7.15E-13 -46: 1.37E-13
-245: 1.54E-04 765: 6.70E+03 -1198: 4.38E-02 786: 1.30E+02 C157: 2.80E-02 N122: 3.58E-02 N205: 3.56E-02 N57: 2.88E-02 0146:-3.11E-02 063: 8.54E-01 088: 2.23E-01 052: 1.85E-01
026: 1.10E-01 NE13: 4.19E-02 NE36: 1.38E-03 NE16: 3.31E-01 MG4: 3.47E-03 MG14:-1.56E-06 MG6: 3.28E-03 S135: 7.46E-02
S19: 6.40E-03 S34: 7.61E-02 S11: 3.50E-03 AR7: 1.22E-05 AR9: 1.12E-05 AR22:-1.81E-08 AR13: 3.19E-06 AR8: 6.11E-09
CA3: 1.92E-06 CA12:-2.23E-10 CA4: 9.23E-07 Ne14: 6.39E-03 Ne24: 1.13E-01 Si3: 1.33E-08 Si4: 3.36E-03 Fe7: 4.21E-10 Fe61:-1.14E-09 Fe23: 1.00E-20 Fe13: 1.00E-20 Si2.5: 1.80E-03 Si6.5:-2.64E-08 C610: 3.50E-05 C370: 1.41E-05
Old hydro optical depths: 1 1.00E+04 2 1.49E-04 3 2.94E-04 4 8.29E-05 5 9.21E-13 6 2.12E-12 7 9.21E-12
Lines: 2-1 9.45E+07 3-2 9.03E-03 4-3 1.22E-09 5-4 9.10E-10 6-5 2.82E-10 7-6 9.51E-09 8-7 1.24E-07 New hydro optical depths: 1 1.00E+04 2 1.63E-04 3 3.23E-04 4 9.11E-05 5 9.26E-13 6 2.13E-12 7 9.24E-12
Lines: 2-1 9.45E+07 3-2 8.67E-03 4-3 1.27E-09 5-4 9.38E-10 6-5 3.01E-10 7-6 9.61E-09 8-7 1.25E-07
Old He Is optical depths: 1 3.05E+03 2 6.51E-04 3-9.54E-17 4-3.90E-16 5-8.08E-16 6-1.45E-15 7-1.66E-14
Lines: 2-1 5.64E+06 3-2 4.17E-04 4-3 4.05E-11 5-4 2.82E-11 6-5 2.45E-10 8-7 3.54E-09
New HE Is optical depths: 1 3.06E+03 2 6.70E-04 3-9.77E-17 4-3.97E-16 5-8.24E-16 6-1.48E-15 7-1.69E-14
Lines: 2-1 5.66E+06 3-2 4.24E-04 4-3 4.10E-11 5-4 2.87E-11 6-5 2.54E-11 7-6 2.78E-10 8-7 3.57E-09
Old He II optical depths: 1 6.60E+02 2 1.00E+04 3-3.55E-16 4-9.28E-16 5-1.82E-15 6-3.15E-15 7-3.41E-14
Lines: 2-1 3.41E+06 3-2 2.74E-05 4-3 4.45E-12 5-4 2.70E-13 6-5-1.53E-11 7-6 6.85E-11 8-7 9.56E-10
New HE II optical depths: 1 6.63E+02 2 1.00E+04 3-3.53E-16 4-9.25E-16 5-1.81E-15 6-3.14E-15 7-3.40E-14 Lines: 2-1 3.43E+06 3-2 2.74E-05 4-3 4.44E-12 5-4 2.90E-13 6-5-1.52E-11 7-6 6.83E-11 8-7 9.53E-10
Hydrogen -0.309 -0.293 Log10 Mean Ionisation (over volume) Helium -0.336 -0.406 -0.835
Carbon -3.839 -0.300 -0.485 -0.875 -1.461 -2.478 -4.310
Nitrogen -0.881 -0.294 -0.760 -0.925 -1.405 -1.555 -3.139 -5.415
Oxygen -0.301 -0.856 -0.620 -1.145 -1.495 -1.875 -2.424 -4.908 Neon -2.033 -0.912 -0.176 -1.083 -1.047 -1.550 -3.098 -3.745 -4.979
Magnesium -3.303 -0.446 -0.412 -1.263 -1.447 -1.075 -1.188 -1.853 -2.934 -4.210 -5.860
Aluminum -4.502 -0.464 -0.819 -0.922 -1.112 -0.846 -0.906 -1.425 -2.489 -4.065 -5.787
Silicon -4.799 -0.194 -1.292 -1.247 -1.580 -1.135 -1.032 -1.301 -2.033 -3.229 -4.731 Sulphur -5.664 -0.513 -0.404 -1.296 -1.599 -1.094 -1.121 -1.306 -1.811 -2.711 -3.992 -5.630
Argon -1.544 -0.401 -0.594 -1.401 -1.677 -1.167 -1.154 -1.208 -1.299 -2.091 -3.127 -4.630 -8.015
Calcium -3.063 -1.284 -0.218 -1.172 -1.640 -1.100 -1.217 -1.630 -2.147 -2.755 -4.197 Iron -2.496 -0.228 -1.384 -0.950 -1.372 -1.166 -1.161 -1.248 -1.956 -2.425 -3.255 -4.229 -5.344
1101 -2.420 -0.220 -1.304 -0.930 -1.372 -1.100 -1.101 -1.240 -2.425 -3.235 -4.229 -3.344

nFn	u 1215 -	1.177	0.4812	C 4	1549	0.125	9.6448	0	5 5112	-4.308	0.0004	S 5	786 -4.851	0.0001
Inc	i 4861	0.816	47.3946	INWD	1549	-0.087	5.9222	0	6 1035	-1.774	0.1217	S 6	933 -2.792	0.0117
Inc	i 1216	0.816	47.3575	DEST	1549	-3.056	0.0064	Ne	2 128	-1.800	0.1147	S 9	1715 -3.850	0.0010
BA	C 0 –	0.203	4.5382	C4 r	1549	-2.518	0.0220	Ne	3 156	-0.393	2.9273	Ar 3	7135 -4.191	0.0005
PA	c 0 –	0.729	1.3501	C 4	4659	-4.116	0.0006	Ne	3 361	-1.461	0.2506	Ar 3	7751 -4.821	0.0001
ΗF	F 0 –	0.501	2.2826	C 6r	34	-3.319	0.0035	Ne	3 3869	-0.343	3.2865	Ar 3	9 -4.497	0.0002
ΗF	в 0–	0.407	2.8376	N 1	5200	-1.888	0.0936	Ne	3 3968	-0.856	1.0083	Ar 4	4740 -4.387	0.0003
Coo		0.285	13.9681	REC	5200	-4.309	0.0004			-2.829	0.0107	Ar 6	4 -4.600	0.0002
Crs	t 960 -	2.289	0.0373	N 1	1200	-4.042	0.0007	Ne	3 1815	-2.690	0.0148	Ca 2	3933 -4.045	0.0007
H-F	в 0–	2.528	0.0215	N 2	6584	-0.496	2.3113	Ne	4 2424	-0.828	1.0745	Ca 2	7306 -3.671	0.0015
H2+	0 -	2.920	0.0087	N 2	6548	-0.973	0.7704			-2.513	0.0222		3934 -4.230	0.0004
HEH	+ 0 -	4.137	0.0005	REC		-3.955	0.0008			-1.897	0.0919		3969 -4.503	0.0002
HeF		1.168	0.4913			-2.231	0.0425			-0.649	1.6247		7291 -3.894	0.0009
HeF		0.980	0.7580	N 2		-2.149	0.0513			-1.082	0.6000		7324 -4.067	0.0006
MeF		4.119	0.0005	N 2		-2.812	0.0112			-3.121	0.0055	Ca 4	32 -4.740	0.0001
MeF		2.485	0.0237			-4.574	0.0002			-2.646	0.0164	Fe 2	7 -3.169	0.0049
TOF		0.413	2.7976			-4.060	0.0006	Ne		-0.289	3.7223	Emis	3 -2.849	0.0103
esc			0.0271			-2.037	0.0665	Ne		-0.287	3.7402	Cool	3 -2.848	0.0103
He2			0.0135			-3.583	0.0019			-2.421	0.0274	TOT	0 -2.679	0.0152
He		1.173	0.4855			-1.277	0.3823	Ne		-1.324	0.3435	FEIR	0 -3.731	0.0013
	I 4471 -		0.0333	N 3		-1.555	0.2018			-3.319	0.0035	Fe 3	0 -4.239	0.0004
	L 5876 -		0.0991	N 3		-2.856	0.0101			-0.434	2.6658		4658 -4.675	0.0002
	B 5876 -		0.0907			-1.242	0.4151			-0.434	2.6665		3892 -3.961	0.0008
	L10830 -		0.5920	N 4		-3.175	0.0048	Mg		-1.865	0.0987	Fe 6	0 -4.175	0.0005
	D10830 -		0.3691			-3.192	0.0047	Mg		-1.857	0.1005		5177 -4.626	0.0002
	L 3889 -		0.0521			-1.470	0.2456	Mg		-1.126	0.5412	Fe 7	6087 -4.231	0.0004
	L 7065 -		0.0438	N 7r		-4.765	0.0001			-2.142	0.0523			
CcH	E 0 –	1.206	0.4504	0 1	6300	-0.831	1.0677	Mg	6 1806	-2.185	0.0472			

	-	2	5	7	5	0	'	0	-	10		12	15	14	15	10	1,
**	0 200	0 000					-10 -										
Hydrogen Helium			-0.835			LC	giu me	an Ionis	ation	(over ra	adius)						
Carbon				-0.875	1 461	0 470	4 210										
Nitrogen																	
Oxygen				-1.145													
Neon				-1.083						4 010	5 060						
Magnesium																	
Aluminum																	
Silicon Sulphur				-1.247													
				-1.296													
Argon				-1.401													
Calcium																	
Iron	-2.496	-0.228	-1.384	-0.950	-1.372	-1.166	-1.161	-1.248	-1.956	-2.425	-3.255	-4.229	-5.344				
0.5-1.0KE	V:1.29E	+09 1.0	-1.5:1.0	D2E+09 1	.5-2.0:	5.74E+0	08 2.0-	2.5:3.71	E+08 2	.5-3:2.8	81E+08	3-5:5.1	4E+08 5	-7.5:2	.66E+08	7.5-10	0:1.41E+08
								malised									
0 05 1	207 0	07 1 0	~ ~ ~		0.00	1 101		1.179			0 40 4	.188	0 47 1	~~~	0.51 1.2	20	0.56 1.245
0.25 1.		.27 1.2		30 1.189 74 0.976				1.179					0.47 1.		1.00 0.9		0.56 1.245
0.62 1.	247 0	.6/ 1.2	12 0.1	/4 0.9/6	0.81	0.998	0.88	1.038	0.97	0.995	0.98 (.995	0.99 0.	995	1.00 0.9	95	
Inward co		· · · · · · · · · · · · · · · · · · ·						1 405.00									
inward co	ntinua	(nurnu)	at nead	1 OF BAL	mer, Ly	man sei	les;	1.406+00	2.38	8+00							
Outwrd co		(ot book	4 of Dol.			dea.	1 400.00									
Outwid Co	ncinua	(nurnu)	at nead	I OI BAI	шег, цу	man ser	ies;	1.406+00	0.00	5+00							
						Time	waant .	continuu	m nh	a t / mard / .	am2 (m	4					
0 26 5	47E+12	0 07 2	218+11	2 0	9.57E+			69E+01		1.18E+0			3.48E+	07	2.58E+02	1 271	2+06
	23E+12				2.07E+			45E+01					3.32E+		3.84E+02		
	30E+12				2.07E- 8.06E-			43E+02 42E-42		1.86E+0			3.09E+		5.71E+02		
	59E+12				3.23E-		8.5 4.			3.06E+0			2.83E+		8.49E+02		
	05E+12				5.51E+		9.5 6.			4.80E+0			2.03E+		1.26E+03		
	67E+12				1.20E+		9.5 6.			2.40E+0			2.30E+		1.88E+03		
	33E+12				1.20E-		2.1 1.			2.40E+0 3.33E+0			2.24E+ 1.99E+		2.79E+03		
	05E+12				1.84E- 3.01E-		3.7 4.			3.33E+0 3.97E+0			1.99E+		2.79E+03 4.14E+03		
					3.01E- 1.04E-										4.14E+03 6.16E+03		
	04E+11						5.4 7.			4.19E+0			1.54E+		0.10E+03	/.8/1	2402
	58E+11 09E+11				5.35E+ 1.11E+		9.5 2.	40E+04		4.26E+0 3.56E+0			1.32E+ 9.31E+				
0.86 4.	096+11	1./8 3	.095-19	5.3	1.116+	.0.5 1	9.5 2.	936402	04.2	3.36E+0	1 10	·/4E+02	9.31E+	00			

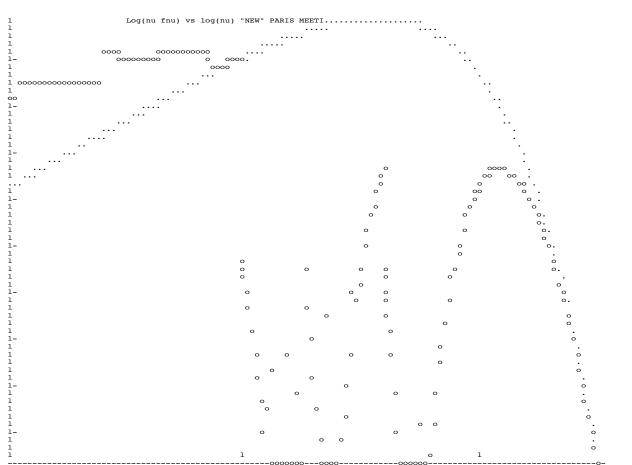
CLOUDY 80.08

Chemical composition He:.100 C:3.00E-04 N:1.00E-04 O:6.00E-04 Ne:1.50E-04 Mg:3.00E-05 A:1.0E-07 Si:3.00E-05 S:1.50E-05 A:1.0E-09 Ca:1.0E-07 Fe:1.00E-07

369Cell Peak3.74E+00	Lo 1.00E-05=0.9105cm	Hi-Con:3.38E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 37.5397	Average nu:2.935E+00	P(X-ray): 31.4677	P(BalC): 36.1444	Q(Balmer C): 46.9767
Q(1.0-1.8): 47.1615	Q(1.8-4.0): 47.4535	Q(4.0-20): 47.0523	Q(20): 40.7978	Ion pht flx:4.313E+12
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): 34.4848	Alf(ox): 0.0000	Total lumin: 37.5572
L/Lsolar: 3.9744	Abs bol mg: -5.2161	Abs V mag: 2.4664	Bol cor: -7.6825	nuFnu(Bbet): 34.5868
U(1.0):4.795E-02	U(4.0):9.981E-03	T(En-Den):3.354E+01	T(Comp):1.436E+05	nuJnu(912A):2.909E+01
Occ(FarIR):2.254E-10	Occ(H n=6):8.337E-14	Occ(1Ryd):1.342E-15	Occ(4R):3.747E-17	Occ (Nu-hi):1.382E-30
Tbr(FarIR):3.749E-10	Tbr(H n=6):3.702E-10	Tbr(1Ryd):2.120E-10	Tbr(4R):2.371E-11	Tbr (Nu-hi):7.278E-24

1 Te:1.447E+04 Hden:3.000E+03 Ne:3.612E+03 R:1.062E+17 Ctr[1Ryd];2.120E=10 Tbr[4R];2.371E=11 Tbr [4N=hi];7.276E=24
1 Te:1.447E+04 Hden:3.000E+03 Ne:3.612E+03 R:1.062E+17 Re0:6.250E+15 dR:1.250E+16 NTR: 3 Htot:5.540E=17 T512: 9.991E+07###
1.78 4666 0.65 5876 0.00 1909 0.12 1549 5.60 6584 0.00 5007 0.26 3727 0.00 6300 0.00 2798 0.00 1035 0.21
Hydrogen 1.293E=04 9.999E=01 H=0/Hden: 1.000E+00 2.228E=12 H H2 3.911E=14 1.338E=12 H2+ HEH 9.890E=15 H col den 3.750E+19
H2 259 3-6 2.646E=11 8.762E=16 8.772E=18 1.145E=17 1.556E=17 2.169E=17 Texc(1a); 4.411E+03 T(cont): 2.969E+01 T(difs): 2.448E+02
Helium 7.307E=07 5.877E=03 9.941E=01 He I 2S3 1.334E=06 Comp H. C 6.663E=23 6.733E=24 Fill Fact 1.000E+00 Gam 1/tot 9.955E=01
Ferssure NgasTgas; 9.341E-07 H:710E=12 4.161E=18 6.523E=18 9.438E=18 8.345E=17 7.756E=16 1.388E=13 PRAD/GAS; 8.650E=04
Freasure NgasTgas; 9.341E-07 H:710E=02 3.113E=01 6.776E=01 0.000E+00 0.000E+00 1.000E+00 0.000E+00 0

9.758E-01 2.421E-02 3.612E-07 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 02/0totl: 0.000E+00 02/totl: 0.000E+00 0.000E+00 9.689E-01 3.114E-02 9.389E-07 0.000E+00 0.000E+ Nitrogen Oxygen Neon Magnesium Aluminium 0 Silicon Sulphur Argon Calcium Iron Calculation stopped because lowest Te reached. Geometry is a thick shell. FeII-MgII photoionization of H N=2 reached 7.3 percent of the total rate out. Photoionization of He 2TriS reached 15.6 percent of the total rate out. Frequency out of range of free-free gaunt factor routine. The ratio of radiation to gas pressure reached 1.16E+00. Caused by Lyman alpha.



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Emission Line Spectrum. Constant Density Model. Closed geometry. Iteration 1 of 1. Luminosity (erg/s) emitted by shell with full coverage.

TOTL 4861 35.402	1.0000	DevB 2 32.83		0 1 630 33.658	0.0180	Mg 5 2751 33.740	0.0218
TOTL 1216 36.842	27.5419	He I 5016 33.70		0 1 1470 32.420	0.0010	Mg 6 1806 32.302	0.0008
TotH 0 37.206	63.7683	DevB 5016 33.26		0 1 7774 31.823	0.0003	Al 3 1860 32.646	0.0018
BFH1 0 37.061	45.6144	He I 3965 33.41		T OI 0 32.611	0.0016	Si 2 35 34.610	0.1616
BFHe 0 36.599	15.7628	DevB 3965 32.74	1 0.0022	6lev 1304 32.613	0.0016	Si 2 2335 34.599	0.1576
TotM 0 35.780	2.3897	He I 3614 33.13	3 0.0054	TOTL 3727 35.773	2.3502	Si 2 1808 33.592	0.0155
н- н 0 32.512	0.0013	DevB 3614 32.60	5 0.0016	TOTL 7325 34.622	0.1662	Si 3 1207 33.696	0.0197
CA B 4861 35.404	1.0043	He I 3448 32.91	4 0.0033	IONZ 3727 33.319	0.0083	Si 3 1895 35.023	0.4182
CA B 1216 36.942	34.7218	DevB 3448 32.18	2 0.0006	IONZ 7325 32.839	0.0027	PHOT 1895 33.321	0.0083
DU B 4861 35.404	1.0043	TOTL 1640 35.73	8 2.1705	O II 3729 35.299	0.7890	Si 4 1397 34.747	0.2215
O(H) 4861 35.411	1.0209	TOTL 4686 34.76	7 0.2320	O II 3726 35.593	1.5529	Si 6 19 32.936	0.0034
O(H) 1216 36.945	34.9046	TOTL 1216 35.32	5 0.8374	O II 2471 34.522	0.1320	S 2 6720 35.222	0.6607
TOTL 6563 35.843	2.7638	Ca B 1640 35.79		O II 7323 34.365	0.0920	S 2 4074 34.474	0.1182
TOTL 4861 35.402	1.0000	DevB 1640 35.79		O II 7332 34.272	0.0742	S 210330 34.301	0.0794
TOTL 4340 35.104	0.5033	Ca B 4686 34.95		O II 834 31.761	0.0002	S II 6731 35.002	0.3979
TOTL 4102 34.873	0.2958	DevB 4686 34.94		0 2 4651 32.881	0.0030	S II 6716 34.821	0.2627
TOTL18751 34.845	0.2777	C 1 1656 32.27	6 0.0007	0 3 1663 34.756	0.2260	S II 4070 34.350	0.0887
TOTL12818 34.573	0.1484	REC 1656 32.13		Rec 1663 33.927	0.0335	S II 4078 33.870	0.0294
TOTL10938 34.350	0.0887	C I 9850 33.52	0.0131	0 3 5007 36.586	15.2764	S II10323 33.847	0.0279
TOTL40512 34.162	0.0576	C 1 8727 32.54		0 3 4959 36.109	5.0921	S II10289 33.718	0.0207
TOTL26252 33.966	0.0366	C 2 158 32.85	5 0.0028	TOTL 4363 34.575	0.1490	S II10373 33.400	0.0100
TOTL74578 33.636	0.0171	C 2 2326 34.97		Rec 4363 32.905	0.0032	S II10339 33.720	0.0208
2 NU 0 36.418	10.3838	C 2 1335 33.72		0 3 2321 33.948	0.0352	S II 1256 31.641	0.0002
TOTL 1216 36.842	27.5419	REC 1335 34.38		C EX 4363 32.171	0.0006	s 3 18 35.229	0.6720
TOTL 1026 31.681	0.0002	C 2 4267 32.61		C EX 5592 32.242	0.0007	S 3 34 34.878	0.2991
TOTL 973 32.620	0.0017	TOTL 977 34.47		0 3 880 34.845	0.2778	S 3 9532 35.719	2.0746
TOTL 950 32.690	0.0019	C3 C 977 33.91		0 3 520 35.538	1.3700	S 3 9069 35.303	0.7964
TOTL 938 32.757	0.0023	C3 R 977 34.33		0 3 834 32.472	0.0012	S 3 6312 34.184	0.0606
LA X 1216 32.275	0.0007	TOTL 1909 35.63		0 3 3341 32.540	0.0014	s 3 3722 33.955	0.0358
C13c 6563 33.958	0.0360	C 3 1907 35.40		0 4 26 35.935	3.4133	S 3 1198 32.491	0.0012
C14c 4861 32.893	0.0031	C 3 1909 35.25		0 4 1402 34.423	0.1050	S 3 1729 33.413	0.0103
CION 0 34.095	0.0493	C3 R 1909 34.16		CONT 1401 34.273	0.0743	s 4 105 35.584	1.5221
INWD 1216 36.842	27.5419	Phot 1909 34.14		0 4 789 32.966	0.0037	S 4 1406 33.546	0.0139
Dest 1216 34.637	0.1720	C 3 2297 33.81		0 4 3412 32.959	0.0036	S 5 1198 32.686	0.0019
Dest 6563 31.966	0.0004	C 3 4187 31.96		TOTL 1218 34.225	0.0666	s 6 933 32.399	0.0010
e sc18751 34.227	0.0670	C 3 4649 32.71		0 5 1218 33.816	0.0260	Ca 2 3933 33.471	0.0117
e sc40512 32.994	0.0039	C 4 1549 35.79		0 5 1214 34.010	0.0406	Ca 2 8579 32.976	0.0038
nFnu 4860 36.017	4.1282	DEST 1549 33.01		0 6 1035 33.187	0.0061	Ca 2 7306 34.087	0.0484
nFnu 1215 34.752	0.2240	C4 r 1549 33.64		Ne 2 128 33.938	0.0344	Ca2K 3934 33.243	0.0069
Inci 4861 34.587	0.1532	C 4 4659 32.06		Ne 3 156 35.829	2.6744	Ca2H 3969 33.082	0.0048
Inci 1216 36.254	7.1168	N 1 5200 33.36		Ne 3 361 34.732	0.2140	Ca2X 8498 31.854	0.0003
BA C 0 36.045	4.4007	N 1 1200 31.49		Ne 3 3869 35.787	2.4287	Ca2Y 8542 32.812	0.0026
PA C 0 35.526	1.3321	N 2 6584 35.43		Ne 3 3968 35.274	0.7451	Ca2Z 8662 32.357	0.0009
111 C 0 551.520	1.5521	A 2 0504 55.45.	1.0,52	16 5 5500 55.274	0.7451	5422 0002 52.557	5.0009

H FF	0	35.652	1.7784	N	2	6548	34.955	0.3577	Ne 3	3343	33.099	0.0050	CaF1	7291	33.868	0.0293
H FB	0	35.751	2.2344	REC		6584	32.326	0.0008	Ne 3	1815	33.239	0.0069	CaF2	7324	33.684	0.0192
Cool	1216	35.911	3.2277	N	2	5755	33.776	0.0237	Ne 4	2424	35.111	0.5115	Ca 4	32	32.610	0.0016
Crst	960	33.371	0.0093	N	2	122	32.947	0.0035	Ne 4	4720	33.314	0.0082	Ca 5	4	31.919	0.0003
H-FB	0	32.837	0.0027	N	2	203	32.011	0.0004	Ne 4	1602	33.930	0.0338	Ca 5	5311	31.715	0.0002
H2+	0	32.454	0.0011	N	2	4239	31.719	0.0002	Ne 5	3426	35.004	0.4001	Fe 2	7	32.494	0.0012
HeFF	0	34.977	0.3759	N	2	5680	32.251	0.0007	Ne 5	3346	34.571	0.1478	Emis	3	32.884	0.0030
HeFB	0	35.197	0.6241	N	2	2140	33.988	0.0386	Ne 5	2976	32.313	0.0008	Cool	3	32.884	0.0030
MeFB	0	31.907	0.0003	N	2	1084	32.418	0.0010	Ne 5	1575	32.788	0.0024	TOT	0	33.033	0.0043
MeFF	0	33.532	0.0135	N	3	1750	34.381	0.0954	Ne 5	242	35.404	1.0045	FEIR	0	31.799	0.0002
TOFF	0	35.738	2.1678	N	3	57	34.397	0.0988	Ne 5	143	35.526	1.3308	Fe 3	0	32.260	0.0007
He I	4471	33.947	0.0351	N	3	990	32.332	0.0009	Ne 5	1134	32.863	0.0029	Fe 3	5270	31.581	0.0002
TOTL	5876	34.431	0.1070	N	4	1486	34.439	0.1090	Ne 6	76	33.516	0.0130	Fe 3	4658	31.825	0.0003
Ca B	5876	34.386	0.0965	N	4	765	31.979	0.0004	Mg 1	4571	31.465	0.0001	Fe 5	3892	31.973	0.0004
TOTL1	0830	35.327	0.8427	N	4	1718	32.947	0.0035	Emis	2798	35.694	1.9592	Fe 6	0	31.976	0.0004
TOTL	3889	34.063	0.0459	N	5	1240	34.184	0.0606	Cool	2798	35.694	1.9592	Fe 6	5177	31.525	0.0001
TOTL	7065	34.127	0.0531	0	1	6300	34.476	0.1186	Mg 4	4	34.532	0.1351	Fe 7	6087	31.666	0.0002
CcHE	0	35.252	0.7081	0	1	6363	33.999	0.0395	Mq 5	13	34.168	0.0584				
He I	2	33.757	0.0227	0	1 :	5577	32.658	0.0018	Mq 5	56	34.906	0.3195				

"NEW" PARIS MEETING PLANETARY NEBULA
Cooling: Cool 1216:0.050 0 3 5007:0.238 0 3 4959:0.079 0 4 26:0.053
Heating: BFH1 0:0.715 BFHe 0:0.247
IONIZE PARMET: U(1-) -1.3192 U(4-): -2.0008 U(sp): -2.50 Q(ion): 43.550 L(ion): 33.879 Q(low): 47.01 P(low) 36.15 ENERGY BUDGET: Heat: 37.206 Coolg: 37.209 Error: 0.6% Compt H: 30.129 WorkF: 37.422 F-F H 30.480 PRADMX:1.16E+00 Column density H12:8.916E+20 H II:8.589E+20 HI:3.274E+19 H-: 7.708E+11 H2: 4.568E+13 H2+:4.323E+11 He H+:4.103E+12
OH: 0.000E+00 Heff:0.000E+00
<pre><nh>:3.000E+03 <tp>:1.24E+04 <to3>:1.14E+04 Ne:3.355E+03 ti(snd):2.38E+11 NeN+d1:2.95E+24 <t(c3)>:1.14E+04 <e(c3)>:3.31E+03</e(c3)></t(c3)></to3></tp></nh></pre>
He/Ha:9.72E-02 = 0.97*true N/Oap:1.83E-01 = 1.10true T(03R):1.130E+04 L THIN:1.00E+30 <t(s2)>:1.02E+04 <e(s2)>:2.22E+03 T He+:1.10E+04 Ete+:3.17E+03 T(O+):1.11E+04 EO+:2.81E+03 iter/zn: 2.000 Te-low:3.68E+03 Te-high:1.45E+04 Hu/zn:2.53E+00</e(s2)></t(s2)>
A = 0.00E+00 erdeFe0.0E+00 Tcompt8.11E+07 thr3.81E+08 < Tden>: 1.23E+04 < dens:7.07E-21
Mean Jeans 1(cm)7.43E+19 M(sun)7.63E+05 smallest: len(cm):4.07E+19 M(sun):1.25E+05 Alf(ox-tran): 0.0000
Optical Depths: CONTN; COMP: 3.32E-04 H-: 1.50E-05 R(1300): 2.20E-04 H2+ 3.03E-06 HeTri:5.87E-04
Pfa:3.32E-04 Pa:3.32E-04 Ba:3.46E-04 Hb:3.43E-04 La:3.07E-03 lr:4.995E+07 1.8:1.15E+07 4.:1.715E+06 21R:3.170E+04 10830: 1.17E+02 3889: 5.00E+00 5876: 2.94E-06 7065: 1.62E-06
1550: 1.09E+04 2800: 3.84E+03 774: 1.00E-20 1240: 1.14E+03 1035: 6.01E+02 1335: 2.91E+03 977: 2.74E+04 1397: 4.30E+03
789: 3.59E+03 1207: 6.24E+03 1085: 2.03E+02 1194: 2.65E+01 1909: 1.09E-02 1895: 1.67E-01 2326: 1.45E-03 1666: 8.69E-02
1750: 3.93E-04 1025: 1.76E+02 352: 1.00E-20 347: 1.00E-20 1860: 2.19E+01 630: 1.18E+04 834: 6.10E+03 835: 4.22E+03
1808: 4.88E+03 1256: 4.82E+01 -3: 2.96E-01 -48: 4.13E-09 3934: 1.79E+01 3969: 9.01E+00 8498: 6.18E-05 8542: 5.69E-04
8662: 3.14E-04 353: 1.00E-20 1304: 6.04E+02 1122: 4.03E-01 990: 1.74E+03 1402: 4.79E-02 1214: 6.35E-02 1486: 9.91E-03 2352: 1.17E-02 1406: 7.74E-02 1656: 1.51E+01 9830: 2.52E-09 8727: 2.03E-08 6300: 1.60E-66 5577: 3.87E-09 7291: 1.20E-06
7324: 8.28E-07 1039: 8.58E+01 -8446: 2.36E-11 -4368: 8.95E-14 -132: 6.08E-15 -113: 4.02E-14 -29: 8.33E-14 -46: 6.33E-14
-245: 9.69E-07 765: 6.03E+03 -1198: 5.12E-02 786: 1.52E+02
C157: 3.26E-04 N122: 3.30E-04 N205: 4.72E-05 N57: 7.45E-03 0146:-1.20E-03 063: 1.55E-02 088: 2.55E-02 052: 6.54E-02
026: 8.62E-02 NE13: 2.04E-03 NE36:-1.78E-03 NE16: 6.25E-02 MG4: 5.60E-03 MG14:-5.27E-06 MG6: 3.49E-03 SI35: 1.64E-03
519: 3.86E-03 S34: 4.91E-03 S11: 5.35E-03 AR7: 3.10E-08 AR9: 3.78E-07 AR22:-4.18E-09 AR13: 1.01E-06 AR8: 6.29E-09 CA3: 1.46E-05 CA12:-9.24E-09 CA4: 1.17E-05 Ne14: 9.62E-03 Ne24: 5.21E-02 Si3: 1.00E-20 Si4: 1.00E-20 Fe7: 1.00E-20
CAS: 1.406-20 CA2: -9.24E-09 CA4: 1.17E-09 Ne14: 9.62E-03 Ne24: 5.21E-02 S15: 1.40E-20 S14: 1.00E-20 Fe7: 1.40E-20
Old hydro optical depths: 1 9.99E+07 2 1.00E-20 3 1.00E-20 4 1.00E-20 5 1.00E-20 6 1.00E-20 7 1.00E-20
Lines: 2-1 9.96E+09 3-2 3.34E-02 4-3 3.33E-04 5-4 1.66E-05 6-5 2.56E-06 7-6 2.56E-07 8-7 2.56E-08
New hydro optical depths: 1 5.00E+07 2 7.76E-06 3 1.50E-05 4 4.26E-06 5 1.07E-12 6 2.48E-12 7 1.07E-11 Lines: 2-1 1.04E+06 3-2 4.94E-03 4-3 1.18E-09 5-4 9.44E-10 6-5 8.33E-11 7-6 1.12E-08 8-7 1.47E-07
DINES. 2-1 1.04E+00 J=2 4.94E-03 4-5 1.10E-09 J-4 9.44E-10 0-5 8.55E-11 /-0 1.12E-08 0-7 1.47E-07
Old He Is optical depths: 1 4.15E+05 2 0.00E+00 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7 5.00E-21
Lines: 2-1 9.96E+09 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 0.00E+00
New HE Is optical depths: 1 2.56E+01 2 2.54E-04 3-9.73E-17 4-3.44E-16 5-7.04E-16 6-1.26E-15 7-1.42E-14
Lines: 2-1 6.59E+04 3-2 9.77E-04 4-3 6.06E-11 5-4 4.05E-11 6-5 3.21E-11 7-6 4.23E-10 8-7 5.46E-09
Old He II optical depths: 1 4.15E+05 2 4.15E+05 3 5.00E-21 4 5.00E-21 5 5.00E-21 6 5.00E-21 7 5.00E-21
Lines: 2-1 9.96E+09 3-2 1.00E-20 4-3 1.00E-20 5-4 1.00E-20 6-5 1.00E-20 7-6 1.00E-20 8-7 0.00E+00
New HE II optical depths: 1 3.38E+01 2 1.03E+02 3-7.69E-16 4-1.98E-15 5-3.88E-15 6-6.72E-15 7-7.27E-14
Lines: 2-1 1.09E+06 3-2 1.08E-04 4-3 1.73E-11 5-4-1.16E-12 6-5-6.90E-11 7-6 2.77E-10 8-7 3.89E-09
Hydrogen -1.104 -0.036 Log10 Mean Ionisation (over volume)
Helium -1.142 -0.173 -0.536
Carbon -2.976 -0.795 -0.303 -0.555 -1.209
Nitrogen -1.413 -0.747 -0.377 -0.555 -1.151 -1.876
Oxygen -1.132 -0.850 -0.248 -0.818 -1.210 -2.235 -4.004
Neon - 1.899 -1.370 -0.153 -0.797 -1.103 -2.597 -5.971 Magnesium -2.960 -0.702 -0.245 -0.754 -1.305 -2.206 -4.644
Aluminum -3.625 -0.473 -0.518 -0.501 -1.384 -2.572 -5.054
Silicon -4.214 -0.545 -0.585 -0.481 -0.916 -2.398 -5.148
Sulphur -4.983 -0.785 -0.317 -0.611 -1.286 -1.333 -1.978
Argon -1.507 -1.138 -0.302 -0.560 -0.985 -1.870 -2.309 -3.703 -5.813 Calcium -1.893 -0.711 -0.335 -0.766 -1.251 -1.113 -1.621 -2.790 -4.774
$ \begin{array}{c} \text{Calchum} & -1.695 & -0.711 & -0.535 & -0.765 & -1.251 & -1.115 & -1.261 & -2.790 & -4.774 \\ \text{Iron} & -2.695 & -0.882 & -0.825 & -0.375 & -1.237 & -0.843 & -1.080 & -2.043 & -4.267 \\ \end{array} $

4 5 1 2 3 6 7 8 9 10 11 12 13 14 15 16 17 Hydrogen -1.435 -0.016 Helium -1.764 -0.364 -0.259 Carbon -3.291 -1.097 -0.445 -0.411 -0.764 Nitrogen -1.761 -1.051 -0.507 -0.445 -0.751 -1.329 Oxygen -1.474 -1.144 -0.368 -0.555 -0.779 -1.670 -3.341 Neon -2.252 -1.684 -0.316 -0.560 -0.687 -2.039 -5.249 Magnesium -3.282 -0.991 -0.369 -0.504 -0.876 -1.640 -3.975 Aluminum -3.945 -0.732 -0.601 -0.349 -0.973 -2.004 -4.366 Silicon -4.550 -0.836 -0.710 -0.411 -0.588 -1.888 -4.490 Sulphur -5.330 -1.091 -0.465 -0.532 -0.985 -0.859 -1.390 Argon -1.856 -1.425 -0.493 -0.492 -0.621 -1.355 -1.685 -3.007 -5.054 Calcium -2.205 -0.965 -0.498 -0.733 -0.987 -0.715 -1.097 -2.163 -4.070 Iron -3.041 -1.214 -1.084 -0.527 -1.158 -0.602 -0.685 -1.503 -3.619 Log10 Mean Ionisation (over radius) Normalised continuum 0.51 6.544 0.56 5.419 1.00 0.999 0.2552.710 0.2738.477 0.3026.227 0.3318.318 0.3613.548 0.3910.272 0.62 4.468 0.67 3.363 0.74 1.527 0.81 1.014 0.88 1.023 0.97 0.999 0.43 8.203 0.47 8.120 0.98 0.999 0.99 0.99 Emergent continuum - phot/ryd/cm2 (r in) 1.8 1.70E-01 3.9 2.74E+08 7.51E+00 1.75E+05 2.0 5.43E+04 4.0 1.80E+06 8.47E+00 2.15E+06 2.3 8.35E+05 4.2 1.47E+05 9.54E+00 1.53E+07 2.5 3.06E+02 4.7 9.80E+01 1.07E+01 3.56E+07 3.2 4.67E+06 5.9 4.88E+00 1.36E+01 2.68E+07 3.6 7.61E+07 6.7 2.40E+03 1.54E+01 1.10E+07 1.0 5.47E+07 1.0 4.15E+07 1.0 3.14E+07 1.1 1.58E+06 1.2 1.21E+04 1.4 1.11E+02 1.6 2.65E+05 0.26 2.66E+13 0.60 4.86E+12 0.29 1.75E+13 0.67 3.69E+12 0.33 1.19E+13 0.76 1.21E+12 0.37 8.80E+12 0.86 1.25E+12 0.42 6.92E+12 0.97 1.32E+12 0.47 6.99E+12 0.99 1.33E+12 0.53 5.76E+12 0.99 1.33E+12 1.73E+01 2.92E+06 1.95E+01 5.17E+05 2.20E+01 5.19E+04 2.48E+01 4.33E+03 2.79E+01 2.35E+02 3.14E+01 7.68E+00

**************************************	*
*	*
* title check pure hydrogen Stromgren sphere	*
* c the answer is R(Stromgren) = 4.16E17 cm	*
* hden 4	*
* sphere static	*
* radius 16	*
* blackbody 50,000k	*
* q(h) 49	*
* stop eden 3.	*
* constant temper 7500	*
* abundances -10	*
* print short	*
* c strom.in	*
* c cray	*
*	*
***************************************	*

Chemical composition He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 Al:1.0E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10

333Cell Peak1.24E+00	Lo 1.00E-05=0.9105cm	Hi-Con:1.16E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 38.5118	Average nu:1.491E+00	P(X-ray): 0.0000	P(BalC): 38.3651	Q(Balmer C): 49.2411
Q(1.0-1.8): 48.9070	Q(1.8-4.0): 48.2845	Q(4.0-20): 45.8883	Q(20): 0.0000	Ion pht flx:7.962E+15
L(gam ray): 0.0000	Q(gam ray): 0.0000	L(Infred): 37.0224	Alf(ox): 0.0000	Total lumin: 38.7538
L/Lsolar: 5.1710	Abs bol mg: -8.2075	Abs V mag: -3.9048	Bol cor: -4.3027	nuFnu(Bbet): 37.1233
U(1.0):2.656E+01	U(4.0):2.053E-02	T(En-Den):2.112E+02	T(Comp):4.787E+04	nuJnu(912A):3.069E+05
Occ(FarIR):9.570E-06	Occ(H n=6):3.435E-09	Occ(1Ryd):1.415E-11	Occ(4R):1.021E-15	Occ (Nu-hi):7.434E-26
Tbr(FarIR):1.592E-05	Tbr(H n=6):1.525E-05	Tbr(1Ryd):2.235E-06	Tbr(4R):6.460E-10	Tbr (Nu-hi):1.336E-19

 Thr (FarIR): 1.592E-05
 Thr (H n=6): 1.525E-05
 Thr (IRyd): 2.235E-06
 Thr (R): 6.460E-10
 Thr (Nu-h1): 1.336E-19

 #####
 1 Te: 7.500E+03
 Hden: 1.000E+04
 Ne: 1.000E+04
 Re: 1.006E+06
 Re: 1.000E+06
 Re: 1.000E+06
 Ne: 1.00E+10
 Ne: 1.00E+10 Iron0.000E+000.000E+000.000E+002.141E-032.600E-017.311E-015.871E-030.000E+000

HeII	4.367E-01	8.337E-14	1.480E-20	3.082E-20	5.645E-20	9.391E-20	9.062E-19	1.141E-17	2.969E-15	PRAD/GAS;	2.544E-02	
Pressure	NgasTgas;	8.269E+07	P(total):	1.207E-08	P(gas):	1.142E-08	P(Radtn):	6.501E-10	Rad accel	7.071E-08	Force Mul	4.954E+02
Carbon	5.134E-05	9.833E-01	1.668E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	H2O+/Otot	0.000E+00	OH+/Ototl	0.000E+00	
Nitrogen	1.620E-01	8.379E-01	1.003E-04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	02/0totl:	0.000E+00	02+/0tot:	0.000E+00
Oxygen	9.302E-01	6.983E-02	1.310E-05	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	Hex(tot):	0.000E+00	A:-12.486
Neon										0.000E+00		
Magnesium () 5.269E-04	9.184E-01	8.106E-02	0.000E+00								
Aluminium (0 4.975E-05	9.895E-01	1.011E-02	3.235E-04	0.000E+00							
Silicon (2.827E-05	9.995E-01	4.417E-04	0.000E+00								
Sulphur (0 1.195E-05	9.720E-01	2.799E-02	0.000E+00								
Argon (0 6.600E-01	3.197E-01	2.023E-02	0.000E+00								
Calcium (0 1.218E-04	1.785E-02	9.819E-01	1.646E-04	0.000E+00							
	0 1.464E-03				0.000E+00							
Calculati	ion stopped	because lo	owest EDEN	reached.								
Geometry	is spherica	1.										

Photoionization of He 2TriS reached 100.0 percent of the total rate out.

W-Heating - cooling mismatch = 1.61E+00 Whats wrong????
 C-I must iterate when SPHERE STATIC is set.
 Frequency out of range of free-free gaunt factor routine.
 The ratio of radiation to gas pressure reached 2.51E+05. Caused by Lyman alpha.

CLOUDY 80.08

**************************************	08 <************************************
title check pure hydrogen Stromgren sphere	,
c the answer is R(Stromgren) = 4.16E17 cm	,
hden 4	,
sphere static	,
radius 16	,
blackbody 50,000k	•
(h) 49	,
stop eden 3.	,
constant temper 7500	•
abundances -10	
print short	,
c strom.in	
c cray	,
**************************************	42 <************************************
>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	s suspect.

Emission Line Spectrum. Constant Density Model. Closed geometry. Iteration 1 of 1. Luminosity (erg/s) emitted by shell with full coverage.

TOTL 4861 36.661	1.0000	Q(H) 1216	38.211	35.5014	TOTL26252	35.254	0.0392	Inci	4861 37.123	2.9030
TOTL 1216 38.112	28.2669	TOTL 6563	37.105	2.7823	TOTL74578	34.924	0.0183	Inci	1216 38.453	62.0146
TotH 0 38.021	22.9116	TOTL 4861	36.661	1.0000	2 NU 0	37.471	6.4625	BA C	0 37.263	4.0035
BFH1 0 38.021	22.9092	TOTL 4340	36.377	0.5203	TOTL 1216	38.112	28.2669	PA C	0 36.761	1.2602
BFHx 0 33.933	0.0019	TOTL 4102	36.157	0.3136	INWD 1216	38.112	28.2664	H FF	0 36.645	0.9639
CA B 4861 36.673	1.0298	TOTL18751	36.129	0.2941	Dest 1216	34.056	0.0025	H FB	0 36.835	1.4930
CA B 1216 38.197	34.3612	TOTL12818	35.856	0.1569	e sc18751	34.716	0.0114	Cool	1216 34.363	0.0050
DU B 4861 36.673	1.0298	TOTL10938	35.638	0.0950	nFnu 4860	37.006	2.2141	TOFF	0 36.645	0.9639
Q(H) 4861 36.677	1.0384	TOTL40512	35.445	0.0609	nFnu 1215	33.852	0.0016			

Cooling: H FF Heating: BFH1	0:0.391 H F 0:1.000		EN STROMGREN S	PHERE			
IONIZE PARMET: ENERGY BUDGET: Column density	U(1-) 1.4242 Heat: 38.021 H12:4.068E+21 OH: 0.000E+00	Coolg: 37.052	Error: 89.3%	Q(ion): 44.701 Compt H: 31.595 H-: 2.344E+11	WorkF: 38.320	F-F H 31.989	P(low) 38.38 PRADMX:2.51E+05 He H+:5.083E+03
<nh>:1.000E+04 He/Ha:9.00E-11 T He+:7.50E+03 <a>:0.00E+00 Mean Jeans</nh>	<pre><tp>:7.50E+03 = 0.90*true EHe+:9.90E+03 erdeFe0.0E+00 l(cm)4.42E+19</tp></pre>	<pre><t03>:7.50E+03 N/Oap:1.34E+00 T(0+):7.50E+03 Tcompt6.21E+03 M(sun)3.76E+05</t03></pre>	Ne:9.988E+03 = 1.34true EO+:9.30E+03 Tthr8.10E+08 smallest:	ti(snd):3.65E+11 T(03R):7.791E+03 iter/zn: 1.000 <tden>: 7.50E+03 len(cm):4.42E+19</tden>	L THIN:1.00E+30	<t(s2)>:7.50E+03 Te-high:7.50E+03 <mol>:5.03E-01</mol></t(s2)>	<e(s2)>:6.86E+03</e(s2)>

*	
* title test against Van Blerkom and Hummer, fig 4	
* c tesest hydrogen grd state rec effic against vb+h exact results	
* c this is their case e) - "zero condition"	
* c their answer for H0/Htot at the illuminated edge is approx 5.8E-4,	
* c and a Stromgren radius of roughly 7.8E16 cm	
* hden 4	
* blackbody 50,000k	
* phi(h) 12.30103	
* stop eden 3.5	
* constant temper 4	
* abundances -10	
* print short	
* c vbhum.in	
* c cray	
*	

Chemical composition He:.000 C:1.00E-10 N:1.00E-10 O:1.00E-10 Ne:1.00E-10 Mg:1.00E-10 A:1.0E-10 S:1.00E-10 A:1.0E-10 Ca:1.0E-10 Fe:1.00E-10

333Cell Peak1.24E+00 Lo	1.00E-05=0.9105cm Hi	-Con:1.16E+01 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 1.8129 Ave	erage nu:1.491E+00 P(X-ray): 0.0000	P(BalC): 1.6661	Q(Balmer C): 12.5421
Q(1.0-1.8): 12.2081 Q(1	1.8-4.0): 11.5855 Q(4.0-20): 9.1894	Q(20): 0.0000	Ion pht flx:2.001E+12
L(gam ray): 0.0000 Q(c	gam ray): 0.0000 L(Infred): 0.3234	Alf(ox): 0.0000	Total lumin: 2.0548
			T(Comp):4.787E+04	nuJnu(912A):7.712E+01
			Occ(4R):2.567E-19	Occ (Nu-hi):1.868E-29
				Tbr (Nu-hi):3.359E-23
	,	(1)	()	
##### 1 Te:1.000E+04 Hden:1.000E+04	4 Ne:9,994E+03 R:1,000E	S+25 B-B0:1.370E+15 d	R:2.739E+15 NTR: 1 Ht	ot:1.988E-16 T912: 9.995E-02###
-1.17 4686 0.00 5876 0.00 1909 0				
				+ 1.758E-20 H col den 2.739E+19
				: 2.638E+01 T(diffs): 2.877E+02
				t 1.000E+00 Gam 1/tot 9.997E-01
He singlet 1.720E-03 8.819E-11 5.00				
HeII 9.168E-01 1.124E-11 4.87				
				1 1.884E-06 Force Mul 1.244E+03
Carbon 1.905E-05 5.321E-02 9.08				
Nitrogen 2.348E-05 4.664E-02 9.13	38E-01 3.949E-02 0.000E	S+00 0.000E+00 0.000E	+00 0.000E+00 02/0tot1	: 0.000E+00 O2+/Otot: 0.000E+00
				0 Hex(tot): 0.000E+00 A:-12.472
Neon 1.298E-04 9.984E-02 8.95				
Magnesium 0 7.654E-05 3.502E-02 9.64				
Aluminium 0 2.683E-05 1.117E-01 6.81				
				0 0.000E+00 0.000E+00 0.000E+00
				0 0.000E+00 0.000E+00 0.000E+00
				0 0.000E+00 0.000E+00 0.000E+00
				0 0.000E+00 0.000E+00 0.000E+00
				0 0.000E+00 0.000E+00 0.000E+00
##### 48 Te:1.000E+04 Hden:1.000E+04				
-0.02 4686 0.00 5876 0.00 1909 0				
Hydrogen 7.432E-01 2.568E-01 H+0/				+ 1.257E-16 H col den 7.786E+20
				: 2.151E+01 T(diffs): 2.625E+02
				t 1.000E+00 Gam 1/tot 3.280E-01
He singlet 2.774E-01 2.083E-11 3.49				
HeII 6.806E-01 7.102E-13 2.46				
			1, ,	,,

Pressure	NgasTgas; 1.331E+	08 P(total): 1.908E-0	8 P(gas): 1.838E-	08 P(Radtn): 7.019E-	10 Rad accel 3.	.234E-07 Force Mul	1.599E+03
Carbon	3.254E-04 9.313E-	01 6.839E-02 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 H2O+/Ot	ot 0.000E+00 OH	H+/Ototl 0.000E+00	
Nitrogen	4.649E-02 9.526E-	01 9.115E-04 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 02/Ototl: 0.	.000E+00 O2+/Otot:	0.000E+00
Oxygen	7.639E-01 2.357E-	01 3.322E-04 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 He	ex(tot): 0.000E+00	A:-12.588
Neon	5.788E-02 3.763E-	01 5.659E-01 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	
Magnesium (0 4.459E-03 9.133E-	01 8.220E-02 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Aluminium (0 3.426E-04 9.848E-	01 1.477E-02 1.297E-0	4 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Silicon (0 1.117E-04 9.951E-	01 4.767E-03 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Sulphur (0 3.198E-05 9.308E-	01 6.917E-02 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Argon (0 4.769E-01 4.635E-	01 5.960E-02 0.000E+0	0 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Calcium (0 6.508E-03 1.107E-	01 8.824E-01 4.389E-0	4 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Iron (0 1.548E-02 9.529E-	01 3.157E-02 1.595E-0	5 0.000E+00 0.000E+	00 0.000E+00 0.000E+	00 0.000E+00 0.	.000E+00 0.000E+00	0.000E+00
Calculat:	ion stopped because	lowest EDEN reached.					
Geometrv	is plane-parallel.						

Geometry is plane-parallel. Photoionization of He 2TriS reached 40.8 percent of the total rate out. W-Heating - cooling mismatch = 1.42E+00 Whats wrong???? Frequency out of range of free-free gaunt factor routine. The radiation to gas pressure reached 2.27E+00. Caused by Lyman alpha. C-The HeII continuum is thin and I assumed that it was thick. Try another iteration.

* title test against Va	n Blerkom and Hummer, fig 4	
* c tesest hvdrogen gro	state rec effic against vb+h exact results	3
* c this is their case		
c their answer for H0	Htot at the illuminated edge is approx 5.	3E-4,
c and a Stromgren rad	ius of roughly 7.8E16 cm	
* hden 4		
 blackbody 50,000k 		
<pre>* phi(h) 12.30103</pre>		
* stop eden 3.5		
* constant temper 4		
* abundances -10		
* print short		
* c vbhum.in		
* c cray		
	********> LOG(U): -2.18 <************************************	******
	st, this calculation is suspect.	
>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>	ation is suggested.	
iggion Tine Chestrum	Constant Density Model. Open geometry	. Iteration 1 of

TOTL 4861 -0.016	1,0000	TOTI 4861 -0.016	1,0000	TOTL 1216 1.447	29.0388	nFnu 1215 -1.748	0.0185
TOTL 1216 1.447	29.0388	TOTL 4340 -0.314	0.5033	TOTL 1026 -2.660		Inci 4861 0.424	2.7579
TotH 0 1.341	22.7791	TOTL 4102 -0.545	0.2962	TOTL 973 -2.666	0.0022	Inci 1216 1.754	58.9147
BFH1 0 1.341	22.7785	TOTL18751 -0.571	0.2784	TOTL 950 -2.634	0.0024	BA C 0 0.595	4.0797
CA B 4861 -0.030	0.9688	TOTL12818 -0.844	0.1486	TOTL 938 -2.591	0.0027	PA C 0 0.082	1.2525
CA B 1216 1.504	33.1156	TOTL10938 -1.067	0.0889	C13c 6563 -2.500	0.0033	H FF 0 0.121	1.3698
DU B 4861 -0.030	0.9688	TOTL40512 -1.255	0.0576	CION 0 -2.474	0.0035	H FB 0 0.298	2.0597
Q(H) 4861 -0.022	0.9865	TOTL26252 -1.451	0.0367	INWD 1216 1.447	29.0387	Cool 1216 -0.426	0.3891
Q(H) 1216 1.512	33.7268	TOTL74578 -1.781	0.0172	e sc18751 -1.799	0.0165	Toff 0 0.121	1.3698
TOTL 6563 0.424	2.7569	2 NU 0 0.807	6.6543	nFnu 4860 0.416	2.7016		

TEST AGAINST VAN BLERKOM AND HUMMER, FIG 4 Cooling: H FF 0:0.356 H FB 0:0.536 Cool 1216:0.101							
Heating: BFH1	0:1.000						
IONIZE PARMET:	U(1-) -2.1755	U(4-): -5.2875	U(sp): -2.18	Q(ion): 9.044	L(ion): -1.047	Q(low): 12.61	P(low) 1.69
ENERGY BUDGET:	Heat: 1.341	Coolg: 0.569	Error: 83.1%	Compt H: -5.894	WorkF: 1.659	F-F H -4.878	PRADMX:2.27E+00
Column density	H12:7.786E+20	H II:7.627E+20	HI:1.589E+19	H-: 4.100E+11	H2: 8.589E+11	H2+:1.553E+11	He H+:1.763E+03
	OH: 0.000E+00	Heff:0.000E+00					
<nh>:1.000E+04</nh>	<tp>:1.00E+04</tp>	<to3>:1.00E+04</to3>	Ne:9.966E+03	ti(snd):6.07E+10	NeN+dl:7.54E+24	<t(c3)>:1.00E+04</t(c3)>	<e(c3)>:9.92E+03</e(c3)>
He/Ha:1.16E-10	= 1.16*true	N/Oap:1.08E+00	= 1.08true	T(O3R):9.978E+03	L THIN:1.00E+30	<t(s2)>:1.00E+04</t(s2)>	<e(s2)>:8.47E+03</e(s2)>
T He+:1.00E+04	EHe+:9.83E+03	T(O+):1.00E+04	EO+:9.51E+03	iter/zn: 1.000	Te-low:1.00E+04	Te-high:1.00E+04	Hlu/zn:1.37E+00
<a>:0.00E+00	erdeFe0.0E+00	Tcompt2.47E+07	Tthr7.97E+08	<tden>: 1.00E+04</tden>	<dens>:1.66E-20</dens>	<mol>:5.05E-01</mol>	
Mean Jeans	l(cm)5.60E+19	M(sun)7.69E+05	smallest:	len(cm):5.60E+19	M(sun):7.69E+05	Alf(ox-tran):	0.0000

	* * * * * * * * * * * * * * * * * * * *
title test of equations of motion in a wind	
c test of wind code	
<pre>c radiative acceleration (e- only) is 9.54E-7 cm s^-2</pre>	
<pre>c fadiative acceleration (e= only) is 9.54E=7 cm s =2</pre> <pre>c terminal velocity (e= only) is 7.6 km s^-1</pre>	
* hden 4	
* table agn	
* luminosiy (total) 45	
radius (parsecs) 1	
stop thickness (parsecs) -1	
no radiation pressure	
* wind 0.1	
* constant temperature 8	
* print only zones	
c wind.in	
* c cray	
*	

Chemical composition He:.098 C:3.63E-04 N:1.12E-04 O:8.51E-04 Ne:1.23E-04 Mg:3.80E-05 Al:3.0E-06 Si:3.55E-05 S:1.62E-05 A:3.6E-06 Ca:2.3E-06 Fe:4.68E-05

546Cell Peak1.78E+00	Lo 1.00E-05=0.9101cm	Hi-Con:7.34E+06 Ryd	E(hi):7.35E+06Ryd	E(hi): 100.01 MeV
P(nu>1ryd): 44.7349	Average nu:3.038E+00	P(X-ray): 43.9062	P(BalC): 44.2392	Q(Balmer C): 55.2020
Q(1.0-1.8): 54.6108	Q(1.8-4.0): 54.5031	Q(4.0-20): 53.9656	Q(20): 52.2283	Ion pht flx:6.858E+14
L(gam ray): 43.6447	Q(gam ray): 50.0597	L(Infred): 44.4533	Alf(ox): -1.4120	Total lumin: 45.0003
L/Lsolar: 11.4175	Abs bol mg: -23.8237	Abs V mag: -21.2231	Bol cor: -2.6006	nuFnu(Bbet): 43.8959
U(1.0):2.287E+00	U(4.0):2.622E-01	T(En-Den):1.386E+02	T(Comp):1.327E+07	nuJnu(912A):1.449E+04
Occ(FarIR):1.288E-03	Occ(H n=6):4.859E-07	Occ(1Ryd):6.683E-13	Occ(4R):3.426E-15	Occ (Nu-hi):4.775E-43
Tbr(FarIR):2.144E-03	Tbr(H n=6):2.157E-03	Tbr(1Ryd):1.056E-07	Tbr(4R):2.167E-09	Tbr (Nu-hi):5.269E-31

D(IINES). 0 000 0 000 0 000	0 0.000 0.000 0.000 1.000 0.0			0 000 0 000 0 000
Hydrogen 1.720E-12 1.000	0E+00 H+0/Hden: 1.000E+00 0.0	000E+00 H- H2 0.000E+00 0	0.000E+00 H2+ HeH+ 0.000E+00	H col den 7.856E+19
	3E-23 1.778E-23 1.928E-23 2.3			
Helium 1.515E-19 3.015	5E-10 1.000E+00 He I 2S3 1.1	169E-20 Comp H, C 7.358E-20 5	5.546E-19 Fill Fact 1.000E+00	Gam 1/tot 9.069E-01
He singlet 1.398E-19 2.029	9E-24 2.866E-31 5.516E-31 1.0	009E-30 1.738E-30 He triplt 1	1.169E-20 1.552E-29 1.279E-31	1.468E-31 1.154E-32
HeII 3.015E-10 1.308	8E-16 1.640E-23 1.685E-23 1.9	994E-23 2.395E-23 1.511E-22 2	2.536E-22 3.121E-20 PRAD/GAS;	0.000E+00
Pressure NgasTgas; 3.062	2E+10 P(total): 4.227E-06 P(gas): 4.227E-06 P(Radtn): 0	0.000E+00 Rad accel 9.103E-07	Force Mul 9.860E-01
Carbon 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 2.5	518E-10 1.499E-05 1.000E+00 H	H2O+/Otot 0.000E+00 OH+/Otot1	0.000E+00
Nitrogen 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 1.967E-09 4.406E-05 1	1.000E+00 O2/Ototl: 0.000E+00	O2+/Otot: 0.000E+00
Oxygen 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 1.142E-08 1	1.148E-04 9.999E-01 Hex(tot):	0.000E+00 A:-16.938
Neon 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 2.476E-07 5.727E-04	9.994E-01
Magnesium 1 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 0.000E+00 2.989E-06	2.125E-03 9.979E-01
Aluminium 2 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 0.000E+00 9.636E-05	4.249E-03 9.957E-01
Silicon 3 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 0.000E+00 2.025E-05	6.052E-03 9.939E-01
Sulphur 5 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 0.000E+00 1.136E-04	1.513E-02 9.848E-01
Argon 7 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 2.084E-06 1.306E-03	3.544E-02 9.633E-01
Calcium 9 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 0	0.000E+00 4.836E-06 1.773E-03	7.338E-02 9.248E-01
Iron 15 0.000E+00 0.000	0E+00 0.000E+00 0.000E+00 0.0	000E+00 0.000E+00 0.000E+00 2	2.699E-06 7.743E-04 5.809E-02	3.313E-01 6.098E-01